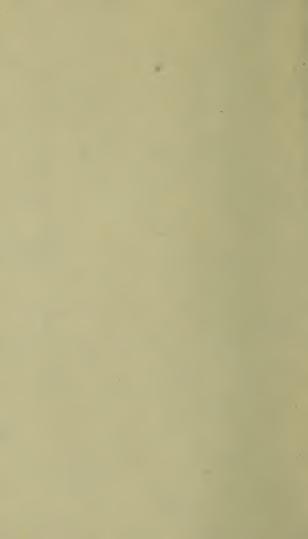
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# HANDY

# MECHANICAL POCKET COMPANION

FOR THE

# Engineer, Business Man & Mechanic.

CONTAINING

TABLE OF METALS, STRENGTH OF MATERIALS, WAGES, BOARD
MEASURE, SCANTLING MEASURE, CUTTING SCREWS BY
LATHE, HORSE-POWER OF SHAFTING, BELTING,
CIRCUMFERENCES, AREAS, SQUARES, CUBES,

SQUARE ROOT, CUBE ROOT ETON ETO COPYRIGHT

OMPILED BY WASHINGTON.

A. W. HABBIN.

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#### PREFACE.

This little collation of authorities and culling of condensed and useful tables, rules, etc., is designed to meet a growing demand for something more practical and concise for the use of Mechanics, in all the different departments of Mechanical industries.

It has been arranged with great care, selected from the best authorities, just the right thing and an endeavor made to put them in the right place.

This volume gives more practical and less theoretical knowledge than can be found in any other book yet offered to the practical Mechanic, and at a price within the reach of all.

The idea has been to have this book published in such a shape that it can be carried in a pocket so that it may be referred to at any time.

A. W. H.



## THE CHEMICAL KINGDOM.

# NAME, WHEN DISCOVERED, BY WHOM, SYMBOLS, COLOR AND SPECIFIC GRAVITY.

Name. Dis- cov. By whom. Sy- m.	Color. Sp'c. G'ty.
Aluminum.  1808  Davy.  Al  Wh	
	ish White 6.70
Arsenic.   1733 Brandt.   As Gra	
	k Gray   1.50
	low'h W'te 9.80
Boran.   1808 Davy.   B   Wh	ite   2.00
	wnish R'd 2.97
Cadmium.   1817   Stromeyer.   Cd   Wh	
Cæsium.   1860   Bunsen.   Cs   Blu	
Calcium.   1808 Davy.   Ca   Wh	
Carbon.   Ancients.   C   Bla	
	y White
	enish 2.49
Chromium.   1797   Vanquelin.   Cr   Gra	yish W'te 6.00
	w White 8.90
	n Gray 5.50
Copper.   Ancients.   Cu   Red	8.90
Didymium.   1841   Mosander.   D	
Erbium.   1841   Mosander.   E   Wh	
	orless   1.29
Gallium. 1875 Lecoq. ?	
Gold.   Ancients.   An   Yel	
Glucinum. 1828 Wohler. G Wh	
	orless .07
Indium.   1863   Reichter.   In   Blu	
	yish Bla'k 4.95
Iridium.   1803   Tennant.   Ir   Wh	
	ish Gray   7.90
Lanthanum. 1841 Mosander.   La   Red	
Lead.   Ancients.   Pb   Blu	
Lithium. 1817 Bunsen. L Wh	
	er White 3.70
	y White 8.00
Mercury.   Ancients.   Hg   Wh	ite   13.60

#### CHEMICAL KINGDOM. (Continued.)

IDt. I	1 01
Name. $\begin{vmatrix} Dis-\\ cov. \end{vmatrix}$ By Whom. $\begin{vmatrix} Sy-\\ m. \end{vmatrix}$ Color,	S. G.
Molybdenum.   1782 Hjelm.   M   Gray	8.60
Nickel. 1751 Cronstedt. Ni White	8.80
Nitrogen. 1772 Rutheford. N Colorless	.97
	10.00
Oxygen.   1774 Priestley.   O   Colorless	1.11
Palladium.   1803   Wallaston.   Pd   Bluish Wh'te	11.80
Phosphorus, 1669 Brandt, P Yellow	2.00
Platinum.   1741 Wood.   Pt   Bluish Wh'te	21.50
Potassium   1807 Davy, K Gray White	.87
Rhodium.   1803   Wallaston.   Ro   Grayish W'te	10.60
Rubidium.   1860 Bunsen.   Rb   Red	
Ruthenium.   1847   Claus.   Ru   White	
Selenium.   1818 Berzelius.   Se   Dark Brown	4.32
Silicon.   1824   Berzelius.   Si   Brown	
	10.50
Sodium.   1808  Davy.   Na   Gray White	.97
Strontium.   1808  Davy.   Sr   Gray	2.50
Sulphur.   Ancients.   S   Yellow	1.99
Tantalum.   1802 Ekeberg.   Ta	
Tellurium.   1798   Klaproth.   Te   Bluish Wh'te	6.20
Thallium.   1861   Crookes.   Th.   Green	
Thorium.   1828   Berzelius.   Th   White	
Tin.   Ancients.   Su   White	7.30
Titanium.   1789 Gregor.   Ti   Red	5.30
Tungsten.   1781 De Layurt.   W   Brown'h B'k	7.40
Uranium.   1789   Klaproth   U   Gray	8.00
Vanadium.   1830   Sefstrom.   V   White	
Yttrium.   1828   Wohler.   Y   White	
Zinc.   1540   Paracelsus.   Zn   Bluish Wh'te	7.00
Zirconium.  1824 Berzelius.  Zr  White	

#### METAL BORING AND TURNING.

Boring Cast-Iron—Divide 25 by the diameter of the cylinder in inches for the revolutions per minute. \*

- " Wrought-Iron—The speed is one fifth greater than for east-iron.
- "Brass—The speed is one half that, for cast—iron.
  Turning Cast-Iron—The speed is twice that of boring.
  - " Wrought-Iron—The speed is one fifth greater than that for cast–iron.
    - ' Brass—The speed is twice that of boring.

Verticle Boring—The speed may be twice that of horizontal boring.

The feed depends upon the stability of the machine and depth of cut.

IRON TURNING and BORING by means of the SLIDE REST.

Diameter in Inches.	Revolution of Spindle per Minute.	Diameter in Inches.	Revolution of Spindle per Minute.	Diameter in Inches.	Revolution of Boring bar per Minute.	Diameter in Inches.	Revolution of Boring bar per Minute.
1 2 3 4 5 6 7 8 9 10 15 20	50. 25. 16.67 12.50 10. 8.32 7.15 6.25 5.5 5. 3.33 2.50	25 30 35 40 45 50 60 70 80 90 100	2. 1.667 1.430 1.250 1.120 1. .834 .716 .626 .554 .500	1 2 3 4 5 6 7 8 9 10 15 20	25. 12.500 8.330 6.250 5. 4.160 3.570 3.125 2.770 2.500 1.660 1.250	25 30 35 40 45 50 60 70 80 90 100	1. .833 .714 .425 .566 .500 .417 .358 .313 .278 .250

Velocities of Wood-working Machinery in Feet or Revolutions per Minute.

Circular Saws, at periphery, 6000 to 7000 feet.

Band Saws, 2500 feet.

Gang Saws, 20 inch stroke, 120 strokes, per minute.

Scroll Saws, 300 strokes, per minute.

Planing machine cutters at periphery, 4000 to 6000 feet.

Work under planing machine, 1-20 of an inch for each cut.

Molding-machine cutters, 3500 to 4000 feet.

Squaring-up-machine cutters, 7000 to 8000 feet.

Wood-Carving drills, 5000 revolutions.

Machine augers, 11/2 inch in diameter, 900 revolutions.

Machine augers, 34 inch in diameter, 1200 revolutions,

Gang Saws require for 45 superficial feet of pine per hour, one Horse Power.

Circular Saws require for 75 superficial feet of pine per hour, one Horse Power.

In oak or hard wood, 34 ths of the above quantity require one Horse Power.

Table to calculate the Pitch of a Toothed Wheel when the radius and number of teeth are given; and the Radius, when the Pitch and number of teeth are given, from 10 to 159 teeth.

No.	Radi-	No	Radi-	N <sub>O</sub>	Radi-	No.	Radi-	No	Radi-
T'h	us.	T'h		T'h	us.	T'h	us.	T'h	us.
-			<u> </u>						
10	1.618	40	6.373	70	11.144	100	15.918	130	20.692
11	1.774	41	6.532	71	11.303	101	16.077	131	20.851
12	1.932	42	6.691	72	11.463	102	16.236	132	21.010
13	2.089	43	6.850	73	11.622	103	16.395	133	21.169
14	2.247	44	7.009	74	11.781	104	16.554	134	21.328
15	2.405	45	7.168	75	11.940	105	16.713	135	21.488
16	2.563	46	7.327	76	12.099	106	16.873	-136	21.647
17	2.721	47	7.486	77	12.258	107	17.032	137	21.806
18	2.869	48	7.645	78	12.417	108	17.191	138	21.965
19	3.038	49	7.804	79	12.576	109	17.350	139	22.124
20	3.196	50	7.963	80	12.735	110	17.509	140	22.283
21	3.355	51	8.122	81	12.895	111	17.668	141	22.442
22	3.513	52	8.281	82	13.054	112	17.827	142	22.602
23	3.672	53	8.440	83	13.213	113	17.987	143	22.761
24	3.830	54	8.599	84	13.370	114	18.146	144	22.920
25	3.989	55	8.758	85	13.531	115	18.305	145	23.079
26	4.148	56	8.917	86	13.690	116	18.464	146	23.238
27	4.307	57	9.076	87	13.849	117	18.623	147	23.397
28	4.465	58	9.235	88	14.008	118	18.782	148	23.556
29	4.624	59	9.394	89	14.168	119	18.941	149	23.716
30	4.788	60	9.553	90	14.327	120	19.101	150	23.874
31	4.942	61	9.712	91	14.486	121	19.260	151	24.034
32	5.101	62	9.872	92	14.645	122	19.419	152	24.193
33	5.260	63	10.031	93	14.804	123	19.578	153	24.352
34	5.419	64	10.190	94	14.963	124	19.737	154	24.511
35	5.578	65	10.349	95	15.122	125	19.896	155	24.620
36	5.737	66	10.508	96	15.281	126	20.055	156	24.830
37	5.896	67	10.667	97	15.440	127	20.214	157	24.989
38	6.055	68	10.826	98	15.600	128	20.374	158	25.148
39	6.214	69	10.985	99	15.759	129	20.533	159	25.307

Rule 1—Divide the required radius by the radius opposite the given number of teeth in the table; the quotient will be the required pitch of the wheel.

Example—To find the Pitch of a wheel whose radius is 43 inches, that shall contain 90 teeth.

Required radius 43+14.327=3 inch pitch.

Rule 2—Multiply the radius opposite the given number of teeth by the pitch required; the product will be the required radius of the wheel.

Example—To find the radius of a wheel that shall contain 48 teeth of 21/2 inch petch.

In the table, radius  $7.645 \times 2.5 = 19\frac{1}{10}$  inches nearly.

#### PROPORTION SCALES FOR GEARING.

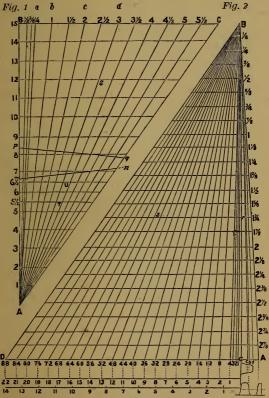


Figure 1 contains the proportions, in which the pitch is supposed to be divided into 15 equal parts.

The construction of this scale is very simple. Thus let A. B. be divided into 15 equal parts, and draw B. C. per-

pendicular to it; and again divide B. C. into a determinate number of parts from B. actual measures of the pitches for which the scale is intended to be used; that is, B a=1/2 inch; B b=1 inch; B c=2 inches, and so on, and join a and A, b and A, c and A, and so on. To complete the scale, draw 15 parallels to B C from the points numbered in the line A B, numbering their intersections (if thought proper) with the line A C in the same order; and also the two parallels T and U, (which are full lines in diagram,) equidistant from the parallels on each side of them.

The scale is thus ready for use, and its principle is selfevident. To get from it the several proportions for a given pitch, say 3 inches=Bd, let the compasses be extended from the intersection of the parallel marked T, with the line A B, to the point where it intersects the line A d; this will be the part of the tooth from the pitch line to the point, and equivalent to 51/2 parts of the pitch. (viz. of Bd;) similarly the compasses being extended from the intersection of the parallel U, with the line A B, to its point of intersection of the line A d. will give the part of the length of the tooth from the pitch line to the root, and equivalent to 62 parts of the pitch. For the whole length of the tooth (if wanted in one measurement) set the compasses to the point where the parallel marked 12 meets the line A B, and extend to its point of intersection of the line A d at s, the length is 12 parts of the pitch B d; the working depth is in like manner found from the parallel marked 11; the thickness from that marked 7; and the width of space from that marked 8. The proportions for any other given pitch comprised in the scale are found in precisely the same way, and if the scale be well constructed they may be measured off with the utmost accuracy. To save confusion it is, however, better in practice to insert in the diagram only those parallels, namely, T. U. 12, 11 8.7, which are required; the others are not requisite, and by inattention may lead to error.

The description of the scale as here given supposes that lateral clearance is constantly  $_{15}^{\rm L}$  of the pitch; but as it is commonly desired that this should vary slightly with the pitch relatively increasing as pitch decreases, two other lines, m n and p q, have been introduced into the scale, to enable such modification to be adopted, should it be required. These lines are drawn at such angles as to give a clearance at 6 inches pitch of 1-18th, which is increased at  $\frac{3}{4}$  inch pitch to  $\frac{1}{10}$ . From these lines the thickness and space are to be taken, instead of using the lines marked 7 and 8, setting the compasses in the points of intersection with the pitch lines, and extending perpendicularly to the line k B; in other words, the shortest distance from the point of intersection with the pitch line to the line k B; is the required measure of the space when the line k k is taken, and of

the thickness of tooth when the line m n is taken.

Figure 2 is more complete than the one described, and when well constructed insures, with moderate care, a degree of accuracy and uniformity, in the construction of the various sizes of wheels for which it is employed, that can hardly be otherwise attained. The principle of its construction is in effect the same as that described, but its use is more extended; the diameter of the wheel being found from it simultaneously with the length and thickness of tooth, width of space, and clearances. The scale is adapted to wheels of all the pitches, from 16 inch up to 3 inches.

ed to wheels of all the pitches, from ½ inch up to 3 inches. The mode of construction is this: having drawn the line A D of any convenient length, raise the perpendicular C B to it, also of any convenient length. On the line A D lay off the greatest pitch off the scale from C to A; then from C towards D lay of seven times the pitch once or twice, according to the sizes of wheels of which the scale is intended to be applied. In the scale given, double of seven times the pitch is laid off, namely. 42 inches; then each of these great divisions being subdivided into 11 equal parts, one of these parts will be equal to four teeth upon the radius of the wheel, so that the whole line C D will be divided into 88 radial pitches. Next on the line C B set off the pitches which may be required in the scale, and through these points draw the 24 parallels to A D, terminating in the lines A B and D B. Then each parallel measured from the line B C to its point of termination in B D, is the radius of a wheel of 88 teeth of the particular pitch marked against it on the line A B. They also express the radii of wheels having less than 88 teeth when measured only to the corresponding point in the line joining B, and the divisional on C D, against which the number of teeth is marked. Thus the radius of a wheel of 52 teeth and 17% pitch, is  $r = 15 \sqrt{a}$ inches very nearly.

The scale may also be used when the number of teeth exceeds 88; for example, to find the radius of a wheel having 100 teeth. Thus having found the radius answering to 88 teeth, upon the same parallel take off the measure answering to the difference 100-88=12 teeth; and the two measures are the same parallel take of the measure answering to the difference 100-88=12 teeth; and the two measures are the same parallel take of the measure and the two measures are the same parallel take of the same parallel take of the measure are the same parallel take of the same parallel take of the same parallel take of the measure are the same parallel take of the same parallel

sures together will be the radius required.

To adapt the scale to odd numbers of teeth, the first division on the right of C is divided into single radial pitches, so that the radius of any wheel may be measured off without having recourse to calculation of any kind Thus, for example, if the wheel is intended to contain 50 teeth, the compasses being extended from 52 to the intersection of the parallel answering to the particular pitch to where it meets the line joining Q and B, will give the radius required, that is, a radius answering to 52–2=50 teeth; and any other number of teeth when not marked against the base may be found in the same way.

For the proportions of the teeth, set off  $C = \frac{7}{10}$  of the pitch, then will  $A = \frac{3}{10}$  of the pitch, which corresponds to

the depth from the point of the tooth to the pitch line. Again, set off C b=7th of the 3 inch pitch, and  $\frac{8}{5}$  on the parallel against the 1 inch pitch, this will be the thickness of the tooth, allowing from a fifteenth for clearance on the largest pitch, to a tenth on those from  $\frac{1}{5}$ 8 inch and under; and A b will be the width of space, including the clearance. Lines being drawn from those points to B com-

plete the diagram.

To use the scale, lay off the addendum of the tooth; that is, length beyond the pitch line, equal to A  $a = \frac{3}{15}$  pitch, and the same length marked off within the pitch line will give the whole working depth of the tooth, namely,  $\frac{9}{15}$  pitch. Then with the measure  $C a = \frac{7}{15}$  pitch in the compasses, mark off the whole length of the tooth, and this will allow  $\frac{1}{15}$  at the bottom for clearance. Again, set off the thickness of toothe C b, and the space A b which will contain the clearance for the particular pitch, varying from  $\frac{1}{15}$  to fully  $\frac{1}{15}$  on the small pitches.

The amount of bottom clearance is here presumed to be

The amount of bottom clearance is here presumed to be uniformly  $\tau_0$  of the pitch; but if it be thought advisable to make this vary as in the case of the lateral clearance, it will then be necessary to insert a third line c B in the scale, and so related to a B that the space a c shall be throughout equal to the depth of tooth from the pitch circle to the root, and giving any bottom clearance that may be desired.

Table of Diametral Pitch, with its Equivalent Circular
Pitch Opposite on the Adjoining Column.

Diametral	Circular	Diametral	Circular	Circular	Diametral	Circular	Diametral
Pitch.	Pitch.	Pitch.	Pitch.	Pitch.	Pitch.	Pitch.	Pitch.
2 2 1 2 1 2 2 3 3 4 5 6 7 8 9	1.57 1.39 1.25 1.14 1.05 .898 .785 .628 .524 .448 .392 .35 .314	11 12 14 16 18 20 22 24 26 28 30 32	.280 .262 .224 .196 .174 .157 .143 .130 .120 .112 .104 .098	134 in. 11/2 ii 11/2 i	1.79 2.09 2.18 2.28 2.39 2.51 2.65 2.79 2.96 3.14 3.35 3.59 3.86	3 in. 11 15 5 16 17 18 18 18 18 18 18 18 18	4.19 4.57 5.03 5.58 6.28 7.18 8.38 10.06 12.56 16.75 25.12 50.24

#### SIMPLE RULES ON GEARING.

The following rules will apply to both Bevel and Spur Gears. When the term "pitch" is used it always signifies diametral (not circular) pitch.

For illustrations we will use gears having 64 teeth and 8

pitch.

To FIND PITCH DIAMETER:—Divide the number of teeth by the pitch: 64+8=8 in. p. diam.

To FIND No. OF TEETH:-Multiply the pitch diam, by the

pitch: 8 in. ×8=64, No. of teeth.

To Find The Pitch:—Divide the number of teeth by the

pitch diam. 64+8 in. =8, pitch.

TO FIND OUTSIDE DIAM. OF SPUR WHEELS:-Add 2 to the number of teeth and divide by the pitch:  $64+2=66 \div 8=814$ in, o, d,

To FIND CIRCULAR PITCH:—Divide the decimal 3.1416 the

diametrical pitch: 3.1416+8=.3927 in.

TO FIND THE DISTANCE BETWEEN THE CENTERS OF TWO SPUR GEARS:—Divide half the sum of the teeth of both gears by the pitch: 64+64=128+2=64+8=8 in. centers.

A simple rule to determine the face of bevel gears is to make them seven times the pitch: 8 pitch bevel will thus

be % in, face.

The following table gives the breadth of teeth for transmitting with safety, different powers at various speeds, under ordinary circumstances; the width being  $2\frac{1}{10}$  times the pitch; for increasing the wear, however, in practice. with coarse pitch, the breadth is usually three or four times the pitch.

	rock-	p g	dth th.	e whee		e pitch		
Pitch.	Thick- ness of Teeth.	Length of Teeth	Breadtl of Teeth.	3 ft. per sec.	4 ft. per sec.	5 ft. per sec.	7 ft. per sec.	11 ft. per sec.
Ins.	Ins.	Ins.	Ins.	H.P.	H.P.	H.P.	H.P.	H.P.
4	1.9	2.8	8.5	19	251	32	45	701
$egin{array}{c} 4 \\ 3^{12} \\ 2 \\ 2^{12} \\ 1^{14} \\ 1^{14} \\ 1^{18} \\ \end{array}$	1.6	2.45	7.3	143	19į	241	34 <sub>4</sub> 25	54
3~	1.4	2.1	6.3	112	141	18	25	391
$2\frac{1}{2}$	1.4 1.2 0.95	1.75	5.2	74	10	12½ 8 6¼	171	$ \begin{array}{c c} 39\frac{1}{2} \\ 27\frac{1}{2} \end{array} $
$2^{}$	0.95	1.4	4.2	$7\frac{1}{2}$ $4\frac{3}{4}$ $2\frac{3}{4}$ $2$	61	8~	11	171
13	0.83	1.22	3.6	3į	5	61	81	131
1 <u>i</u>	0.71	1.05	3.1	$2\frac{3}{4}$	31/2	$egin{array}{c} 4rac{1}{2} \ 3rac{1}{2} \ 2rac{1}{2} \ 2 \end{array}$	$6^{\bar{1}}_4$	10 -
11	0.59	0.87	2.6	2	$2\frac{7}{2}$	31	45 31 24 25	64
1 į	0.53	0.79	2.3	1½ 1½	21	$2\frac{1}{2}$	31	51
1	0.48	0.7	2.1	11	13	2	$2\frac{4}{5}$	42
7 8	0.41	0.61	1.82	1	12	13	$2\frac{1}{2}$	$3\frac{3}{5}$
34	0.36	0.52	1.57	7 10	10	11	11/2	$2\frac{1}{2}$
78345812	0.33	0.43	1.31	1 2	614 5 3212143525 9155 255	34	1	$\begin{array}{c} 5\frac{1}{2} \\ 4\frac{2}{5} \\ 3\frac{4}{5} \\ 2\frac{1}{2} \\ 1\frac{7}{10} \end{array}$
1 2	0.24	0.35	1.05	$\frac{7}{10}$ $\frac{1}{2}$ $\frac{3}{10}$	2 5	118 34 12	7 10	1,10

#### TABLE FOR CUTTING SCREWS BY LATHE.

No. of Te'th	Number of Teeth.	Number of Teeth.	Number of Teeth.
No. of threads per in. of screw.  Mandrel-Pinion.  Leading screw wheel.	No. of threads per in. of screw.  Mandrel-Pinion. Stud-Wheel. Stud-Pinion. Leading screw wheel.	No. of threads per in. of screw  Mandrel-Pinion.  Stud-Wheel.  Stud-Pinion.  Leading screw wheel.	No. of threads per in. of Mandrel-Pinion. Stud-Wheel. Stud-Pinion. Leading screw wheel.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	28~  75 140 20 150	32   30   80   20   120   33   40   110   20   120   34   30   85   20   120   35   60   140   20   150   36   30   90   20   120   38   30   95   20   120   38   40   120   20   130   44   30   110   20   150   44   30   110   20   150   445   30   90   20   150   451   40   130   20   140   502   35   30   100   20   150   523   40   140   20   150   523   40   140   20   150   556   30   110   20   150   556   30   120   20   140   60   30   120   20   150   65   30   130   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   20   140   20   150   70   70   70   70   70   70   70

The foregoing table shows the train of wheels to be used in cutting screws varying in pitch from 1 to 70 threads to the inch; the leading or guide screw is supposed to have two threads per inch, yet may the table be still employed when the leading screw has four threads to the inch, for the same train of wheels would sult for cutting screws of double fineness; and similarly when the leading screw has only 1 thread to the inch, a screw of only one-half the fineness will be produced with any train given in the table.

#### RULE for GEARING UP ENGINE LATHES for SCREW CUTTING.

Read from the lathe index the number of threads per inch cut by equal gears and multiply it by any number that will give for a product a gear on the index; put this gear upon the stud, then multiply the number of threads per inch to be cut by the same number and put the resulting gear upon the screw.

Example.—To cut 111/2 threads per inch, We find on the index that 48 into 48 cuts 6 threads per inch, then

 $6\times4=24$ , gear on stud, and  $111/9\times4=46$ , " " screw.

Any multiplier may be used so long as the products include gears that belong with the lathe. For instance, instead of 4 as a multiplier we may use 6.

Thus  $6\times6=36$ , gear upon stud, and  $111/9\times6=69$ . "screw,

### TABLE giving the proportions of the U. S. or SELLERS, STANDARD threads for screws, nuts and bolts.

Charles and control control and control									
Out Side Diam, of Screw in Inches,	Number of Threads per Inch.	Diam. of Screw at the Root of the Thread in Dec. of an Inch.	Width of Top and Bottom Thread in Dec. of an Inch.	Out Side Diam, of Screw in Inches,	Number of Threads per Inch.	Diam. of Screw at the Root of the Thread in Dec. of an. Inch.	Width of Top and Bottom Thread in Dec. of an Inch.		
1.4 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	20 18 16 14 13 12 11 10 9 8 7 7 6 6 5 5 5	.185 .24 .294 .344 .344 .4 .507 .62 .731 .837 .94 1.065 1.16 1.289 1.389 1.491	.0062 .0074 .0078 .0089 .0096 .0104 .0113 .0126 .0138 .0156 .0178 .0208 .0208 .0208 .0227 .025	2 2 2 2 2 3 5 5 5 5 5 4 4 4 4 15 5 5 5 5 6	444493333322222222222222222222222222222	1.712 1.962 2.176 2.426 2.629 2.879 3.1 3.317 3.567 3.798 4.028 4.256 4.48 4.753 5.203 5.423	.0277 .0277 .0312 .0312 .0357 .0357 .0357 .0413 .0413 .0435 .0476 .05 .05 .05 .05 .05 .05 .05 .05 .05 .05		

TABLE showing the number of THREADS to the inch for each diameter of SCREW bolts and SCREW taps.

(English Standard.)
Screw bolts. Se Screw taps. Thre'ds to the Inch. Thre'ds Diam. in Ins. V-Threads. Sq. Taper T's. to the Inch. in Ins. T'ds Diam. to In. in Ins. Diam. T'ds in Ins. to In. 16 22234 141 18 16 14 12 11 11 10 10 9 9 8 8 7 7 6 6 5 5 99877776666654433222 56 13876 15811341178111 456 1 18143812583478 1 12583478 

	Proportions of Flange and Solid nail-lap Couplings.											
	Flange.								$H\epsilon$	alf- $L$	ap.	
Diam. of Shaft.	Diameter of Flange.	Thickness of Flange.	Diam. of Boss.	Depth of Boss.	No. of Bolts.	Diam. of Bolt.	Diam. of Circle of Bolts.	Diam. of Shaft.	T'ck's of Metal.	D. of Coupling.	Length of Coup.	Length of Lap.
Ins	Ins	Ins	Ins		Ins	Ins			Ins	Ins	Ins	Ins
1 1 <sup>1</sup> / <sub>2</sub> 2 2 <sup>1</sup> / <sub>2</sub> 3 3 <sup>1</sup> / <sub>2</sub> 4 4 <sup>1</sup> / <sub>2</sub> 5	$\begin{array}{c} 5 \\ 6\frac{1}{2} \\ 8 \\ 9\frac{1}{2} \\ 11 \\ 12\frac{1}{2} \\ 14 \\ 15\frac{1}{2} \\ 17 \\ 20 \\ \end{array}$	347.8 16 113.6 13.1 125.6 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5	21414 3414 51414 6718 87834 112	2 2 2 3 3 4 4 4 5 5 6 7	3 3 4 4 4 6 6 6 6	111111111111111111111111111111111111111	3½ 4¼ 6 7¼ 8½ 9¾ 11 12½ 13½ 16	$\begin{vmatrix} 1 \\ 1^{\frac{1}{2}} \\ 2 \\ 2^{\frac{1}{2}} \\ 3 \\ 4 \\ 4^{\frac{1}{2}} \\ 5 \end{vmatrix}$	$\begin{array}{c} 1 \\ 1^{\frac{1}{2}34} \\ 2^{\frac{1}{2}38} \\ 2^{\frac{1}{2}5834} \\ 2^{\frac{1}{2}4} \end{array}$	3 4½1 5½2 7¼4 9 9 10½	544 634 814 934 1076 1288 1312 1458 1534	1 13834 2181278 2278 34458 4

11 13 13 Flange Couplings are a common and useful kind for small and medium shafts, up to about 6 in. diameter.

Solid Couplings are perhaps the best of all for small shafts up to, say, 41/2 or 5 inches diameter, for large shafts they become clumsy and heavy.

TABLE of the DIAMETERS and CIRCUMFERENCES of angle iron hoops, with angles inside and outside.

From 6 inch to 6 feet diameter.

Diam- eter.	Angle Outward Circum- ference.	Angle Inward Circum- ference.	ircum-   Diam-   Outward		Angle Inward Circum- ference.
Ft. in. 0 6 0 7 0 8 0 9 0 10 0 11 1 1 1 1 1 1 1 1 1 1 1 1 1	Ft. in. 151-151-152-151-152-151-152-151-152-151-152-151-152-151-152-152	Ft. in. 1 11 13 2 64 4 4 10 5 5 8 12 7 7 7 5 8 8	Ft. in. 4567890110369036903690	Ft. in. 6 10 1 7 6 6 8 8 8 6 6 6 10 1 7 7 8 8 8 9 9 6 4 10 3 7 7 9 11 11 2 5 6 6 6 6 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ft. in. 34 14 14 14 15 16 16 17 11 14 14 16 14 17 17 11 14 14 15 16 17 17 17 18 18 18 14 15 16 17 17 18 18 18 14 19 18 14 15 16 17 17 18 18 18 14 18 18 18 14 18 18 18 18 18 18 18 18 18 18 18 18 18

In the Table of Angle Outwards, the breadth or thickness of the Angle Iron must be added to the circumference; thus—suppose you require to form a ring of 2 inch Angle Iron, 1 ft. 6 in. inside diameter add 2 in. to the diameter=1 ft. 8 in. and you will find the circumference or length of Iron to be 4 ft. 115% in.

In the Table of Angle Inwards, the above rule is reversed, and the breadth or thickness of Iron must be subtracted from the outside diameter; thus—required a ring of 3 in. Angle Iron 2 ft. outside diameter, subtract 3 in. from the diameter=1 ft. 9 in. and you will find the circumference or length of Iron to be 5 ft. 1178 in.

Table showing the proper thickness for Steam-Cylinders, from 6 to 90 inches in diameter.

Diam. of	Thick-	Diam. of	Thick-	Diam. of	Thick-	Diam. of	Thick-
Cylinder.	ness.	Cylinder.	ness.	Cylinder.	ness.	Cylinder.	ness,
Ins. 6 8 10 12 14 16 18 20 22 24 26	Ins44 .545 .65 .755 .86 .965 1.07 1.175 1.28 1.385 1.49	Ins.  28  30  32  34  36  38  40  42  44  46  48	Ins. 1.595 1.7 1.805 1.91 2.015 2.12 2.225 2.33 2.435 2.54 2.645	1ns. 50 52 54 56 58 60 62 64 66 68 70	Ins. 2.75 2.855 2.96 3.065 3.17 3.275 3.38 3.485 3.59 3.695 3.8	72 74 76 78 80 82 84 86 88 90	Ins. 3.905 4.01 4.115 4.22 4.325 4.43 4.535 4.64 4.745 4.85

#### PROPORTIONS OF PLUMMER-BLOCKS.

Diam. of Bearing.	Length of Bearing.	Height to Center.	Length of Sole.	Center of Hold- down b'lt.	Diam. of Bolts.	Size of Holes for Bolts.
Ins. 11 2 21 3 31 4 41 5 6 7 8 9 10 11 12	Ins.  2\frac{1}{2} 3 4 4\frac{1}{2} 5 4 7 6 10 11 12 13	Ins. 21.434 16.24 16.24 16.24 16.24 16.24 16.24 16.24 16.24 11.2	Ft. In. 0 9 101 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ft. In. 0 7 0 8 9 1 0 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Inches	In.   In.

Proportions of Sunk Keys for Wheels and Pulleys.

Diam. of shaft in Ins.	1	2	3	4	5	6
Breadth of key.	3/8	5/8	7/8 .43	11/8	13/8	15/8
Thickness of key. Depth sunk in shaft.	.25	.125	.15	.175	.61	.225
Depth sunk in wheel.	1.15	.215	.28	.345	.41	.485
Diam. of shaft in Ins.	7	8	9	10	11	12
Breadth of key.	17/8	21/8	23/8	25/8	1 27/8	31/8
Thickness of key.	.80		.98	1.07	1.16	1.25
Depth sunk in shaft.	.25	.275	.30	.325	.35	.375
Depth sunk in wheel.	.55	.615	68	.745	.81	.875

The depth sunk in the shaft and in the wheel is measured at the side of the key, and not at its center.

The thickness of Metal round the Eye of Pulleys.

th hip		Diameter of Shaft in Inches.									
iar Per Per	1	2	3	4	5	6					
₩ Page		Thickn	ess roun	d eye in	inches.						
1 2 3 4 5 6 7 8 9	1 3	1 11:014:38 12:2	116 14 996 12 15 16 17 16 17 16 17 16 17 16 17 16 17 16 17 17 17 17 17 17 17 17 17 17 17 17 17	$egin{array}{c} 1_{\frac{36}{15}83478} \ 1_{\frac{16}{15}14} \ 2_{\frac{16}{15}14} \ 2_{14} \ \end{array}$	11255 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	158 124 178 24 24 25 24 26 27 26 27 26 27					

Table of the greatest admissible distances between the bearings of continuous shafts, subject to no transverse strain except from their own weights.

Diam. of shaft in Ins.	Distance bearings	between s in feet.	Diam.	Distance between bearings in feet.			
	Wrought iron.	Steel.	in Ins.	Wrought iron.	Steel.		
1 2 3 4 5 6	12.27 15.46 17.70 19.48 20.99 22.30	12.61 15.89 18.19 20.02 21.57 22.92	7 8 9 10 11 12	23.43 24.55 25.53 26.44 27.30 28.10	24.13 25.23 26.24 27.18 28.05 28.88		

# AVERAGE CUTTER SPEED AND FEED ON SOFT CAST IRON SURFACES.

The figures are adapted to calculations in milling upon soft cast-iron surfaces, and are subject to change to accompany variations in condition and character of work. order to figure accurately upon milling work, the speed of cutter and amount of feed per revolution must be observed -that known, the computation is simple, as follows: Multiply the number of revolutions of cutter per minute by the length of feed at one revolution and the product is inches per minute that can be milled. Allowing about 40 ft. per minute for surface speed of cutter, a 1/2 inch cutter should run at 300 revolutions per minute, with a feed of 1-150 of an inch to a revolution, giving a result of 2 ins. of light milling per minute. An inch cutter would make 150 revolutions per minute, with a feed of 1-100 of an inch on a moderately heavy cut, allowing 11/2 inches of milling per minute. A 3 inch cutter would run 50 revolutions per minute, with a feed of 1-50 of an inch on heavy work, giving a result of 1 inch of milling per minute. The above are examples selected from observed results in practical shop usage.

The following table of metallic baths is given in PARKES CHEMICAL ESSAYS.

No.	Edge tools to be tempered in the various baths.	Compose of the back.	aths.	Tem. Far.
1	Lancets, in a bath composed of	7	4	420°
$\frac{1}{2}$	Other Surgical Instruments.	$\frac{7_{\frac{1}{2}}}{8}$	4	430°
3	Razors, &c.,	8	4	442°
4	Pen knives and some imple-			
	ments of Surgery.	81	4	450°
5 6	Larger pen knives, scalpels &c,	10	4	470°
6	Scissors, shears, garden hoes,			
	cold chisels, &c.	14	4	490°
7	Axes, firmer chisels, plane			-
	irons, pocket knives, &c.	19	4	509°
8	Table knives, large shears, &c.	30	4	530°
$\frac{8}{9}$	Swords, watch springs, &c.	48	4	550°
10	Large springs, daggers, augers,			
	small fine saws, &c.	50	2	558°
11	Pit saws, hand saws, and some	Boilin	ng	1
	particular springs.	Linseed	d oil.	600°
12	Articles which we require to be	Melting		
	still somwhat softer.	Lead.		612°

#### TEMPERING STEEL.

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taps.
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s, &c.
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#### TEMPERING RECIPES.

CASE-HARDENING with PRUSSIATE of POTASH.—Heat the articles after polishing to a bright red, rub the surface over with the prussiate of potash, allow it to cool to a dull red, and immerse it in water.

CASE-HARDENING MIXTURES.—Three parts of prussiate of potash to one part of sal-ammoniac, mixed, or two parts of sal-ammoniac, two parts of bone dust, and one part of prussiate of potash.

Case-Hardening.—Place horn, hoof, bone-dust, or shreds of leather, together with the article to be case-hardened, in an iron box subject to a blood-red heat, then immerse the article in cold water.

TEMPERING BORING INSTRUMENTS.—Heat the tool to a blood-red heat; hammer it until it is nearly cold; reheat it to a blood-red heat, and plunge it into a mixture of 2 ozs. each of vitriol, soda, sal-ammoniae and spirits of nitre, 1 oz. of oil of vitriol, 1/2 oz. of saltpeter, and 3 gallons of water, retaining it there until it is cold.

To Give Iron A Temper To Cut Porphyry.—Make your iron red-hot, and plunge it into distilled water from nettles, and acanthus, or in the very juice pounded out from these plants.

TEMPERING BATHS FOR STEEL.—Twenty gallons of spermaceti oil; 20 lbs. beef suet rendered; 1 gallon of neatsfoot oil; 1 lb of pitch; 3 lbs. black resin.

These two last articles must be previously melted together, and then added to the other ingredients; when the whole must be heated in a proper iron vessel, with a close cover fitted to it, until the moisture is entirely evaporated, and the composition will take fire on a flaming body being presented to its surface, but which must be instantly extinguished again by putting on the cover of the vessel.

This recipe will only last for a few weeks constant use.

For Saws &c.—The composition is 2 lbs. suet, and a 14 lb, of beeswax to every gallon of whale-oil, these are boiled together, and will serve for thin works and most kinds of steel. The addition of black resin, to the extent of about 1 lb; to the gallon, makes it serve for thicker pieces and for those that refused to harden before; but the resin should be added with judgment, or works will become too hard and brittle. The composition is useless when it has been constantly employed for about a month; the period depends, however, on the extent to which it is used, and the, trough should be thoroughly cleaned out before new mixture is placed in it.

### Practical Thickness in Decimals of an Inch of Good Plate Iron in Steam-Boilers, Single Riveted.

P—Steam pressure in pounds per square inch above atmosphere.

				pieci c.	•						
70	DIAMETER of Boiler in Inches.										
<i>P</i> .	10 15	20 25	30 35	40 50	60 70	80	90	100	120	150	
10	1.10  .10	.11 .11 .	12 .12	.13 .13	1.14 .14	1.15	.15	.15	.16	.17	
15	10 .10	.11 .12 .	13 .13	.13 .14	.15 .15	.16	.18	.19	.19	.22	
20	.11  .11				.16 .17		.20	.20	.22	.26	
25		.12 .13 .					.22	.23	.25	,30	
30		.13 .14 .					.24	.25	.28	.33	
40		,14 .15 .					.28	.30	.34	.40	
50		.15 .16 .					.33	.35	.40	.47	
60	.14   .14	.16 .17 .					.37	.40	.46	.55	
70	.14 .15						.42	.45	.52	.60	
80		.18 .20 .					.46	.50	.58	.70	
90	.15  .17			.28 .32			.50	.55	.60	.77	
100		.20 .22 .					.55	.60	.70	.85	
120	.16  .19				.46 .52		.60	.70		1.00	
150	.17  .22				.55 .60		.77			1.20	
200	.20  .25	.30 .35 .	40 .45	.50 .60	.70 .80	.90	1.00	1.10	1.30	1.60	

#### Facts for Boiler Makers.

Rankine's Riveting Rules.—Diameter of Rivet for Plates less than 1/2' thick to be equal to twice the thickness of the plate. For plates 1/2" and upwards 11/2 times thickness of plate. The length of rivet iron required to make the "head" equals 21/2 times the diameter of the rivet.

Boiler Maker's Rule.—In addition to the thickness of the plates the following allowance is made for the head, both giving the whole length of rivets.

RIVET.	COLD RIVETED.	HOT RIVETED
3/8 inch.	5/8 inch.	200,000
1/2 '' 5/6 ''	34 ··	78 inch.
3,4	70	11/8 "

For boilers the rivets are 134 inch from center to center in single riveting, and 2 inches in double riveting; flues the same.

To have a tight fit in the sections for a boiler or other tubular work, make the inside diameter of the inside tube equal to the Inside diameter of the outside tube, less 6 times the thickness of the iron.

Fairbairn's Table of Dimensions of Rivets for Boilers.

Thick.of Plate in Inches.	Diam. of Rivet in Ins.	Length of Rivet to head in Ins.	Pitch in inches.	Lap in single Joints in Ins.	double	of Head
이 아무 사람이 나오면 나오면 하는데 하는데 아니다.	381225834117811 118	75 125 125 214 2234 314	114 1258 1258 214 22534 3	$egin{array}{c} 1_{4} \\ 1_{278} \\ 2_{1416234} \\ 2_{24} \\ 2_{3} \\ 3_{14} \\ \end{array}$	21-18-18-18-18-18-18-18-18-18-18-18-18-18	1215933475514355134 1135534 1135534

#### Lloyd's Rule for Shipbuilding.

Diam of Rivets.	5/8"		34"			7/8"			1"			
Thick- ness of Plates:	5 16	" 6 16	" 7 16	, 8 16	9 16	" 10 16	" 11 16	" 12 16	" 13 16	" 14 16	" 1 <u>5</u> 16	1

Rivets to be 1/4" larger in diameter in the stem stern post, and keel.

Boiler pressure allowed as per Government Rule—Diameter of Boiler in inches.

Example.—Pressure allowed for Boiler 8 feet diameter, 3-8 iron,  $8\times12=96\div6.930=72.18$  pounds.

Table showing the Diminution of Iron Boiler-Plates at High Temperatures; the maxim Tenacity being at 550°=65.000 lbs. per square inch.

Iron Boilers.

Table showing the Diminution of strength of Copper Boiler-Plates by addition to the Temperature the cohesion at 32° being 32.800 lbs. per square inch.

Conner Roilers

	1ron B	ouers.		Copper Botters,						
Temp. obser- ved.	Dim. of Tenac'y obser'd.			Temp. above 32°	Dim- inu- tion.	Tem. above 32°	Dim- inu- tion.			
550° 570° 596° 600° 630° 662° 722° 732° 734° 766°	.0000 .0869 .0899 .0964 .1046 .1155 .1436 .1491 .1535 .1589 .1627	824° 932° 947° 1030° 1111° 1115° 1159° 1237° 1245° 1317°	.2010 .3324 .3593 .4478 .5514 .6000 .6011 .6352 .6622 .6715	90° 180° 270° 360° 450° 460° 513° 529°	.0175 .054 .0926 .1513 .2046 .2133 .2446 .2558	660° 769° 812° 880° 984° 1000° 1200° 1300°	.3425 .4398 .4944 .5581 .6691 .6741 .8861 1.0000			

Table Given Horse-Power of Boilers the Following Sizes: at 60 lbs. Pressure.

sui llaus .msid   2222226000000000000000000000000000000	Length shell.ft.	Num. Tubes.	Length Tubes. Feet.	Diam. Tubes. Inches.	Heating surface Square Ft.	Horse-Power.	Diam. shell Ins.	tj.lleus that shell.ft.	Num. Tubes.	Length Tubes. Feet.	Diam. Tubes. Inches.	Heating surface Square Ft.	Horse-Power.
72	18 16 16	70 90 112	18 16 16 15 18 17 16 16 15 14 13 18 17 16	4 25 35 35 35 35 35 35 35 35 35 35 35 35 35	$\begin{vmatrix} 1502 \\ 1472 \end{vmatrix}$	100	54	12	60 40	12	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	624 683	41
72	16	90	16	$\frac{31}{2}$	1472	98 99 93 80 76 72 72	48 48 48 48 48 48 42 42 42 42 42 42 42 42 42	16	40	16	31/2	683	46
72	15	$\frac{112}{112}$	15	5	1596 1400 1200	99	48	15	49	16	3	684 642	46
60	10	65	19	21	1900	80	40	10	49 49	15 14	3	600	43
60	18 17	65 65 65 80 80 80	17	21	1148	76	48	19	40	12	9	555	40 37 34 36 33 34 32 30 27 26 24 22
60	16	65	16	31	1075	72	48	12	49 49 65	13 12	3	513	34
60	16	80	16	32	1088	72	48	iī	65	îĩ	21	542	36
60	15	80	15	3	1020	68	48	10	65	10	$\frac{51}{2}$	495	33
60	14	80	14	ă	952	68 63 59 63 60 53 55 52	42	15	38	15	32	508	34
60	13	80	13	Ĭ š	884	59	$\overline{42}$	14	38 38	14	3	476	32
54	18	50	18	31	951	63	42	13	38	13	3	441	30
54	17	50	17	31	900	60	42	12	38 38	12	3	408	27
54	16	50	16	3 3	795	53	42	11	45	11	$2\frac{1}{2}$	390	26
54	16	60	16	3	832	55	42	10	45	10	$2\frac{1}{2}$	355	24
54	15	60	15 14	3	1075 1088 1020 952 884 951 900 795 832 780 728 676	52	42	9	45	9 8 7	$2\frac{1}{2}$	320	22
54	14	60	14	3	728	48	42	8 7	45	8	$2\frac{1}{2}$	285	19 16
54	13	60	13	3	676	45	42	7	45	7	$2\frac{1}{2}$	248 !	16

# ALLOYS and COMPOSITION.

ADDOIS was COMIOSITION.												
Name of Metal.	Copper.	Zinc.	Tin.	Nickel.	Lead.	Antimony.	Bismuth.	Silver.	Cobalt of Iron.			
Argentan.		24.	1	21.	1	1	1_					
Argentiferous.	50.	2.5		40.	2.5		Iror	i. 2.5				
Babbitts Metal.	3.7	l	89.			7.3						
Brass Common.			10.5			1						
66 66	75.	25.			i i							
Engine			0 =									
bearings.		1.8	6.5		1							
maiu.	79.3	6.4	14.3			1						
TOC III UVE		0.5	_		-	1		_				
bearings.	50.	2.5	5.		5.							
main icai	000											
Instrum'ts		00	7.8		1		l					
FIHCHDECK		20.			1			1				
Tr. TOHINGO	88.8	11.2	0.4		i							
nonea.		22.3	3.4	10								
Tutenag.	50.	31.	0.0	19.								
Tenacious.		2.8	8.3									
W 110019.	90.	80.	10.									
W 11160.	10.		10.									
WIFE.	67.	33	8.									
" Glands. " Yellow.	65.	$\frac{.5}{20.}$	0.									
" Richer.	40. 50.	10.										
moner.		10.			5.							
" Red. Britannia me'l.	10.	10.	25.		υ.	9.5						
when fus'd add			40.			$\frac{2.5}{2.5}$	25.		,			
Box metal.	80.	10.				4.0	40.	Ť				
Bronze, Yellow.	100.8		2.4									
" Red.	130.5	10.0	4.4									
" Alloy.	80.	2.	18.									
" Cymbals.	80.	4.	20.									
" Gun met'l.	90.		10.					1				
66 66	93.		7.									
" Medals.	93.		7.									
" Statuary.	91.4	5.5	1.4		1.7							
Bell metal l'rge.	80.	0.0	20.									
Chinese Silver.	65.1	19.3		13.				2.48	12.			
" w'te cop'er.		25.4		31.6					-4.			
Church Bells.	80.	5.6	10.1	-2.5	4.3		1					
66 6.	69.	0.0	31.									
Clock "	72.		26.5				Iron	. 1.5				
Electrotype m't.			4.		100.	3.						
Flanges to stand												
Brazing.	64.	2.			2.	4						

## Alloys and Composition (Continued).

Name of Metal.	Copper.	Zinc.	Tin.	Nickel.	Lead.	Antimony.	Bismuth.	Iron.
German Silver.	33.3			33.3				
** **	40.4			31.6				2.6
" fine,	49.5	24.	10.4	24.	ĺ			2.5
Gongs, Gun Metal for	81.6		18.4					
Gun Metal for bearings.	90.3	9.7	.3					
House Bells.	77.	3.1	23.					
Lathe Bushes.	80.		20.		-			
Mach'ery b'r'gs.	87.5		12.5					
" " hard.	77.4	7.	15.6					
Metal that ex-							0.0	
pands in co'ling.	00	co			75.	16.7	8.3	
Muntz Metal. Musical Bells.	90. 87.5	60.	12.5					
Nickel-Silver	01.5		12.0					
"com. English	60.	17.8		22.2				
Nickel-S. Paris-								
ian.	66.	13.6		19.3				
Pewter Best.		- 1	86.		00	14.		
Duintin a Ohan			80.		20.			
Printing Char- acters.		1			80,	20.		
Sheathi'g Metal	56.	45.			00,	20.		1
Speculum "	66.	10.	22.		Arse	enic.	12.	
66	50.	21.	29.					
Stereotype Met.			10.		100.	16.		
Tough Br'ss En-								
gine work.	100.	15.	15.					
Tough Brass heavy bearings.	160.	5.	25.					
Telescopic Mir-	100.	υ.	40.					
rors.	66.6		33.4					
Temper	33.4		66.6					
White Metal.	11.	11.	42.6			85.2		
" " hard.	69.8	25.8	4.4					

# Melting points of alloys.

Lead.	Tin.	Bismuth.	Melting Point.
2 parts	3 parts.	5 parts.	212 degrees.
1	4 11	5 - '	246
	1 "	1 "	286 ''
	2 "	- ī "	336 "
2 ''	ā "		334 "

Horse-power which can be safely carried by shafts for prime movers gears, well supported by bearings, and making 100 revolutions per minute. Horse-power which can be safely transmitted by shafts making 100 revolutions per minute, in which the transverse strain, if any, need not be considered.

	111111	ute.		not be considered.						
Diam. in Ins.	Wr'ght Iron.	Steel.	Cast- Iron.	Diam. in Ins.	Wr'ght Iron.	Steel.	Cast- Iron.			
	H. P.	H. P.	H. P.	11	H. P.	H. P.	H. P.			
1.00			0.60	1.20	2.00	3.20				
1.20	1.00	1.60					1.20			
1.25	1.95	3.12	1.17	1.25	3.90	6.24	2.34			
1.50 1.75	3.37	5.39	2.03	1.50	6.74	10.78	4.06			
1.75	5.36	8.58	3.22	1.75	10.72	17.16	6.44			
2.00	8.00	12.80	4.80	2.00	16.00	25.60	9.60			
2.25	11.39	18.22	6.83	2.25	22.78	36.44	13.66			
2.50	15.62	24.99	9.37	2.50	31.24	49.98	18.74			
2.75	20.80	33.28	12.48	2.75	41.60	66.56	24.96			
3.00	27.00	43.20	16.20	3.00	54.00	86.40	32.40			
3.25	34.33	54.93	20.60	3.25	68.56	109.86	41.20			
3.50	42.87	68.59	25.72	3.50	85.74	137.18	51.44			
3.75	52.73	84.37	31.64	3.75	105.46	168.74	63.28			
4.00	64.00	102.40	38.40	4.00	128.00	204.80	76.80			
4.25	76.77	122.83	46.06	4.25	153.54	245.66	92.12			
4.50	91.12	145.79	54.67	4.50	182.24	291.58	109.34			
4.75	107.17	171.47	64.30	4.75	214.34	342.94	128.60			
<b>5</b> .00	125.00	200.00	75.00	5.00	250.00	400.00	150.00			
5.25	144.70	231.52	86.82	5.25	289.40	463.04	173.64			
<b>5.5</b> 0	166.37	266.19	99.82	5.50	332.74	532.38	199.64			
<b>5</b> .75	190.11	304.18	114.06	5.75	380.22	608.36	228.12			
6.00	216.00	345.60	129.60	6.00	432.00	691.20	259.20			
6.25 6.50	244.14	390.62	146.49	6.25	488.28	781.24	292.98			
6.50	274.62	439.39	164.78	6.50	549.24	878.78	329.56			
6 75	307.55	492.08	184.53	6.75	615.10	984.16	369.06			
7.00	343.00	548.80	205.80	7.00	686.00	1097.60	411.60			
7.00 7.25 7.50 7.75	381.08	609.73	228.65	7.25	762.16	1219.46	457.30			
7.50	421.87	674.99	253.13	7.50	843.74	1349.98	506.26			
7.75	465.48	744.77	279.29	7.75	930.96	1489.54	558.58			
8.00	512.00	819.20	307.20	8.00	1024.00	1638.40	614.40			
8.25	561.52	898.43	336.91	8.25	1123.04	1796.86	673.82			
8.50	614.12	982.59	368.47	8.50	1228.24	1965.18	736.94			
8.75	669.92	1071.87	401.95	8.75	1339.84	2143.74	803.90			
9.00	729.00	1166.40	437.40	9.00	1458.00	2332.87	874.80			
9.25	791.45	1266.32	474.87	9.25	1582.90	2532.64	949.74			
9.50	857.37	1371.79	514.43	9.50	1714.74	2743.58	1028.86			
9.75	926.86	1482.98	556.12	9.75	1853.72	2965.96	1112.24			
	1000.00	1600.00	600.00	10.00	2000.00		1200.00			

RULE:—Multiply the power given in the Tables by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

of the DIAMETER Of SHAFTS BEING the FIRST MOVERS. TABLE

105		22.22.22.22.22.22.22.22.22.22.22.22.22.
0		9861846761249 297614
100		646.00000000000000000000000000000000000
95		$\frac{2}{2}$
90		ವವ್ಯಪ್ಪಪ್ಪಪ್ಪಪ್ಪಪ್ಪಕ್ಷಕ್ಕಕ್ಕಪ್ಪಪ್ಪಡ್ಡಿಡ್ಡ ರು ಬಹಗೆದಿದ್ದ ಪಹಗೆದ್ದಿಬ್ಬಹಗಳು
85		44444466666666666666666666666666666666
- 08		23.00.00.00.00.00.00.00.00.00.00.00.00.00
75	ES.	$\frac{2}{2}$
70	INCHES	CONTROL   CONT
65	ï	23.83.83.83.83.83.83.83.83.83.83.83.83.83
09	FTS	272000 147444000000000000000000000000000000
55	SHA	80000000000000000000000000000000000000
09	Jo	ä. w. w. w. 4. 4. 4. 4. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
45	TER	$\frac{1}{100}$ $\frac{1}$
40	DIAMETER	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
35	A	88444444666666666666666666666666666666
30		4001000000 040400000 044444000000000000
75		44446666666666666666666666666666666666
102		4.4.0.0.0.0.0.0.1.5.1.0.0.0.0.0.0.0.0.0.0.0
15		40000000000000000000000000000000000000
-		
10		66.66 66.66
MGI MGI		40000000000000000000000000000000000000

The Diameter of small shafts in mills, &c, will be found by dividing the number by 1.56.

Transmitting Efficiency of Iron shafting at different speeds, as Prime mover or Head shaft carrying Main Driving Pulley or gear well supported by bearings.

#### COLD ROLLED IRON SHAFTING.

of Ins.		Number of Revolutions per Minute.											
Ħ.	60   80   100   125   150   175   200   250   30												
Diam. Shaft. 1	Horse-Power.												
11/2	2.7	3.6	4.5	5.6	6.7	7.9	9.0	11.	13.				
13/4	4.3	5.6	7.1	8.9	10.6	12.4	14.2	18.	21.				
2	6.4	8.5	10.7	13.	16.	19.	21.	26.	21. 32.				
21/4	9.	12.	15.	19.	23.	26.	30.	38.	46.				
21/2	12.	17.	21.	26.	23. 31.	36.	41.	52.	62.				
$\frac{23}{4}$	16.	22	27.	34.	41. 54. 68.	48.	55.	70.	62. 82.				
3	21.	29.	36.	45.	54.	63.	72.	90.	108.				
31/4	27.	36.	45.	57.	68.	80.	91.	114.	136.				
31/2	34.	45.	57.	71.	87.	100.	114.	142.	172.				
334	42.	56.	70.	87.	105.	123.	140.	174.	210.				
4	51.	69.	82.	106.	128.	149.	170.	212.	256.				
41/2	73.	97.	121.	151.	182.	212.	243.	302.	364.				

#### TURNED IRON SHAFTING.

of Ins.		Number of Revolutions per Minute.											
EE:	60	80	100	125	150	175	200	250	300				
Diam. C Shaft. In	Horse-Power.												
13/4	2.6	3.4	4.3	5.4	6.4	7.5	8.6	10.7	12.9				
2	3.8	5.1	6.4	8.	9.6	11.2	12.8	16.	19.2				
21/4	5.4	7.3	8.1	10.	12.	14.	16.	20.	24.				
21/2	7.5	10.	12.5	15.	18.	22.	25.	31.	37.				
23/4	10.	13.	16.	20.	24.	28.	25.	40.	48.				
3	13.	17.	20.	25.	30.	35.	40.	50.	60. 81.				
31/4	16.	22.	27.	34.	40.	22. 28. 35. 47.	<b>54.</b>	67.	81.				
31/2	20. 25. 30.	27.	34.	42.	51.	59.	68.	85.	102.				
$33\bar{4}$	25.	33.	42.	52.	63.	73.	84.	105.	126.				
4	30.	41.	51.	64.	76.	89.	102.	127.	153.				
41/2	43.	58.	72.	90.	108.	126.	144.	180.	216.				
5	60.	80.	100.	125.	150.	175.	200.	250.	300.				

To find the Horse-Power of other speeds not in the table.

RULE.—Multiply the power given in the 100 revolutions column, by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

Transmitting Efficiency of Iron shafting at different speeds, as Second movers of Line shafting, Bearings 8 feet apart.

#### COLD ROLLED IRON SHAFTING.

	1												
of Ims.		Number of Revolutions per Minute.											
= -	100	100   125   150   175   200   225   250   300   350											
E #	100	140	1 100	110	200	440	400	300	1 390				
Diam. Shaft.	Horse-Power.												
11/2	6.7	8.4	10.1	11.8	13.5	15.2	16.8	20.	23.				
15/8	8.6	10.7	12.8	15.	17.1	19.3	21.5	26.	31.				
134 178	10.7	13.4	16.	18.7	21.5	24.2	26.8	32.	39.				
178	13.2	16.5	19.7	23.	26.4	29.6	32.9	39.	46.				
2	16.	20.	24.	28.	32.	36.	40.	48.	56.				
21/8	19.	24.	29. 34.	33. 39.	38.	43.	48.	57.	67.				
$\frac{214}{238}$	22.	28.	34.	39.	45.	50.	56.	68.	80.				
238	27.	33.	40.	47.	53.	60.	67.	70.	94.				
$\frac{21/2}{23/4}$	31.	39.	47.	54.	62.	69.	78.	93.	109.				
23/4	41.	52.	62.	73.	83.	93.	104.	125.	145.				
3	54.	67.	81.	94.	108.	121.	134.	162.	189.				
31/4	68.	86.	103.	120.	137.	154.	172.	205.	240.				

#### TURNED IRON SHAFTING.

of Ins.		Number of Revolutions per Minute.											
ij±:	100	125	150	175	200	225	250	300	350				
Diam. Shaft. 1	Horse-Power.												
134 178	6.	7.4	8.9	10.4	11.9	13.4	14.9	17.9					
17/8	7.3	9.1	10.9	12.7	14.5	16.3	18.2	21.8					
2	8.9	11.1	13.3	15.5	17.7	20.	22.2	26.6	31.				
21/8	10.6	13.2	15.9	18.5	21.2	23.8	26.5	31.8	37.				
21/4	12.6	15.8	19.	22.	25.	28.	31.	38.	44.				
23/8	15.	18.	22.	26.	29.	33.	37.	44.	52.				
$21/_{2}$	17.	21.	27.	26. 30. 40.	34.	39.	43.	52.	60.				
$\frac{23\overline{4}}{3}$	23.	29.	34.	40.	25. 29. 34. 46.	28. 33. 39. 52.	58.	69.	81.				
3	30.	37.	45.	52.	60.	67.	75.	90.	105.				
31/4	38.	47.	57.	66.	76.	85.	95.	114.	133.				
31/2	47.	59.	71.	83.	95.	107.	119.	143.	167.				
4	71.	89.	107.	125.	142.	160.	178.	213.	249.				

To find the Horse-Power of other speeds not in the table.

RULE.—Multiply the power given in the 100 revolutions column, by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

Transmitting Efficiency of Iron shafting for simply Transmitting Power and short counters.

#### COLD ROLLED IRON SHAFTING.

of Ins.	Number of Revolutions per Minute.												
Diam.	100   125   150   175   200   267   300   367   400												
Diam Shaft.		Horse-Power.											
11/4	6.5	8.1	9.7	11.3		17.4	19.5						
13/8	8.5 11.2	10.7 14.	12.8 16.8	15. 19.6	17. 22.5	22.7	25.5 33.	31.	34.				
1½ 15/8	14.2	17.7	21.2	24.8	28.4	38	42.	59 59	45. 57.				
134	18.	22.	27.	31.	35.	47.	53.	41. 52. 65.	71.				
134 178	22. 26. 32. 38.	27.	33.	38.	44.	30. 38. 47. 58. 71.	65.	79.	87.				
2	26.	33.	40.	46.	53.	71.	80.	97.	106.				
21/8	32.	40.	<u>47</u> .	55.	63.	84.	95.	116.	127.				
21/4	38.	47.	57.	66.	76.	101.	114.	138.	152.				
23/8	44.	55.	66.	77.	88.	118.	133.	163.	178.				
21/2 23/4	52. 69.	65. 84.	78. 99.	91. 113.	104. 138.	138. 184.	155. 207.	190. 254.	207. 277.				

#### TURNED IRON SHAFTING.

of Ins.	Number of Revolutions per Minute.											
Et.	100	125	150	175	200	267	300	367   400				
Diam. Shaft.	Horse-Power.											
11/2 15/8	6.7	8.4	10.1	11.8	13.5	17.9	20.3	24.8 27.				
15/8	8.6	10.7	12.8	15.	17.1	22.8	25.8	31.5 34.3				
134	10.7	13.4	16.	18.7	21.5	28.	32.	39. 43. 48. 52. 58. 64. 70. 76. 83. 90.				
17/8	13.2 16.	16.5 20.	19.7	20.	26.4	<b>30.</b>	1 49.	48. 52.				
21/8	10.	24.	24.	20.	20	51	40.	48. 52. 58. 64. 70. 76.				
21/8	22.	28.	24. 29. 34.	30.	45	60	60	83. 90.				
236	19. 22. 27.	33.	40.	23. 28. 33. 39. 47.	32. 38. 45. 53.	70	70	96. 105.				
21/2	31.	39.	47.	54.	62.	28. 35. 42. 51. 60. 70.	32. 39. 48. 57. 68. 79. 93.	114. 125.				
21/4 23/8 21/2 23/4	41.	52.	62.	73.	83.	111.	125.	153. 167.				
3	54.	67.	81.	94.	108.	144.	162.	198. 216.				
31/4	68.	86.	103.	120.	137.	182.	205.	250. 273.				

To find the Horse-Power of other speeds not in the table. RULE.—Multiply the power given in the 100 revolutions column, by the number of revolutions made by the shaft per minute; divide the product by 100; the quotient will be the power which can be safely carried.

Table of Horse-Power which may be transmitted by open Single Belts to Pulleys running 100 Revolutions per minute. The diameters of the Driving and Driven Pulley being equal.

Y.			Width	of Be	lt in I	nches.		
Diam. Pulley	2	21/2	3	31/2	4	41/2	5	6
of P				HORSE-	Power.			
Ins. 6 61/2 771/2 8 81/2 91/2 10 11 12 13 14 15	.44 .47 .51 .55 .58 .62 .65 .69 .73 .80 .87 .95	.54 .59 .64 .68 .73 .77 .82 .86 .91 1.00 1.18 1.27	.65 .71 .76 .82 .87 .93 .98 1.04 1.09 1.31 1.41 1.52	.76 .83 .89 .95 1.02 1.08 1.15 1.21 1.27 1.40 1.53 1.65 1.77	.87 .95 1.01 1.09 1.16 1.24 1.31 1.39 1.45 1.60 1.75 1.89	.98 1.07 1.14 1.23 1.31 1.39 1.48 1.56 1.63 1.80 1.97 2.12	1.09 1.19 1.27 1.36 1.45 1.55 1.64 1.74 1.81 2.00 2.18 2.36 2.53 2.73	1.31 1.42 1.53 1.64 1.75 1.86 1.97 2.08 2.18 2.40 2.62 2.83 3.05
15 16 17 18 19 20 21 22 23	1.09 1.16 1.24 1.31 1.39 1.45 1.52 1.60 1.67	1.36 1.45 1.55 1.64 1.73 1.82 1.91 2.00 2.09	1.64 1.74 1.85 1.96 2.07 2.18 2.29 2.40 2.51	1.91 2.03 2.16 2.29 2.42 2.55 2.67 2.80 2.93	2.19 2.32 2.47 2.62 2.76 2.91 3.05 3.20 3.35	2.46 2.61 2.78 2.95 3.11 3.27 3.44 3.60 3.75	2.73   2.91   3.09   3.27   3.45   3.64   3.82   4.18	3.29 3.48 3.70 3.92 4.14 4.36 4.58 4.80 5.02
n. ley.		×	Width	of Be	lt in Ir	ches.		
Diam. of Pulley.	4	5	6	8	10	12	14	16
of				HORSE-	POWER			
Ins. 24 25 26 27 28 29 30 31 32 33 34 35	3.5 3.6 3.8 3.9 4.1 4.2 4.5 4.7 4.8 4.9 5.1	4.4 4.5 4.7 4.9 5.1 5.3 5.4 5.8 6.2 6.4	5.2 5.5 5.7 5.9 6.1 6.3 6.6 6.8 7.2 7.4 7.6	7. 7.3 7.6 7.8 8.1 8.4 8.7 9.3 9.6 9.9 10.2	8.7 9.1 9.5 9.8 10.2 10.5 10.9 11.3 11.6 12. 12.4 12.7	10.5 10.9 11.3 11.8 12.2 12.6 13.1 13.5 14. 14.4 14.8 15.3	12.2 12.7 13.2 13.7 14.3 14.8 15.3 15.8 16.8 17.3 17.9	14. 14.5 15.1 15.6 16.3 16.9 17.4 18. 18.6 19.2 19.8 20.4

Horse-Power of Belts-(Continued).

	1)	ORSE-I	OWER	OF DE	L15-(C	ontinu	ou).				
Diam. Pulley.	,		Width	of Be	lt in Ir	iches.					
Diam Pulle	4	5	6	8	10	12	14	16			
of 1		Horse-Power.									
36 37 38 39 40	5.2 5.4	6.5	7.8 8.1	10.5	13.1 13.5	15.7 16.2	18.3 18.9	20.9 21.5			
38	5.5	6.9	8.3	11	13.8	16.6	19.3	22.1			
39 40	5.7 5.8	7.1 7.3	8.5 8.7	11.3 11.6	14.2 14.7	17. 17.5	19.9 20.4	22.7 23.3			
42	6.1	7.6	9.2	12.2 12.8	15.3	18.2	21.4	24.3			
44 46	6.4	8. 8.4	9.6 10.	13.4	16. 16.7	19.2 20.1	22.4 23.4	25.6 26.8			
48 50	7.	8.8	10.4	14.	17.4 18.2	21.	24.4	28.			
54	7.2 7.8	9. 9.8	10.9 11.8 13.1	14.6 15.6	19.6	21.8 23.6	25.4 26.4	29. 31.2			
60 66	8.8 9.6	10.8 12.	13.1 14.4	17.4 19.2	21.8 24.	26.2 28.8	30.6 33.6	34.8 38.4			
72	10.4	13.	15.6	21.	26.2	31.4	36.6	41.8			
78 84	11.4 12.2	14.2 15.2	17. 19.4	22.6 24.4	28.4 30.6	34. 36.4	39.8 42.8	45.4 48.6			
- ×			Width	of Be	elt in I	nches.		-			
Jiam. Pulley.	18	1 20	22	1 24	1 26	28	30	32			
	10	1 20			POWER		1 00	1 04			
of of		1	1	HURSE-	TOWER						
Ins. 24	16	17	19	21	23	24	26	28			
30 36	19 24	22 26	24 29	26 31	28 34	31 37	33 39	35 42			
38	25	28	30	33	36	39	41	44			
40 42	$\frac{26}{28}$	29 31	32 34	35 36	38	41 43	44 46	47			
44	29 31	32	35	38	42	45	48	51			
48 50	33	35 36	38	42 44	45 47	49 51	52 54	56 58			
54	35 39	39 44	43 48	47 52	50 57	53 61	58 65	62 70			
60 66	43	48	53 58	58	62	67	72	77			
72 78	47 51	52 57	58 62	63 68	68	73 80	78 85	84 91			
84	55	61	67	73	79	86	91	97			
96 120	63 78	70 88	76 96	84 104	90	$\frac{98}{122}$	104 130	112 140			
144	94	104	116	126	136	146	156	168			

The Horse-Power of Double Belts is 10-7 of that given in the Tables.

RULE:--Multiply the power given in the Tables by the number of revolutions made by the pulley per minute; divide the product by 100, the quotient will be the power transmitted.

The following table exhibits the necessary width of belts to transmit different number of Horse-Power.

1.4	Diameter of Pulleys and Drums in feet.								
Horse- Power.	2	3	4	5	6	7	8	9	10
田五			Wid	th of	Belt	in I	nches.		
1 2 2 3 4 4 5 6 6 7 8 9 9 10 2 14 4 16 8 20 25 30 35 40 45 5 5 5 6 6 5 7 7 5 8 8 5	1.8 3.6 5.4 7.2 9.0 10.8 12.6 14.4 16.2 21.6 25.2 28.8 32.4 54.0 63.0 72.0 90.0	1.2 2.4 3.6 4.8 6.0 7.2 8.4 9.0 12.0 11.0 10.8 12.0 41.0 30.0 42.0 48.0 66.0 66.0 66.0 78.0 78.0 78.0 78.0 78.0 78.0 78.0 78	Wid  0.9 1.88 2.7 3.6 4.5 5.4 6.3 7.2 8.1 9.0 10.0 6.2 27.0 31.6 27.0 40.5 54.0 67.5 72.0 67.7 6.0	th of 0.7 1.4 2.1 2.1 2.9 3.6 4.3 5.0 7 5.7 6.4 2.5 12.9 11.5 12.9 11.8 0 33.4 33.9 6 43.2 46.8 55.0 455.0 56.2	Belt 0.6 1.2 2.4 3.0 3.0 4.2 4.8 5.4 6.0 7.2 8.6 10.8 115.0 115.0 121.0 33.0 34.0 34.0 45.0 45.0 45.0	in I 0.5 1.00 2.5 3.00 2.5 3.05 4.1 6.1 7.1 7.1 7.1 7.1 28.2 23.1 7.2 28.2 30.8 33.9 38.5 41.1 4.1 4.1 4.1	nches.  0.45 0.9 1.3 1.8 2.2.7 3.1 6.0 4.0 4.5 6.3 7.2 113.5 15.7 120.2 224.7 27.0 29.2 33.7 36.0 38.2	0.4 0.8 1.2 1.6 2.0 2.4 2.8 3.2 4.0 4.8 5.6 6.4 7.2 2.0 0.0 11.0 0.0 12.0 22.0 24.0 24.0 24.0 24.0 24.0 32.0	0.3 0.7 1.0 1.4 1.8 2.1 2.5 2.8 3.2 3.6 4.3 5.0 5.7 9.0 10.8 12.6 14.4 16.2 18.0 19.8 12.6 19.8 23.4 24.7 25.8 26.8 26.8 27.0 28.0 28.0 28.0 28.0 28.0 28.0 28.0 28
90 95 100			81.0	64.8 68.4 72.0	54.0 57.0 60.0	46.2 48.8 51.4	40.5 42.9 45.0	36.0 38.0 40.0	32.4 34.2 36.0

EXAMPLE.—What should be the width of belt to transmit 14 horse-power from a water wheel, having on its shaft a 5 feet drum. Find 14 in column marked "Horse-Power." opposite this number in the table, in the column 5, marked "Diameter of Pulleys and Drums in feet." will be found 10 inches, which is the required width of belt.

#### REMARKS ON BELTING.

The average thickness of single belts is 3-16 of an inch, andwhen made of good ox-hide, well tanned, their breaking strength, per inch of width, has been determined as follows:

In the solid leather, 675 lbs. At the rivet holes of splices, 362 ... At the lacing holes, 210 ...

The safe working tension is assumed to be 45 lbs. per inch of width, which is equal to a velocity of about 60 square feet per minute per horse-power, which is safe practice for single belts in good condition.

About three-quarters of the trouble experienced in broken pulleys, hot boxes, etc., can be traced to the fault of tight belts.

The smooth side of the belt should run next to the pulley, as it will drive 25 per cent. more than if run with flesh side.

Belts that are dry and slip can be made to adhere more closely by putting on a little neats-foot or castor oil. The first is considered the best to use. Do not put rosm on the belts as it causes them to crack by making them hard.

Where narrow belts are to run over small pulleys. -15 feet is a good average—the belt having a sag of  $1\frac{1}{2}$  to 2 inches.

For larger belts, working on larger pulleys, a distance of 20 to 25 feet, with a sag of 21/2 to 4 inches.

For main belts working on very large pulleys, the distance should be 25 to 30 feet, with a sag of 4 to 5 inches.

### RULES for CALCULATING the SPEED of DRUMS and PULLEYS.

The diameter of the driver being given, to find its number of revolutions.

*Rule:*—Multiply the diameter of the driver by number of its revolutions, and divide the product by the diameter of the driven, the quotient will be the number of revolutions of the driven.

The diameter and revolutions of the driver being given, to find the diameter of the driven that shall make any given number of revolutions in the same time.

Rule:--Multiply the diameter of the driver by its number of revolutions and divide the product by the number of revolutions of the driven; the quotient will be its diameter.

To ascertain the size of the driver.

Rule:—Multiply the diameter of the driven by the number of revolutions you wish to make, and divide the product by the revolutions of the driver; the quotient will be the diameter of the driver.

N. B.—In ordering Pulleys, be careful to give the exact size of the Shaft on which they are to go, also state how you wish them finished on the face; *Flat* face for shifting belt, *Rounding* for non-shifting belt.

The following table shows the velocity of belts; the column marked "Revolution Shaft" shows the number of revolutions which the line or driven shaft is supposed to make per minute; the column marked "Diameter of Drum" shows the diameter of the drum on the line or driven shaft.

olu- Shaft			I	Diamet	er of	Drum			-		
	2	21/2	3	31/2	4	41/2	5	51/2	6		
Rev tion	Number of Feet.										
100	628	785	942	1099	1256	1413	1570	1727	1884		
110	690	863	1036	1208	1381	1554	1727	1899	2072		
120	753	942	1130	1318	1507	1695	1884	2072	2260		
130	816	1020	1224	1428	1632	1836	2041	2245	2449		
140	879	1099	1318	1538	1758	1978	2198	2417	2637		
150	942	1177	1413	1648	1884	2119	2355	2590	2826		
160	1004	1256	1507	1758	2009	2260	2512	2763	3014		
170	1067	1334	1601	1868	2135	2402	2669	2935	3202		
180	1130	1413	1695	1978	2260	2543	2826	3108	3391		
190	1193	1491	1789	2088	2386	2684	2983	3281	3579		
200	1256	1570	1884	2193	2512	2826	3140	3454	3768		

Example 1.—The line shaft is required to make 120 turns per minute, and it is desired to have the belt run 1800 feet per minute; required, the diameter of the driven drum. Find 120 in the column marked "Revolution Shaft;" opposite to this number in the table find 1800 or the nearest to it, which is 1884 feet; over this number in the column marked "Diameter of Drum," will be found 5 feet, the diameter of the drum.

Example 2.—The line shaft makes 100 turns per minute, the diameter of the driven drum is 4 feet; required, the number of feet the belt moves a minute. Find 100 in the column marked "Revolution Shaft," opposite to the number in the table, and under 4 in the column marked "Diameter of Drnm," will be found 1256 feet.

The following table shows the width of the counter-belt that drives the counter-shaft, from which any number of

large size board-planing machines from one to four may be driven. The columns marked "Pulleys," shows the diameter of the smallest of the two pulleys on which the counter-belt runs; the columns marked "No. Machines," shows the number of machines to be driven.

ys.	No. Machines.				SS.	No. Machines.			
Pulleys.	1   2   3   4					1	2	3	4
P		Pulleys	1	elt.					
12 14 16 18 20 22 24	7 1 2 1 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2	$ \begin{vmatrix} 15 \\ 13 \\ 11_{\frac{1}{4}} \\ 10 \\ 9 \\ 8_{\frac{1}{4}} \\ 7_{\frac{1}{2}} \end{vmatrix} $	22½ 19½ 16¾ 15 13¼ 12¼ 11¼	$egin{array}{c} 30 \\ 26 \\ 22rac{1}{2} \\ 20 \\ 18 \\ 16rac{1}{2} \\ 15 \\ \end{array}$	26 28 30 32 34 36	31/31/3 31/4 3	7 6 5 5 5 5 4 5	101 91 9 81 81 71	$ \begin{vmatrix} 13\frac{3}{4} \\ 12\frac{3}{4} \\ 12 \\ 11\frac{1}{4} \\ 10\frac{1}{3} \\ 10 \end{vmatrix} $

EXAMPLE—Required the width of a belt to drive two board-planing machines, the diameter of the smallest pulley being 20 inches. Find 20 in the column marked "Pulley," opposite to this number in the table, and under 2 in the column marked "No. Machines," will be found 9 inches, the required width of a counter-belt that drives a counter-shaft which drives two large size board-planing machines.

Table of Power Transmitted by Wire Ropes.

Diam	No. of	Diam	Rev	olutions	per Minu	ite.
Diam. of wh'el		of	80	100	120	140
in feet.	Rope.	Rope.		Horse-	POWER.	
4	24	287	3.3	4.1	5.0	5.8
5	23 22	7,	6.9	8.6	10.3	12.1
$\frac{6}{7}$	22	15	10.7	13.4	16.1	18.7
7	22	15	16.9	21.1	25.3	29.6
8	21	1	22.0	27.5	33.0	38.5
8	20	76 15 25 13 12 12 58	40.0	41.5	50.0	51.9
10	19	11	55.0	58.4	73.0	82.5
11	18	ii.	64.9	75.5	81.0	97.3
12	17	34	93.4	99.3	116.7	124.1
13	17	3	112.0	140.0	168.0	
14	16	7	141.0	148.0	185.0	
15	16	161634347878	217.0	259.0	300.0	

#### WEIGHTS of MATERIALS.

TABLE Showing Standard Sizes of AMERICAN and ENGLISH WIRE GAUGES In Parts of an Inch.

1	- E %	- = %	1 = 5 %	12 = 21	T	1 = 3	- = zi	= :6	نبعة
No. of Gauge.	Amer'n Gauge ir ecimals	Amer'n Gauge in Tracti'ns.	English rauge in ecimals	English kauge i racti'ns	of se	Amer'n Gauge in Jecimals.	Amer'n Gauge i Tacti'n	Inglish Fauge ii ecimals	Ga'
0.00	e ge El	e e e	1.20 grill	Engli rauge racti	No.	ii ke e	5 g 2	음등	0
28	Amer'l Gauge Jecimal	Amer' Jauge racti'i	Englis Gauge Decima	Englis rauge racti'i	No. o	Amer' Gauge Jecima	Amer'i Gauge Fracti'i	Englist Gauge Jecimal	120
1,-1	<u>, O A</u>	1.0%	<u> </u>	I OH			1	700	因
	Inch	Inch	Inch	Inch	1 '	Inch	Inch	In.	In.
0000	.46	15-32	.454	15-32	18	.0403		.049	
000	.4096	13-32	.425	27-64	19	.0359	T 003	.042	3-64
00	.3648	23-64	.380	3-8	20	.0319	1-32	.035	
0	.3248	21-64	.340	11-32	21	.0284		.032	1-32
1 2 3 4 5 6	.2893	19-64	.300	19-64	22	.0253		.028	
2	.2576	1-4	.284	9-32	23	.0225		.025	
3	.2294	15-61	.259	1-4	24	.0201	7.04	.022	1
4	.2043	13-64	.238	15-16	25	.0179	1-64	.02	1 04
2	.1819	3-16 5-32	.220	13-64	26	.016		.018	1-64
9	.1443	9-64	.180	3-16	27 28	.0126		.016	
8	.1285	1-8	.165	5-32	$\frac{20}{29}$	.0112		.012	
9	.1144	1-0	.148	9-64	30	.012		.012	
10	.1019	7-61	.134	3-01	31	.01		.009	
11	.0907	3-32	.120	1-8	32	.0079		.008	
12	.0808	0.02	.109	7-64	33	.007		.007	
13	.0719	5-64	.095	3-32	34	.0063		.005	
14	.0641	001	.083	0.02	35	.0056		.004	
15	:057		.072	5-64	36	.005			
16	.0508		.065		37				
17	.0452	3-64	.058	1-16	38				

Table showing the thickness and weight of Galvanized Sheet Iron by American gauge,

Wire Gauge.	Thick- ness.	Weight per Sq Foot.	Wire Gauge.	Thick- ness.	Weight per Sq Foot.
No.	Ins.	OZ.	No.	Ins.	OZ.
30	.012	10	22	.0253	21
29	.0112	11	21	.0284	24
28	.0126	12	20	.0319	28
27	.0142	14	19	.0359 -	33
26	.016	15	18	.0403	
25	.0179	16	17	.0452	43.
24	.0201	17	16	.0508	43,
23	.0225	19	14	.0641	60

Table showing weight of Lead Pipe required for a given head (or fall) of water.

					·				
in	ire		Calibre in Inches.						
2:12	ssu sq ch.								
GE3	r se	3/8	1/2	5/8	3/4	1	11/4	11/2	
He tr	Pre per i		We	eight p	per foot in lbs.				
20	10	.38	.63	.87	1.	1 1.5	2.	3.	
20 30	15	.5	.75	1.38	1.5	2.	$\overline{2.5}$	3.5	
40		.68 .75	1.	1.75	2.	2.5	3.	4.	
50 75	20 25 38 50	.75	1.25	2.	2.5	3.	4.	5.	
	38	1.	1.63	2.38	3.38	4.	4. 5. 7.	6.	
100		1.25	2.	3.	4.0	5.		10.	
150	75	1.38	2.5	3.5	4.5	6.	9.	12.	
200	100	1.5	3.	4.	5.	17.	12.	15.	

The above weights of pipe are of sufficient strength to permit the water to be shut off, or stopped. When the water is permitted to run constantly, two-thirds of the above weight will answer,

LEAD PIPE. Weight per lineal foot. (AMERICAN).

de.			Thi	ckness	in In	ches.			
E Sign		7 1 1/ 1 2 1 1/ 1 1/ 1							
Calcula- ed insid Diam.	16	1/8	16	1/4	3/8	1/2	5/8	3/4	
De Sa			We	eight in	Don	nde			
te C	1		***	agne n	1 1001	ius.			
Ins.								1	
3/2	.427	.97	1.65	2.44	4.38				
1/9	.548	1.21	2.01	2.93	5.11	7.79			
- 56	.670	1.46	2.38	3.42	5.85	8.77	12.2		
3/4	.791	1.70	2.74	3.90	6.58	9.75	13.4	17.6	
3/8 1/2 5/8 3/4 7/8	.911	1.95	3.11	4.39	7.31	10.7	14.6	19.1	
1″	1.03	2.19	3.47	4.88	8.04	11.7	15.8	20.5	
114	1.28	2.69	4.21	5.85	9.5	13 7	18.3	23.4	
11/6	1.52	3.18	4.94	6.83	11.	15.6	20.7	26.3	
13/4	1.76	3.67	5.67	7.81	12.4	17.6	23.2	29.3	
274	2.01	4.16	6.40	8.78	13.9	19.5	25.6	29.3 32.2	
214	2.25	4.65	7.13	9.76	15.4	21.5	28.1	35.1	
21/6	2.49	5.14	7.86	10.7	16.8	23.4	30.5	38.0	
23/4	2.73	5.63	8,59	11.7	18.3	25.4	32.9	41.	
11/4 11/2 13/4 2 21/4 21/2 23/4 3 31/2	2.98	6.12	9.32	12.7	19.7	27.3	35.4	43.9	
31/6	3.46	7.10	10.8	14.6	22.7	31.3	40.3	49.7	
4	3.95	8.08	12.2	16.6	25.6	35.2	45.2	55.6	
7	1 0.00	1 0.00	1 12.2	10.0	1 20.0	1 50.2	10.2	00.0	

Joints to lead pipes require 1 lb. of solder for every inch diameter.

## Weight of Lead Pipe. (ENGLISH.)

		Com- mon.	Med- ium.	Strong.
1/2 in. bore w'g't 5/8 " 34 " 11/4 " 11/2 " 13/4 "	per 15 ft. length. " " 12 " " "	lbs. 15 18 24 42 42 50 70 84	lbs. 18 22 32 56 52 72 81 96	lbs. 22 47 42 64 63 84 90 112

WEIGHT and DIMENSIONS of LEADEN BALLS.

Number of balls in a pound from 15-16 ths to .237

of an inch in Diameter.

of an inch in Diame	ter.
Diameter   No.   Diameter   No.   No.	Diameter No.
1.67   1   .57   25	.301   170
1.326 2 .537 30	.295 180
1.157   3   .51   35	.29 190
1.051 4 .505 36	285 200
977 5 3488 40	281 210
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	276 220
.873 7 .453 50	272 230
835 8 366 60	268 240
802 9 3407 70	265 250
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	
	.262 260
.75   11   .388   80	.259 270
.73   12   .375   88	.256 280
.71 13 372 90	.252 290
.693   14   .359   100	.249   300
.677   15    .348   110	.247   310
.662   16   .338   120	.244   320
.65   17   .329   130	.242   330
.637   18   .321   140	.239   340
.625   19   .314   150	.237   350
615 20 307 160	

Thickness and weight per square foot of Window Glass.

	The state of the s										
No.	Thick- ness.	Weight.	No.	Thick- ness.	Weight.						
12 13 15 16 17 19	Ins. .059 .063 .071 .077 .083 .091	oz. 12 13 15 16 17 19	21 24 26 32 36 42	Ins. .1 .111 .125 .154 .167	0z. 21 24 26 32 36 42						

Diameter and number of Pellets in an ounce of shot. (American Standard).

Num- ber.	Diam. in Inches.	Pel lets.	Num- ber.	Diam. in Inches.	Pel- lets.
TT T BBB BB B 1 2	.21 .20 .19 .18 .17 .16 .15 .14	32 38 44 49 58 69 82 98	5 6 7 8 9 10 11 12	.12 .11 .10 .09 .08 .07 .06 .05	149 209 278 375 560 822 982 1778

Table Showing Weight per Foot of Sheet and Bar Brass.

Thickness, or Diameter, or Side, inches.	Sheets, Square foot.	Square Bars, 1 foot long.	Round Bars, 1 foot long.	Thickness, or Diameter, or Side, inches.	Sheets, Square foot.	Square Bars, I foot long,	Round Bars, 1 foot long.
1-16	2.7	.015	.011	1-16	45.95	4.08	3.20
1/8 3-16	5.41	.055	.045	1/8	48.68	4.55	3.57
3-16	8.12	.125	.1	3-16	51.4	5.08	3.97
1/4	10.76	.225	.175	1/4 5-16	54.18	5.65	4.41
5-16	13.48	.350	.275	5-16	56.85	6.22	4.86
3/8	16.25	.51	.395	3/8 7-16	59.55	6.81	5.35
7-16	19.	.69	.54	7-16	62.25	7.45	5.85
1/4 5-16 3/8 7-16 1/2 9-16	21.65	.905	.54 .71 .9	1/2 9-16	65.	8.13	6.37
$9 - \bar{1}6$	24.3	1.15	.9	9-16	67.75	8.83	6.92
5/8	27.12	1.4	1.1	5/8 11-I6	70.35	9.55	7.48
11-16	29.77	1.72	1.35	11-Ĭ6	73.	10.27	8.05
3/4	32.46	2.05	1.06	3/4	75.86	11.	8.65
13-16	35.18	2.4	1.85	13-16	78.55	11.82	9.29
7/8	37.85	2.75	2.15	7/2	81.25	12.68	9.95
15-16	40.55	3.15	2.48	7/8 15-16	84.	13.5	10.58
1	43.29	3.65	2.89	1	86.75	14.35	11.25

Dia		of Rou Weight p in len	per foot	Cop		PER FOOT. Weight per foot in length.
3/8	inch.	.424 .755	lbs.	11/4	inch.	4.71 lbs. 5.71 "
5/8	"	1.17		11/2		6.79 "
5/8 3/4 7/8	"	$\frac{1.69}{2.31}$	**	15/8 13/4	66	7.94 '' 9.21 ''
11/8	"	$\frac{3.02}{3.82}$	• • • • • • • • • • • • • • • • • • • •	17/8	• 6	10.61 '' 12.08 ''

# Plate or Sheet Iron, Brass, Copper and Lead. Weight of a Superficial Foot in Pounds. (AVOIRDIPOIS)

* -	(Avoirdupois).									
1	Thickness in Parts of an Inch.									
Inch.	16   18	1 16	$\frac{1}{4} \mid \frac{5}{16}$	3   1	76   1	5   5	1 1 %			
Brass " " 2	.5   5. .7   5.5 .9   5.8 .7   7.4	8.7 11	0.9 <b>1</b> 3.6 1.6 <b>1</b> 4.5	15.   17 16.3   19 17.4   20 22.2   25	$\begin{array}{c c} . & 21.8 \\ .3 & 23.2 \end{array}$	28.9 34	5 37.9			
Thickness by										
Wire Gauge.	0000.	000.	00.	0	1	2	3			
Thickness in decimals of an inch.	.454	.425	.380	.340	.300	.284	.259			
Iron in lbs. Brass" " Copper "	18.99 21.11 21.61	17.78 19.76 20.53	15.89 17.67 18.37	14.22 15.81 16.43	12.5 13.75 14.5	12. 13.2 13.9	11. 12.1 12.75			
Thickness by		rmingl	nam wi	ire-gau	ge, and	d in de	ci'als.			
Wire Gauge.	4	5	6	7	8	9	10			
Thickness in decimals of an inch.	.238	.220	.203	.180	.165	.148	.134			
Iron in lbs. Brass" " Copper "	10. 11. 11.6	8.74 9.61 10.1	8.12 8.93 9.4	7.5 8.25 8.7	6.86 7.54 7.9	6.24 6.86 7.2	5.62 6.18 6.5			
Thickness by	the Bi	rmingl	ham w	ire-gau	ge, and	d in de	eci'als.			
Wire Gauge.	11	12	13	14	15	16	17			
Thick.in dec. of an inch.	.120	.109	.095	.083	.072	.065	.058			
Iron in lbs. Brass. "	5.5	4.38	3.75   4.12	3.12 3.43	3.1	2.5	2.18			
Copper." Thickness by	5.8 the Bi	5.08   rming	4.34   ham w	3.6 ire-gau	3.27   ge, and	2.9 d in de	2.52 eci'als.			
Wire Gauge.	18	19	20	21	22	23	24			
Thick, in dec. of an inch.	.049	.042	.035	.032	.028	.025	.022			
Iron in lbs. Brass. " Copper. "	1.86   2.04   2.15	1.7   1.87   1.97	1.54 1.69 1.78	1.4 1.54 1.62	1.25 1.37 1.45	1.12 1.23 1.3	1. 1.1 1.16			

Cast-Iron Pipes, Hollow Columns, or Cylinders, Weight per lineal foot.

Diam. of	1			Thick	kness	in Inc	hes.		
Bore.	1/4:	3/8	1/2	5/8	3/4	7/8	1 !	11/8	11/4
					94 1				
Ins.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
1	3.06	5.06	7.36	9.97	12.89	16.11	19.63	1	
11/4	3.68	5.98	8.59	11.51	14.73	18.25	22.09		
11/2	4.29	6.9	9.82	13.04	16.56	20.4 22.5	24.54		
13/4	4.91 5.53	7.83	$11.05 \\ 12.25$	14.57	18.41	22.5	27.		
2	5.53	8.75	12.25	16.11	20.25	24.7 26.84	29.45		
21/4	6.14	9.66	13.5	17.64	22.09	26.84	31.85		
21/2			14.72		23.92	28.93	34.36		
23/4	7.36	11.5	15.91	20.7	25.71	31.14	36.81		
3	7.98	12.43	17.18	22.19	27.62	28.93 31.14 33.29	39.25	45.56	52.2
31/4	8.59	13.34	18.35	23.78	29.45	35.44 37.58 39.73 41.88	41.72 44.18	48.32	55.22
31/2	9.2	14.21	19.64	25.31	31.3	37.58	44.18	51.08	58.29
$33\sqrt{4}$	9.76	15.19	20.86	26.85	33.13	39.73	46.63	53.84	61.36
4	10.44	16.11	22.1	28.38	34.98	41.88	49.	56.61	64.25
41/4	11.1	17.08	$23.37 \\ 24.54$	29.97	29.45 31.3 33.13 34.98 36.87 38.65	44.03	51.6	59.42	67.45
41/2	11.66	17.94	24.54	31.44	38.65	46.17	53.99 56.45	62.12	70.56
43/4	12.27	18.87	25.77 27.	32.98	$\frac{40.5}{42.25}$	48.32	56.45	64.89	73.63
5	12.88	19.78	27.	34.54	42.25	50.46	58.9	67.64	
51/4	13.5 14.11	20.71	28.23	36.05	44.18	52.62	61.36	70.41	79.77
$51/_{2}$	14.11	21.63	$\frac{29.45}{30.68}$	37.58	46.02	54.76	63.81	73.17	82.84
53/4	14.73	22.55	30.68	39.12	47.86	56.91	63.81 66.27 68.5	75.94 78.7	85.91
6 7 8 9	15.34	23.47	31.9	40.65		59.06	68.5	78.7	89.
7	17.79	27.15	36.8	46.79	56.84	67.65	78.5	89.74	101.25
8		30.83	41.7	52.92	64.42		88.25	100.78	114.
9		34.52	46.5	59.07	71.5	84.84	99.5	111.84	126.
10	25.16	38.2	51.5	65.2	79.16	93.42	108.	122.87	138.
11		41.88		71.33	86,5	102.01 110.6	117.5	133.92	150.3
12	30.06	45.55	61.	77.46	93.6	110.6	127.25	144.96	163.
14	-			90.6	109.6	129. 146.4	148.8	168.7	189.
16					124.5	146.4	148.8 168.6	181.0	213.8
18					139.4	163.7	188.4	213.3	238.5
20						181.1	208.2	235.6	263.3
24					182.		247.9	280.2	312.9
28					213.		286.		360.
30					227.		305.		384.
34					257.	-	345.		443.

Weight of Cast-Iron, Brass, Copper and Lead Balls from 1 inch to 12 inches in diameter.

Diam.	Cast- Iron.	Br'ss.	Cop- per.	Le'd	Diam	Cast- Iron.	Br'ss.	Cop-Le'd
Ins. 1 11/2 2	.136 .46	.158	.166 .56	.214 .727	7	47.76 57.52	54.5 67.11	1bs.   1bs.   57.1   73.7   70.0   90.   85.2   110.1

#### (TABLE CONTINUED).

Diam. Cast	Br'ss.	Cop- Le'	d Diam	Cast-  Iron.	Br'ss.	Cop-   per.	Le'd
Ins.   1bs.   21/2   2.13   3.68   31/4   5.84   41/2   12.42   5   17.04   51/2   22.68   6   29.45   61/2   37.44	4.3 6.82 10.2 14.5 19.9 26.47 34.3	Tbs.   Tbs.   2.60   3.3   4.5   5.8   7.14   9.5   10.7   13.8   15.25   19.6   20.8   26.3   27.74   36.6   35.9   46.4   45.76   59.1	81/2 9 91/2 10 101/2 11 111/2 12 12	99.4 116.9 136.35 157.84 181.48	100.0 115.9 136.4 159.0 184.0 211.8 242.0	102.3 121.3 143.0 166.4 193.0	156.7 184.7 215.0 250.0 286.7 327.7

Weight of Parallel Angle Iron of equal sides, and Parallel T Iron, equal depth and width.

Parallel Angle Iron. Parallel T Iron. Uniform |W'g't of 1||Width of |Uniform |W'g't of 1 Length thickn'ss lineal ft. top table thickn'ss lineal ft. Through-in lbs and and total through-in lbs and of sides in Ins. out. dec. parts depth. out. dec. parts Ins. Ins. Ins. Ins. 3 23/4 8.0  $\frac{1}{2}$ 18.25 13.75 6 7.0 23/8 9.75 4 3/8 21/4 2 23/4 31/2 3/8 8.5 4.5 full 3/8 3.75 3 7.5 3.0 21/2 5-16 4.63 2.5 21/4 5-16 4.5 13/8 No. 6 w.g. 1.75 2 5-16 3.75 11/4 3.0 1.5 13/4 1/4 1/4 9 11/2 11/8 1.25 2.25 1.75 10 11/4 1.0 .875 3-167/8 10 1.0 3/4 78 1/8 .73 .563 1/8 5/8 34 .63 1/2 12 .5

Table Showing Number of Rivets in One Hundred Pounds.

Len- | Diameter in Inches | | Len- | Diameter in Inches

Len- gth in	Diam	eter i	n Inch	es.	Len- gth in	Diameter in Inches.			
Ins.	1/2	5/8	1 1 1 1 6	3/4	Ins.	1/2	5/8	11 16	3/4
3/4	1092	665			31/4	433	267	212	180
7/8	1027	597			31/2	413	248	201	169
1	940	538	450		334	395	241	192	160
11/8	840	512	415		4		230	184	158
11/4	797	487	389	356	41/4	1	220	177	150
13/8	760	460	370	329	41/2		210	171	146
11/2	730	440	357 -	280	43/4		200	166	138
15/8	711	420	340	271	5	[ ]	190	161	135

Table Showing No. of Rivets in 100 Pounds. (CONTINUED).

Len-	Diai	neter i	n Inch	nes.	Len- gth in	Diameter in Inches.			
Ins.	1/2	5/8	1 <u>1</u>	34	Ins.	1/2	5/8	16	3/4
13/4	693	390	325	262	51/4		180	156	130
17/8	648	375	312	257	51/2		172	151	124
2	608	360	297	243	53/4		164	145	120
21/8	573	354	289	237	6		157	140	115
21/4	555	347	280	232	61/4		150	138	111
21/2	525	335	260	220	61/2		146	134	107
$23\sqrt{4}$	500	312	242	208	634		143	129	104
3	460	290	224	197	7		140	125	100

## Weights of Taper Angle Iron, of equal Sides, and Taper $\tau$ Iron.

Tape	er An equa	gle II l Side	con, of			Tap	er T Ir	on.	
Length of sides in Ins.	Thickness of Edges.	Thickness of Root.	W'g't of 1 lineal ft. in lbs. & dec. parts.	Width of top table in Ins.	Total depth in Inches.	Thickness of top table at edges.	Uniform thickness of rib.	Thickness of top table at root.	W'g'tof 1 lineal ft. in lbs. & dec. parts.
21/2	1/2 1/2 7-16 3/8 5-16‡ 1/4 1/4	5-16‡ 5-16 5-16*	14.0 10.37 8.25 6.5 5. 5.87 3.25 2.62	Ins 3 2 21/2 2 2 2	Ins   31/4   25/8   3   21/2   11/2   11/2	Ins 38 38 5-16 1/2 5-16 1/4	7-16 1/2 5-16 1/2‡ 3/8 1/4	Ins 1/2 7-16 7-16 5/8 5/8‡ 5-16	8.0 8.0 5.25 6.5 3.5 2.87
		* Be	ire.				† Fui	7.7.	

#### Number of Nails in a Pound.

Title.	Size.	No.	per lb		Title.	Size	. No	per <b>lb.</b>
2 penny fine.	111/8 II	n.   760	nails.	16	pen, f	31/2 I	n (32	nails.
3 "	11/4 '	"  480	66	120	•	4	" 24	61
4 "	11/2	1300	66	30		41/9	" 18	66
5 "	134 '	' 200	66	40		5	. 14	66
6 "	2	" 160	66	50		51/2	" 12	66
7 "	21/4	'  128	66	160		16	" 10	66
8 "	21/2	' 92	66	6	fense	2	"  80	66
9 "	234	' 72	- 66	l¦8	61	21/2	" 50	66
10 "	3	60	- 66	10	66	3	" 34	44
12 "	314	. 44	66	12	6+	31/4	" 29	66

Number of Tacks in a Pound.

	Mullio	er of rack	S III a I O	arre.	
Title.	Length.	No. per lb.	Title.	Length.	No. per lb.
1 oz.	1/8 In.	16.000	10 oz.	11-16	1.600
11/2	3-16	10.666	12	3/4	1.333
2	1/4	8.000	14	13-16	1.143
21/2	1/4 5-16	6.400	16	78	1.000
3	3/8 7-16	5.333	18	15-16	.888
4	7-16	4.000	20	1	.800
6	9-16	2.666	22	1 1-16	.727
8	5/8	2.000	24	1 1/8	.666

Table Showing Weight of 100 feet of Iron, Steel, Copper and Brass Wire. (English and American Gauges).

rican Eng. gauge		lmeri	can (	Jauge	Э.	Birmingham Gauge.				
American and Eng. No.of gauge	Thick's in Dec.		ire p ineal		)	Thick's in Dec.	7	Vire linea	per 10 l feet	00
N a A	FI	Ι	S.	. C.	B.	可谓	I.	S.	C.	В.
	Ins	lbs.		lbs.	lbs.	Ins	lbs.	lbs.	lbs.	lbs.
0000	.46	56.07	56.60	64.05	60.51	.454	54.62	55.13		58.93
000	.409	44.46		50.79		.425	47.86	48.32		51.64
00	.364	35.26	35.59	40.28	38.06	1.38	38.27	38.63		41.28
0	.324	27.96	28.23	31.94	30.18	.34	30.63	30.92		33.05
1 3 4 5 6 7 8 9	.289	22.17	22.38	25.33	23.93	.3	23.85	24.07	27.24	25.73
2	.257	17.58	17.75	20.09	18.98	. 284		21.57	24.41	23.06
3	.229	13.94		15.93		259	17.78	17.94	20.03	19.18
4	.204	11.06	11.16	12.63	11.93	. 238	15.01	15.15		16.19
5	.181	8.77		10.02	9.46	.22	12.82	12.95		13.84
6	.162	6.95	7.02	7.94	7.50	203	10.92	11.02		11.78
7	.144	5.51	5.56	6.30	5.95	.18	8.58	8.66	9.80	9.26
Ø	.128	4.37	4.41	4.99	4.72	.165	7.21	7.28	8.24	7.78
10	.114	3.46	$\frac{3.50}{2.77}$	3.96	3.74 2.96 2.35	.148	5.80	5.85	6.63	6.26
10	.101	2.75		3.14	2.90	.134	4.75	4.80	5.43	5.13
11	.090	2.18 1.73	2.20	2.49	2.30	.12	3.81	3.85	4.35	4.11
12	.080		1.74	1.97	1.86	.109	3.15	3.18	3.59	3.39
13	.071	1.37	1.38	1.56	1.48	.095	2.39	2.41	2.73	2.58
14 15	.064	1.08	1.09 .87	1.21	1.17	0.083	1.82	1.84	2.08	1.96
16	.057 $ .050$	.86	.69	.98	.93	0.072	$1.37 \\ 1.12$	1.38 1.13	1.57 1.28	1.48 1.21
17	.045	.68	.54	.78 .61	.75	.065  $ .058 $	1.14		1.08	.96
18	.040	.34	.34	.01	.58	.049	.89 .63	.90 .64	.72	.68
19	.035	.34	94	.38	.36	.049		.47	.53	.51
20	.031	.27	97	30	.29	.035	99	.33	.37	.35
21	.028	21	91	.24	23	.032	97	97	.31	90
$\frac{21}{22}$	.025	.21 .17 .13	.34 .27 .21 .17 .13 .10	.19	,18	.028	.46 .32 .27 .20 .16 .12 .10	.27 .21	.23	.29
23	.023	12	12	.15	.14	.025	16	.16	.19	.18
$\frac{23}{24}$	.020	110	10	.12	:11	.023	12	.13	.15	.14
25	.017	.08	108	.09	.09	.02	10	.10	:12	:17
$\frac{25}{26}$	.015	.06	.06	.07		.018	.08	.08		.09
	1.010	1 .00	1 .00	1 .01	1 .0.	1.010	.00	•170		.00

Table Showing Weight of Wrought Iron, Steel, Copper and Brass. (American and English Gauges).

an ng. uge	A	meri	can G	auge		Birmingham Gauge.				
American and Eng. No.of gauge	ick's Dec.	Plat	es per	r Sq.	foot.	Plates per Sq. fo				
Na	답되	I.	S.	C.	B.	[급표]	I.	S.	C.	В.
	Ins	lbs.	lbs.	lbs.	lbs.	Ins	lbs.	lbs.	lbs.	lbs.
0000	.46	18.45		20.83	19.68	.454	18.21	18.45	20.56	
000	.409		16.65	18.55	17.53	.425	17.05	17.28		18.19
00	.364	14.63	14.83	16.52	15.61	.38	15.24		17.21	16.26
0	.324	13.03	13.20	14.71	13.90	.34		13.82	15.40	14.55
1	.289	11.60	11.76	13.10	12.38	.3	12.03	12.19	13.59	12.84
2	.257	10.33	10.47	11.67	11.02		11.39	11.54	12.86	12.15
1 2 3 4 5 6 7 8 9	.229	9.20 8.19	9.32	10.39	9.81	259	10.39	10.53	11.73	11.08
4	.204	8.19	8.30 7.39 6.58	9.25	8.74 7.78 6.93 6.17	.238	9.54	9.67	10.78	10.18
5	.181	7.30	7.39	8.24 7.33 6.53	7.78	.22	8.82	8.94 8.25 7.31 6.70	9.96	9.41
6	.162	6.50	6.58	7.33	6.93	.203	8.14 7.22 6.62	8.25	9.19	8.68
7	.144	5.78	5.86 5.22	6.53	6.17	1.18	7.22	7.31	8.15	7.70
8	.128	5.15	5.22	1 5.82	5.49	.165	6.62	6.70	7.47	7.06
9	.114	4.59	4.65	5.18	4.89	1.148	5.93	6.01	6.70	6.33
10	.101	4.08	4.14	4.61	4.36 3.88	.134	5.37	5.44	6.07	5.73
11	.090	3.64	3.68	4.11	3.88	.12	4.81	4.87	5.43	5.13
12 13	.080	3.24	3.28 2.92	3.66	1 3.45	11.109	4.37 3.81 3.33 2.88	4.83	4.93	
13	.071	2.88	2.92	3.25	3.07	.095	3.81	3.86 3.37	4.30	4.06
14	.064	2.57	2.60	2.90	2.74		3.33	3.37	3.75	3.55
15	.057	2.28	2.32	3.25 2.90 2.58	2.44	.072	2.88	2.92	3.26	3.08
16	.050	2.03		2.30	2.17	.065	12.60	2.64	2.94	2.78
17	.045	1.81		2.05	1.93	.058	2.32	2.35	2.62	
18	.040	1.61	1.63	1.82		.049	1.96			2.09
19	.035	1.44			1.53	.042		1.70		1.79
20 - 21 22 23 24 25	.031	1.28		1.44	1.36		1.40	1.42	1.58	1.49
21	.028	1.14	1.15			.032	1.28		1.44	1.36
22	.025	1.01	1.03				1.12	1.13	1.26	1.19
23	.022	.90		1.02		.025	1.00	1.01		1.07
24	.020	.80	.81	.91	.86		.88	.89		.94
25	.017	.71	.72	.81	.76		.80		.90	.85
26	.015	.63	.64	.72	.68	.018	.72	.73	.81	.77

Weight of a lineal foot of Square and Round Malleable Bar Iron from 1-4 inch to 12 inches in diameter. (AVOIRDUPOIS POUNDS).

Size Inches, Sq.Rolled bar Iron Round ""	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	.87 .47
Size Inches. Sq. Rolled Iron. Round " "	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	.74 .51

Square and Round Malleable Bar Iron. (Continued).

Size Ins. Sq.R.I.bar Round "	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
· Do	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Do	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Do	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
Do	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
Do	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$

Weight of 9 feet length, of flanged Cast-Iron Pipes of various diameters.

Diameter of Bore.	Thickn'ss of Metal.	Diameter of Flange	Thickn'ss of flange.	Diameter of Cir.thr- o'gh hole'	Diam. of Holes.	No. of Holes	Weight.
Ins. 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Ins. 388 382 2588 444 37888 388 7888 7888 111	Ins. 61/2 71/2 101/2 12 14 15 161/2 19 20 21 22 23 241/2 251/2 28 29	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ins. 434 6 734 834 10 1134 1234 151/2 1634 1734 1834 1934 2034 22 23 24 25 26	Ins. 588 344 788 11 11 8 11 8 11 11 11 11 11 11 11 11	444466666666688888888888888888888888888	$\begin{array}{c} \text{Cwt-qr-Ib} \\ 0-3-0 \\ 1-0-3 \\ 1-0-3 \\ 1-3-5 \\ 2-1-12 \\ 3-2-1 \\ 4-3-17 \\ 5-2-9 \\ 6-1-12 \\ 7-0-0 \\ 8-3-24 \\ 9-3-5 \\ 10-2-0 \\ 10-2-0 \\ 12-0-25 \\ 12-3-8 \\ 13-2-17 \\ 16-1-15 \\ 17-2-13 \\ 18-0-26 \\ \end{array}$

TABLE SHOWING WEIGHT OF I FOOT OF SEAMLESS
DRAWN BRASS AND COPPER TUBING.

Outside	Length	Brown & Sharpe's	Weight p	er Ft.
Diameter.	reet.		Brass.	Copper.
Outside Diameter.  38 1/2 58 34 13-16 78 15-16 1 11/8 11/9 15/6 13/8 1 13-16 17/8 1 15-16 2 2 2 2 3 4 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Feet.  12 12 12 12 12 12 12 12 12 12 12 12 12		Brass.  1bs17 .25 .33 .42 .47 .52 .58 .66 .85 .98 .1.20 1.35 1.70 1.82 1.95 2.	Copper.  1bs17 .25 .35 .46 .57 .69 .89 .97 .1.25 1.40 1.60 1.76 1.88 2.01 2.06 2.10 2.16
	10 10 10	66 66	2.05 2.10 2.35 2.36 3.	2.16 2.40 2.42
21/ <sub>2</sub> 25/8 23/4 31/	10 10 10 10 10	8 & 81/2	3.67 3.75 3.92 4.18	3.10 3.75 3.90 4.05 4.30
31/4 31/2 4 5	10 10 10 10	66 66	4.18 4.50 5.40 6.75	4.63 5.56 6.95

WEIGHT OF A SQUARE FOOT OF CAST AND WROUGHT IRON, COPPER, LEAD, BRASS AND ZING.

From I-16 to 2 inches in Thickness.

Thick- ness.	Cast- Iron.	Wr'g't Iron.	Copper.	Lead.	Brass.	Zine.
Ins.	lbs.	lbs.	lbs.	lbs.	lbs	lbs.
1-16	2.346	2.517	2.89	3.691	2.675	2.34
1/8	4.693	5.035	5.781	7.382	5.35	4.68
3-16	7.039	7.552	8.672	11.074	8.025	7.02
1/4	9.386	10.07	11.562	14.765	10.7	9.36

WEIGHT OF A SQUARE FOOT OF CAST AND WROUGHT IRON, COPPER, LEAD, BRASS AND ZINC. (TABLE CONTINUED).

Thick- ness.	Cast- Iron.	Wr'g't Iron.	Copper.	Lead.	Brass.	Zinc.
Ins. 5-16 3/8	lbs. 11.733 14.079	lbs. 12.588 15.106	lbs. 14.453 17.344	lbs. 18.456 22.148	lbs. 13.375 16.05	lbs. 11.07 14.04
7-16 1/2 9-16 5/	16.426 18.773 21.119 23.466	17.623 20.141 22.659 25.176	20.234 23.125 26.016 28.906	25.839 29.53 33.222 36.913	18.725 21.4 24.075 26.75	16.34 18.72
5% 11-16 34 13-16	25.812 28.159 30.505	27.694 30.211 32.729	31.797 34.688 37.578	40.604 44.296 47.987	29.425 32.1	
7/8 15-16 1	32.852 35.199 37.545	35.247 37.764 40.282	40.469 43.359 46.250	51.678 55.37 59.061		
11/8 11/4 13/8	42.238 46.931 51.625 56.317	45.317 50.352 55.387 60.422	52.031 57.813 63.594 69.375			
$1\frac{1}{2}$ $1\frac{5}{8}$ $1\frac{3}{4}$ $1\frac{7}{8}$	61.011 65.704 70.397	65.458 70.493 75.528	75.156 80.938 86.719		111	
2,00	75.090	80.563	92.500			

Weight of a lineal foot of Flat Rolled Iron from 1-4 inch to 15-16 inch thick by 1 inch to 3 inches wide.

W'd'h of Iron.					Thi	ckne	ss in	Inc	hes.			
¥ Ja	1/4	16	3/8	1 7 6	1/2	9 16	5/8	116	3/4	1 13	17/8	15
lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
11/8							2.08 2.34					
11/8	1.04	1.30	1.56	1.82	2.08	$\frac{2.10}{2.34}$	2.60	2.86	$\frac{2.01}{3.12}$	3.38	3.64	3.90
1¼ 1¾ 1½	1.14	1.43	1.71	2.	2.29	2.57	2.86	3.15	3.43	3.72	4.01	4.29
11/2							3.12 3.38					
15% 134 178 2							3.64					
1%	1.56	1.95	2.34	2.73	3.12	3.51	3.90	4.29	4.68	5.07	5.46	5.85
2	1.66	2.08	2.50	2.91	3.33	[3.75]	4.16	4.58	5.	5.41	5.83	6.25
21/8	1.77	2.21	2.65	3.09	2.54	3.98	4.42 4.68	4.86	5.62	5.75	6.19	7.03
2¼ 23/8							4.94					
21/2	2.08	2.60	3.12	3.64	4.16	4.68	5.20	5.72	6.25	6.77	7.29	7.81
25/8	2.18	2.73	3.28	3.82	4.37	4.92	$5.46 \\ 5.72$	6.01	6.56	7.10	7.65	8.20
276							5.98					
21/2 25/8 23/4 27/8 3	[2.50]				5.	5.62	6.25	6.87	7.50	8.12	8.75	9.37

To ascertain the Weights of larger sizes take the half size of that required, and double it. Thus, required the weight of  $4\times1/2$  in. refer to  $2\times1/2$  in.=3.33 $\times2$ =6.66 lbs.

Table showing the weight of water in pipes of various diameters, one foot in length.

Diam. in Ins.	Weight in lbs.	Diam.	Weight in lbs.	Diam. in Ins.	Weight in lbs.	Diam. in Ins.	Weight, in lbs.	Diam. in Ins.	Weight in lbs.
333344445555566667777888	3	81234 9 914 1234 10 10 10 10 10 10 10 10 10 10 10 10 10 1	2412 26 27-14-15 30-15 3	14 14 14 14 14 14 14 14 14 14 14 14 14 1	$\begin{array}{c} 663 \\ 691 \\ 4 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ 1$	$ \begin{array}{ c c c c }\hline & 19\frac{1}{2}\frac{1}{3}\frac{1}{4}\\ & 20\frac{1}{2}\frac{1}{2}\\ & 21\frac{1}{2}\frac{1}{2}\\ & 22\frac{1}{2}\frac{1}{2}\\ & 22\frac{1}{2}\frac{1}{2}\\ & 23\frac{1}{2}\frac{1}{2}\\ & 24\frac{1}{2}\frac{1}{2}\\ & 25\frac{1}{2}\frac{1}{2}\\ & 26\frac{1}{2}\frac{1}{2}\\ & 27\frac{1}{2}\frac{1}{2}\\ & 28\frac{1}{2}\\ & 29\frac{1}{2}\\ & 29\frac{1}{2}\\ \end{array} $	129½ 132 14314 15014 15014 15014 15014 15014 180	$ \begin{vmatrix} 30 \\ 301^{\frac{1}{2}} \\ 31 \\ 31 \\ 32 \\ 321^{\frac{1}{2}} \\ 33 \\ 331^{\frac{1}{2}} \\ 341^{\frac{1}{2}} \\ 35 \\ 361^{\frac{1}{2}} \\ 37 \\ 37 \\ 37 \\ 391^{\frac{1}{2}} \\ 391^{\frac{1}{2}} \\ 40 \end{vmatrix} $	3063 31714 32744 349 360 3714 394 4053 44154 454 479144 456 479144 456 51855 51855 51855 5455

TABLE SHOWING the WEIGHT of WATER AT DIFFERENT TEMPERATURES.

Temp Farh.	W'g't of a Cubic foot.	Temp. Farh.	W'g't of a Cubic foot.	Temp. Farh.	W'g't of a Cubic foot.	Temp. Farh.	W'g't of a Cubic foot.
40° 42 52 62 72 82 92	62.408 62.406 62.377 62.321 62.025 62.015 62.004	102° 112 122 132 142 152 162	61.092 61.078 61.063 61.047 61.030 61.011 60.920	172°   182   192   202   212   230   250	60.72 60.55 60.28 60.05 59.82 59.37 58.85	275° 300 350 400 450 500 600	58.17 57.42 55.94 54.34 52.70 51.02 47.64

The boiling point of water decreases one degree (on an average) for every 530 feet above sea level. The boiling point at sea level being 212 degrees.

## $\begin{array}{c} DIMENSIONS\ OF\ BOLT\ AND\ NUTS\ SQUARE\\ AND\ HEXAGONAL. \end{array}$

meter Bolt.	of.	th of Nut.	of	of d.		VOLU	JME.	
Diameter of Bolt.	Depth Nut.	Width Sq. N	Diam Hex'l	Width of Head.	Hexa'l Nut.	Square Nut.	Hexa'l Head.	Bolt per inch of Length.
Ins.	Ins	Ins	Ins.	Ins.	Cu.Ins.	Cu. Ins.	Cu.Ins.	Cu.Ins.
1/8 3-16	.15	.2	1/4 3/8 1/2 5/8 3/4 7/8	.2	.00425		.0045	.01227
3-16	.2 .25 .35	.3	3/8	.3	.01276		.0152	.02761
1/4 5-16	.25	.45	$\frac{1}{2}$	.4	.02836		.036	.04908
5-16	.35	.55	5/3	.5	.06235	.07903	.07	.07669
3/8 <b>7-</b> 16	.4	.6	3/4	.6	.10209	.09984	.1215	.1104
7-16	.5	.75	7/8	.7	.17368	.2061	.1929	.1503
1/2 9-16	.55	.85	1	.75	.25584	.28941	.2531	.1963
9-16	.6	.95	11/8 11/4	.85	.34449	.3924	.3658	.2485
5/8	.7	1.1	11/4	.95	.49625	.6323	.5076	.3067
11-16	.75	1.2	13/8	1.05	.64328	.8016	.6822	.3712
3/4 13-16	.8	1.3	11/2 15/8	1.125	.81664	.9986	.8543	.4417
13-16	.9	1.4	15/8	1.25	1.0782	1.2977	1.143	.5184
7/8 1	.95	1.5	$\frac{13\cancel{4}}{2}$	1.35	1.3199	1.5663	1.435	.6013
1	1.1	1.75	<b>2</b>	$\frac{1.5}{1.7}$	1.996	2.5048	2.025	.7854
11/8 11/4	1.25	1.95	21/4	1.7	2.8701	3.5106	2.926	.994
11/4	1.37	2.15	$21/_{2}$	1.875	2.8846	4.6518	3.955	1.227
13/8	1.5	2.4	$\frac{2\sqrt{4}}{3}$	2.1	5.1474	6.414	5.457	1.484
11/2	1.65	2.6	3	2.25	6.737	8.2384	6.834	1.767
15/8	1.8	2.8	31/4 31/2	2.45	8.6267	10.381	8.778	2.073
13/8 11/2 15/8 13/4 17/8	1.9	3.	31/2	2.625		12.53	10.853	2.405
1/8	2.05	3.25	33/4	2.8	13.058	15.993	13.23	2.761
<u>Z</u>	2.2	3.45	4	3.	15.97	19.275	16.2	3.141

#### MARKS and weight of English Tin-Plates.

	g		
Brand.	Plates per Box.	Length and Breadth.	Net W'g't per Box.
1C or 1 com	No. 225	Inches. 1334 by 10	lbs. 112
$\overline{2}$ C	**	131/4 " 93/4	105
3C HC	"	123/4 " 91/2 133/4 " 10	98 119
HX 1X	"	1334 " 10	157
$2\mathbf{X}$		1334 " 10 1314 " 934	140 133
3X 1XX	"	123/4 " 91/2 133/4 " 10	126 161
1XXX	"	1334 " 10	182
1XXXX 1XXXXX	"	1334 " 10 1334 " 10	203 224
1XXXXXX DC	100	1334 " 10	245 98
DX	100	1634 " 121/2	126

MARKS and weight of ENGLISH Tin-Plates. (Continued).

Brand.	Plates per Box.	Length and Breadth.	Net W'g't per Box.
	No.	Inches.	lbs.
DXX	100	1634 " 121/2	147
DXXX	- 61	1634 " 121/2	168
DXXXX	66	1634 " 121/2	189
SDC	200	15 " 11"	168
SDX	66	15 " 11	188
SDXX	44	15 " 11	209
SDXXX	66	15 "11	230
SDXXXX	66	15 " 11	251
SDXXXXX	66	15 "11	272
SDXXXXXX	66	15 " 11	293
Leaded IC	112	20 " 14	112
" IX	112	20 " 14	140
ICW	225	1334 " 10	112
IXW	225	1334 " 10	140
CSDW	200	15 " 11	168
CIIW	100	163/4 " 121/2	105
XIIW	100	1634 " 121/2	126
TT	450	1334 " 10	112
XTT -	450	1334 " 10	126

Note:—When the plates are 14 by 20 inches there are 112 in a box.

Table of Standard Dimensions of Wrought Iron
Welded Tubes.

				***	ucu	i ubcs.			
Nominal Diameter.	External Diameter.	Thickness.	Internal Diameter.	Internal Circum.	H-0	Length of pipes per sq. foot.of Int'al and Extern'l sufaces.	Internal area.	Weight per ft.	No. of threads per inch of Screw.
Ins.	Ins.		Ins.	Ins.	Ins.	Feet Feet	Ins.	1bs. .24	07
1/8 1/4 8/8 1/2 3/4	.40	.068	.27	.85		14.15 9.44	.057	.24	27
1/4	.54	.088	.36	1.14	1.7	10.5 7.075	.104	.42	18
3/8	.67	.091	.36 .49 .62	1.55	2.12	7.67 5.657	.192	.56 .84	18
1/2	.84	.109	.62	1.96	2.65	6.13 4.502	.305	.84	14
3/4	1.05	.113	.82	2.59	3.3	4.64 3.637	.533	1.13	14
1	1.31	.134	1.05	3.29	4.13	3,66 2,903	.192 .305 .533 .863	1.67	111/2
11/4	1.66	14	1.38	4.33	5.21	2.77 2.301	1.496	2.26	14 111/ <sub>2</sub> 111/ <sub>2</sub> 111/ <sub>2</sub>
11/5	1.9	.145	1.61	5.06	5.97	2.37 2.10	2.038	2.69	111/6
11/ <sub>4</sub> 11/ <sub>2</sub> 2 21/ <sub>2</sub> 3	$\frac{1.3}{2.37}$	.154	2.07	6.49	7.46		3.355	3.67	111/2
01/				0.49				5.77	11/2
21/2	2.87	.204	2.47	7.75	9.03	1.55 1.324	4.783		8 8
3	3.5	1.217	3.07	9.64	11.	1.24 1.091	7.388	7.55	1 8

(TABLE CONTINUED).

				(					
Nominal Diameter.	External Diameter.	Thickness.	Internal Diameter.	Internal Circum.	External Circum.	Length of pipes per sq. (2) foot. of Int'al and Exter'al surfaces.	Internal area.	Weight per ft.	No. of threads per inch of Screw.
Ins.	Ins.	Ins		Ins.	Ins.	Feet   Feet		lbs.	
31/2	4.	.226		11.15	12.57	1.08 0.995	9.887	9.05	8
4′-	4.5	.237	4.07		14.14	.95 0.849	12.73	10.73	8
41/9	5.	.247	4.51	14.15	15.71	.85 0.765	15,939	12.49	8
5	5.56		5.04	15.85	17.47	.78 0.629	19.99	14.56	8
Ř.	6.62	.28	6.06	19.05	20.81	.63 0.577	28, 889	18 77	8
ž	7.62	.301		22.00		.54 0.505	38 737	23 41	8
ġ	8.62	.322		25.08		.48 0.444	50 039	28.35	Ř
ğ	9.69	.344	9.	28 28	30.43	.42 0.394			Ř
41/ <sub>2</sub> 5 6 7 8 9 10	10.75	366		31 47	33.77	.38 0.355	78 838	40 64	888888888
10	120.00	1.000	120.02	02.11	100.11	100 0.000	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	10.01	

Tables of the different quantities of Coal-gas of the Specific gravity .420, delivered in one hour, from horizontal pipes of different diameters and lengths, and under different pressure.

Quantities delivered by a 2 inch main in Cubic feet.

ngth pip's yds.		sure in i		Perpendicular Head of water.					
in of the	0.50	0.75	1.00	1.50	2.00	3.00			
10	2896	3558	4135	4923	5792	6950			
15	2364	2904	3331	4080	4728	5768			
20	· 2047	2507	2886	3541	4094	4994			
25	1830	2241	2580	3165	3660	4465			
30	1673	2049	2368	2894	3346	4082			
40	1445	1770	2037	2490	2890	3525			
50	1294	1585	1824	2238	2588	3157			
100	915	1121	1290	1582	1830	2232			
150	748	916	1054	1304	1496	1825			
200	647	792	912	1119	1294	1578			
250	579	709	816	1010	1158	1412			
300	522	639	736	903	1044	1273			
400	457	559	644	790	914	1115			
500	409	500	576	707	818	997			

Rule:—The discharge of the same gas through different openings and under the same pressure are proportional to the areas of the orifices in circular inches or to the square of their diameters.

### QUANTITIES DELIVERED BY A 6 INCH MAIN IN CUBIC FEET.

Length of pipe in yds.		sure in i and part		Perpendicular Head of water.			
m yus.	0.50	0.75	1.00	1.50	2.00	3.00	
100	8240	10095	11657	14276	16484	20190	
<b>1</b> 50	6730	8242	9517	11657	13460	16484	
200	5828	7138	8242	10095	11657	14276	
300	4759	5828	6730	8242	9517	11657	
<b>4</b> 00	3929	4813	5557	6806	7858	9626	
- 500	3686	4515	5213	6384	7372	9030	
600	3365	4121	4759	5828	6730	8242	
700	3115	3816	4406	5396	6230	7632	
800	2778	3403	3929	4813	5557	6807	
900	2747	3365	3886	4759	5494	6730	
1000	2606	3192	3686	4515	5213	6384	
1760	1965	2406	2778	3403	3929	4813	
2640	1604	1965	2269	2778	3208	3929	
3520	1389	1702	1965	2406	2778	3403	
5280	1134	1389	1604	1965	2269	2778	
- 7040	982	1149	1389	1702	1965	2298	
8800	879	1076	1287	1521	1758	2152	
10000	824	1010	1166	1428	1648	- 2019	

For a 12 inch main multiply by 4 " "24 " "16 " "16 " divide " 4

### Diameter and length of gas-pipe to transmit given volumes of gas to branch.

Diam- eter.	Length.	Volume   per hour.	Diam- eter.	Length.	Volume per hour.
Ins	Feet.	Cub. Ft.	lns.	Feet.	C. Ft.
.4	100	50	5.32	2000	2000
1.	200	250	6.33	4000	2000
$\frac{1.97}{2.65}$	600	500	7.	6000	2000
	1000	700	7.75	1000	6000
3.16	1000	1000	9.21	2000	6000
3.87	1000	1500	10.95	1000	8000

The pressure with which gas is forced through pipes should seldom exceed 2½ inches of water at the Works, or the leakage will exceed the advantages to be obtained from increased pressure.

When pipes are laid at an inclination either above or below the horizon, a correction will have to be made in estimating the supply, by adding or deducting  $_{1}^{1}$  $_{0}$  of an inch from the initial pressure for every foot of rise or fall in the length of the pipe.

Size of pipe required to furnish gas from the main

from 2 lamps to 30.

			-		
Number			Number	Length	Diam.
of	from	of	of	from	of
Lamps.	Main.	Pipe.	Lamps.	Main.	Pipe.
2 3 4 6	Feet. 40 30 40 50	Ins. 3/8 3/8 1/2 5/8	15 20 25 30	Feet. 130 150 180 200	Ins. 1 11/4 13/4 11/2
10	100	3/4			- /-

Regulation of the diameter and Extreme length of Tubing and number of burners permitted.

Diameter of Tubing.	Length.	Number of Burners	Capacity of Meters.	Number of Burners
Ins. 14 3/8 1/9 5/8 3/4 1 11/2 2	Feet. 6 20 30 40 50 70 100 150 200	1 3 6 12 20 35 60 100 200	Light. 3 5 10 20 30 45 60 100	6 10 20 40 60 90 120 200

HOW TO TELL THE STATE OF THE METER. Each figure or division, on the different dials of the Inex, indicates as follows: On the right hand dial, 100, 200,

dex, indicates as follows: On the right hand dial, 100, 200, 300 cubic feet, &c.; on the middle dial, 1,000, 2,000, 3000, &c.; on the left hand dial, 10,000, 20,000, 80,000, &c.



Look at the left hand dial, and set down the figure at the least value next the pointer, which, on the above diagram, is 1. Next look at the middle dial. As before, set down the least figure next the pointer, which, in the diagram, is 3. Next, look at the right hand dial. Take whichever figure is nearest, which, in the diagram is 5. Set all these figures down, thus: 135, and add two ciphers, to represent hundreds, and you have 13,500, which is the present state of the meter. If a previous observation has been taken, subtract the state of the meter at that observation from the present state, and the difference is the amount consumed in interval.

#### STRENGTH of MATERIALS.

A Table of the depths of square beams or bars of Cast-Iron, calculated to support from 1 cwt to 14 tons in the middle, the Deflexion not to exceed 1-40 of an inch for each foot in length.

				HOL	110	1 01		100	0 111	10115	,011.			
ts	bt S.				1	LEI	VGT	H	IN .	FFE	T.			
Weight in cwts.	Weigh in Ibs.	41	6	81	10	12	14	16	18	20	22	24 [	26	28
Ve	li Ne			_	7	TI				VCH				
	170	7 ().	1 41			) EI	0.0	0 1	0.51			2.0	0.0	
1	112	1.2	1.4	1.7	1.9	4. 0	2.2	2.4	2.5 3.0	2.6 3.1	2.7	2.9	3.0	3.1
Z	224	1.4	1.7	2.0	2.4	4. 4	2.0	2.0	3.3	3.4	3.3 3.6	3.4	3.6 3.9	3.7
3	990	1.0	2.0	2.4	2.4	2. (	9.1	9.1	2.5	3.7	3.9	4.0	4.2	4.1
1 2 3 4 5 6 7 8 9 10	560	1 0	2.0	2.5	2.0	2. 0	0.1	2.5	3.5 3.7	3.9	4.1	4.3	4.4	4.3
6	672	1.0	2.5	2.6	2.0	ບ. ບ ຊິງ	3.0	3.7	2.1	4.1	4.3	4.5	4.6	4.8
7	784	1 9	23	2.7	3.0	3 3	3.5	3 8	3.9 4.1	4.2	4.4	4.6	4.8	5.0
8	896	20	2.4	2.8	3 1	3 4	3.7	3 9	4.2	4.4	4.6	4.8	5.0	5.2
ğ	1.008	20	2.5	2.9	3 2	3. 5	3.8	4.0	4.3	4.5	4.7	4.9	5.1	5.3
10	1.120	21	2.6	3.0	3.3	3. 6	3.9	4.2	4.4	4.7	4.9	5.2	5.3	5.4
ii	1.232	2.1	2.6	3.0	3.4	3. <del>7</del>	4.0	4.3	4.5	4.8	5.0	5.3	5.4	5.6
12	1.344	2.2	2.7	3.1	3.5	3. 8	4.1	4.4	4.7	4.9	5.1	5.3	5.5	5.7
13	1.456	2.2	2.7	3.1	3.5	3.8	4.2	4.4	4.7	4.9	5.2	5.4	5.6	5.9
14	1.568	2.3	2.8	3.2	3.6	3.9	4.2	4.5	4.8	5.0	5.3	5.5	5.7	6.0
15	1.680	2.3	2.8	3.2	3.6	4.0	4.3	4.6	4.9	5.2 5.2	5.4	5.6	5.8	6.1
16	1.792	2.4	2.9	3.3	3.7	4.0	4.4	4.7	5.0	5.2	5.5	5.7	5.9	6.2
17	1.904	2.4	2.9	3.4	3.8	4.1	4.4	4.7	5.0	5.3	5.5	5.8	6.0	6.2
18	2.016	2.4	3.0	3.4	3.8	4. 2	4.5	4.8	5.1	5.4	5.6	5.9	6.1	6.4
19	2.128	2.5	3.0	3.5	3.9	4. 2	4.6	4.9	5.2	5.4	5.7	6.0		6.5
1 T	2.240	2.5	3.0	3.5	3.9	4, 3	4.6	4.9	5.2	5.5	5.8	6.0	6.3	6.5
11/4 11/2 13/4	2.800	2.6	3.2	3.7	4.1	4. 5	4.9	5.2	5.5	5.8	6.1	6.4	6.6	6.9
11/2	3.360	2.8	3.4	3.9	4.3	4.7	5.1	5.5	5.8	6.1 6.3	6.4	6.7	7.0	7.2
15/4	3.920	2.9	3.5	4.0	4.5	4. 9	5.3	5.7	6.0	6.3	6.7	6.9	7.2 7.6	7.2 7.5 7.7
21/2	4.480	2.9	5.0	4.1	4.7	5. T	5.5	5.9	6.2	6.5	6.8 7.3 7.6	7.2	7.6	7.7
3	0.000	5.1	3.0	4.4	4.9	อ. อ	0.0	0.4	6.6	6.9 7.3 7.5 7.8	7.5	7.6 7.9	7.9 8.3	8.2 8.6
31/2	7 940	3.0	4.0	4.0	5.2	5 8	6.2	6.7	6.9 7.1	7.5	7.9	8.2	8.6	8.9
4	8 060	3.5	1 2	4.0	5.5	6.0	6.5	7.0	7.4	7.0	8.2	8.5	8.9	9.2
41/2	10.080	0.0	4.5	5.1	5.7	6.2	6.7	7 2	7.6	8.0	8.4		9.1	9.5
5 2	11.200		4.5	5.2	5.8	6 4	6.9	7.4	7.8	8.2		9.0	9.4	9.7
6	13 440		1.0	5.5	6.1	6.7	7 2	77	82	8.6	90	9.4	9.8	10.2
6	13.440 15.680			5.7	6.3	6.9	7.5	8.0	8.2 8.5	8.9	9.4	9.8 10.1	10.2	10.2 10.6
8	17.920			5.9	6.6	7.2	7.8	8.3	8.8	93	9.7			
9	20.160			6.0	6.8	7.4	8.0	8.5	9.0	9.5	10.0	10.4	10.9	11.3
10	22.400				6.9	7.6	8,2	8.8	9.3	9.8	10.3	10.7	11.2	11.6
11	1112 2244 448 3366 448 8966 672 224 8966 672 1.098 8966 1.098 1.120 1.332 1.344 81.680 1.568 8.966 8.9				7.1	7.8	8.4	9.0	9.5	10.0	10.5	11.0	11.5	11.9
12	26.880				7.2	7.9	8.4 8.6	9.2	9.7	10.2	10.8	11.2	11.7	11.3 11.6 11.9 12.1
13	29.120				7.4	8.1	8.8	9.4	9.9	10.4	11.0	11.5	11.9	12.4
14	31.360	1			7.5	8.3	8.9	9.5	10.1	10.6	11.1	11.7	12.1	12.6
Def	lexion	1.1	.15	.2	.25	0	.35	1	.45	E	EE	c	CE	P
in I	nches.	1.1	.10	.4	.40	0.	66.	.4	64.	.5	.55	.6	.65	.7

TABLE (Continued).

nt is	o pt				L	engt!	h in	Feet				
elght tons.	eight Tbs.	10	12	14	16	18	20	22	24	26	28	30
₩ii	ii ₩	-			De	pth	in I	nche	s.			
15	133600	7.7	8.4	9.1						12.3		
16	35840	7.8	8.5	9.2	9.8	10.4	11.0	11.5	12.0	12.5		
17	38080	7.9	8.7			10.6	11.2	11.7		$12.7 \\ 12.9$		13.7 13.9
18 19	40320	8.0 8.1	8.8   8.9	9.0	10.1	10.0	11.6	$\frac{11.9}{12.2}$	12.9	13.1		14.1
20	44800	0.1	9.0	9.7	10.3	11 0	11 6	12.5	12.7	13.2	13.8	14.2
$\tilde{2}\tilde{2}$	49280		9.2	(10.0)	10.7	111.3	111.9	012.8	13.0	13.6	14.1	14.6
24	53760		9.4	10.2	10.9	11.5	12.2	2 13.0	13.4	.13.9	14.4	14.9
26	58240									14.2		
28	62720		9.8	10.6	11.4	12.0	12.	113.5	13.9	14.4	15.0	15.5
	exion	.25	.3	.35	4	.45	.5	.55	1.6	.65	.7	.75
in I	nches.				1	1	1 *-	1 *	1	1	1	1
Len	gth in	14	16	18	20	22	24	26	28	30	32	34
F	'eet.				,	1		إلنبا				7.
30	67200		11.5	12.2	12.9	13.5	14.1	14.7	15.2	15.7	16.3	16.8
32	71680		11.7	12.4	13.1	13.7	14.3	14.9		16.0		
34 36	76160 80640		$11.9 \\ 12.0$	12.0	10.0	13.9 14.1	14.0	15.2		16.2 16.5		
38	85120			13.0	13.6	14.3	14.9	15.5	16.1	16.7	17.2	17.8
40	89600			13.1	13.8	14.5	15.1	15.7	16.4	16.9	17.5	
42	94080		12.5	13.3	14.0	14.7	15.3	15.9	16.5	17.1		18.2
44	98560		12.7	13.5	14.2	14.9	15.5	16.1	16.8	17.4	17.9	18.5
46	103040									17.6 17.7	18.1 18.3	
48 50	$107520 \\ 112000$		13.0	13.7	14.0 14.6	15.2	16.9	16.5	17.1	17.7		
	116480			14.0	14.7	15.5	16.2	16.8	17.5	18.1	18.7	19.2
	120960			14.1	14.9	15.7	16.3	17.0	17.6	18.2	18.8	19.4
56	125440			14.3	15.0	15.8	16.5	17.1	17.8	18.4	19.0	19.6
58	129920									18.5		
	134400			14.5	15.3	16.0	16.7	17.4	18.1	18.7	19.3	19.9
	lexion	35	1.4	.45	.5	.55	.6	.65	.7	.75	.8	.85
ın 1	nches.	1	1 -		1	.,,,,					1	

Examples illustrative of the Table:—1 To find the depth of a rectangular bar of cast-iron to support a weight of 10 tons in the middle of its length the deflexion not to exceed 1-40 of an inch per foot in length, and its length 20 feet, also let the depth be six times the breadth.

Opposite six times the weight an under 20 ft. in length is 15.3 inches, the depth, and 1-6 of 15.3 = 2.6 inches, the breadth.

(2). To find the diameter for cast-iron shaft or solid cylinder that will bear a given pressure the flexure in the

middle not to exceed 1-40 of an inch for each foot of its length, the distance of the bearing being 20 ft. and on the

middle equals 10 tons.

Constant multiplier 1.7 for round shafts, then  $10 \times 1.7 = 17$ . and opposite 17 tons and under 20 ft. is 11.2 inches for the diameter. But half that flexure is quite enough for revolving shafts; hence  $17 \times 2 = 34$  tons, and opposite 34 tons is 13.3 inches for the diameter.

Tensile Strength of Metals. Weight necessary to tear asunder one square inch.

Name of Materials.	In pounds Avoirdupois.	1n Tons of 2,000 lbs.
Antimony Cast.	1.060	0,5
Bismuth "	3.250	1.6
Brass, fine yellow cast.	17.968	8.9
" Wire.	49.000	24.5
Copper Cast.	19.000	9[5
Sheets.	30.000	15 0
" Bolts.	33.000	16.5
" Wire.	60.000	30.0
Gun metal.	36.000	18.0
Lead Cast.	1.824	0.9
" Sheet.	3.300	1.6
Steel.	111.500	57,5
Tin Cast.	4.600	2,3
Platinum.	56.000	28.0
Silver.	40.000	20.0
Gold Cast.	20.000	10,0
" Wire.	30.000	15.0
Zinc.	7.500	3,5
Cast-Iron.	20.834	10.4
Wrought-Iron.	56.000	28.0
Cast Steel.	88.600	44.3

## RELATIVE POWER of METAL to RESIST TORISON, WROUGHT-IRON BEING UNITY.

Wrought-Iro	on		-				-			-		-		_		-		1.
Cast-Iron		-		-		-		-			-		-		-		_	.90
Cast-Steel	-		-		-		-		-	-		-		-		_		1.93
Gun Metal		~		-		-		-			-		_		~		_	.27
Brass -	-		-		-		-		-	-		-		_		_		.23
Copper -		-		-		-		-		_	_				_		_	.22
Tin	-		-		-		-		_			_		_		_		.13
Lead -	~	-		-		-		-		-			-		-		-	.10

#### HANDY MECHANICAL,

# Strength of White Pine Struts or Pillars. (Moderately Seasoned).

th:		Dimer	nsions	of Cros	s-Sect	ions in	inches	3.
Length in feet.	$4 \times 5$	4×6		$4\times8$	4×9			$4\times12$
				oad in '				
6 7 8 9 10 11	4.1 3.8 3.5	5.0	5.8 5.3	6.6	7.4 6.8 6.3	8.3 7.5	9.1	9.9
8	3.8	4.5	4.9	5.6	6.3	7.0	8.3	9.0 8.4
9	3.2	3.9	4.6	5.2 4.6	5.9	6.5	7.2	7.8
10	3.2 2.9 2.6	3.5	4.0	4.6	5.2	5.8	6.3	6.9
11	2.6	3.2	3.7	4.2	4.7	5.3	5.8 5.2	6.3
13	2.4 2.0 1.8 1.4 1.1	3.2 2.9 2.4	3.7 3.3 2.8 2.5 1.9	4.2 3.8 3.2 2.8 2.2 1.8 1.6	5.9 5.2 4.7 4.3 3.6 3.2 2.5 2.0	4.0	4.4	5.7 4.8 4.2 3.3
14	1.8	2.1	2.5	2.8	3.2	3.5 2.8 2.3	4.4 3.9	4.2
15	1.4	1.7	1.9	2.2	2.5	2.8	30	3.3
16	1.1	1.4	1.6	1.8	2.0 1.8	$\frac{2.3}{2.0}$	2.5	2.7
12 13 14 15 16 17 18	0.9	1.4 1.2 1.1	1.4 1.2	1.4	1.6	1.8	2.5 2.2 1.9	2.4 2.1
	5×5	5×6	5×7	5×8	5×9	5×10	5×11	5×12
8	5.0	6.0	7.0	8.0 7.5	9.0	10.0	11.0	12.0
9 <b>1</b> 0	4.7	6.0 5.6 5.3 4.9 4.6	6.6	7.5 7.0	9.5 7.4 6.4 5.2 4.1 3.2 2.7	9.4 8.8 8.2 7.6	10.3 9.7	11.3
11	4.4	1 2.5	6.2 5.7 5.3 4.9 4.5	6.6	7.9	8.2	9.0	10.6 9.8
$\frac{11}{12}$	4.1 3.8 3.5	4.6	5.3	6.1	6.8	7.6	8.4	9.1
13 14 15	3.5	4.2 3.8 3.5	4.9	5.6	6.4	1 7 0	7.7	8.4
14	3.2	3.8	4.5	5.1 4.6	5.8	6.4	7.0 6.4	7.7
16	2.6	3.1	3.6	4.2	4.7	6.4 5.8 5.2	5.7	6.2
17	2.3 2.1 1.8	3.1 2.8 2.5	3.2	3.7	4.1	46	5.1	5.5
18	2.1	2.5	2.9	3.4	3.8	4.2 3.6	4.6	5.0
19 20	1.8	$\frac{2.2}{1.8}$	2.9 2.5 2.1	2.9 2.4	3.2 9.7	3.0	$\frac{4.0}{3.2}$	4.3 3.6
20	$6\times5$	6×6	$6\times7$	$6\times8$	6×9	6×10	6×11	$6\times12$
10	6.9	7.1 6.7 6.3 5.9		9.5	10.7	11.8	13.0	14.2
11	5.6	6.7	8.3 7.8 7.4 6.9 6.5 6.2	8.9	10.0	11.2	12.3	13.4 12.6
12 13	5.3 5 0	6.3	7.4	8.4	9.5 8.8	10.5 9.8	11.5 10.8	12.6
14	4.7	5.6	6.5	7.9 7.5		9.0	10.8	11.8 11.2
15	4.4	5.3	6.2	7.1	7.9	9.3 8.8	9.7	10.6
16	4.1	4.9 4.5	5.7	6.5	7.3	8.2	9.0 8.3	9.8
17 18	3.8 3.5	4.5	5.7 4.3 4.9 4.4	5.9 5.6	8.4 7.9 7.3 6.8 6.3 5.7 5.2	8.2 7.5 7.0	8.3 7.7	9.0 8.4
19	$\frac{3.5}{3.2}$	4.2 3.8 3.5	4.4	5.1	5.7	6.4	7.0	7.6
20	3.0	3.5	4.1	4.7	5.2	5.8	6.4	7.0
21	2.6	$\frac{3.1}{2.8}$	3.6	4.1	4.7	5.2	5.7	6.2
22	2.3	2.8	3.3	3.7	4.2	4.7	5.2	5.6

Strength of White Pine Struts or Pillars. (Continued).

(Moderately Seasoned).

Safe load in Tons of 2000 lbs.   10	A		Dimer	sions (	of Cros	s-Secti	ons in	inches	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	e ze	$\frac{1}{7\times5}$							7×12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	nf								•//12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	1 87							194
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	7.2	8.6	10.1	11.5	13.0			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	6.8	8.0	9.5	10.9	12.2	13.6	15.0	16.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	. 13	6.5				11.6	13.0		15.4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14					11.1			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15							12.9	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10			7.0	0.9		10.6		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18			7.0			10.0	11.6	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	4.7	5.6	6.6	7.5	8.5	9.4	10.3	11.2
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	20	4.4	5.2	6.1	7.0	7.8	8.8	9.6	10.4
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	21						8.2		9.8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	22						,		9.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						8×9			8×12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			11.5	13.4		17.2	19.2		23.0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11		10.8	12.6		16.2	18.0	19.8	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12		10.2	11.9	13.6				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			9.7	10.8	12.9				
16     7.0     8.4     9.8     11.2     12.6     14.0     15.4     16.1       17     6.7     8.0     9.4     10.7     12.1     13.4     14.7     16.0       18     6.4     7.7     9.0     10.2     11.5     12.8     14.1     15.       19     6.1     7.4     8.5     9.7     10.9     12.2     13.3     14.8       20     5.8     7.0     8.1     9.3     10.4     11.6     12.8     14.4	15			10.2	11.7		14.6		17.6
17   6.7   8.0   9.4   10.7   12.1   13.4   14.7   16.1   18   6.4   7.7   9.0   10.2   11.5   12.8   14.1   15.4   19   6.1   7.4   8.5   9.7   10.9   12.2   13.3   14.5   14.6   12.8   14.1   15.4   14.5	16	7.0			11.2	12.6	14.0	15.4	16.8
19   6.1   7.4   8.5   9.7   10.9   12.2   13.3   14.8   14.0   12.2   13.3   14.8   14.0   1	17		8.0		10.7			14.7	16.0
20   5.8   7.0   8.1   9.3   10.4   11.6   12.8   14.0	18				10.2				15.4
20   9.8   7.0   6.1   9.3   10.4   11.0   12.8   14.0   15.5   6.6   7.7   9.9   0.0   11.0   19.1   19.5	19	6.1	7.4	8.5	9.7		12.2		
	20	5.5	6.6	7.7	8.8	9.9	11.0	12.8	13.2
22   5.3   6.3   7.4   8.4   9.5   10.6   11.6   12.1	21 22								12.6
								-	$9\times12$
	10						البابنكات		28.6
11   11.0   13.1   15.3   17.6   19.7   22.0   24.1   26.3			13.1	15.3	17.6		22.0	24.1	26.2
12   10.3   12.4   14.4   16.4   18.5   20.6   22.7   24.3				14.4		18.5			24.8
13   9.8   11.7   13.7   15.6   17.5   19.6   21.5   23.4	13	9.8	11.7	13.7		17.5	19.6		23.4
	14			13.0					22.6
	15	8.9	10.7					19.6	21.4
	16		10.2			10.3	16.0	17.0	19.8
18 7.9 9.5 11.1 12.6 14.2 15.8 17.4 19.0 18 7.9 19.5 11.1 12.6 14.2 15.8 17.4 19.0	18	7.9	9.5		12.6	14.7			19.0
18     7.9     9.5     11.1     12.6     14.2     15.8     17.4     19.1       19     7.6     9.1     10.7     12.0     13.7     15.2     16.7     18.3	19	7.6				13.7			18.2
20   7.3   8.7   10.2   11.6   13.1   14.6   16.0   19.4		7.3		10.2	11.6	13.1	14.6	16.0	19.4
21   7.0   8.4   9.8   11.2   12.6   14.0   15.4   17.3	21					12.6			17.8
22   6.8   8.1   9.5   10.8   12.1   13.6   14.9   16.	22	6.8	8.1	9.5	10.8	12.1	13.6	14.9	16.2

Strength of White Pine Struts or Pillars. (Continued).

(Moderately Seasoned).

t.	I	Dimensi	ons of (	cross-Se	ctions i	n inches	5.
egg.	10×6	10×7	10×8	10×9	10×10	10×11	10×12
Length in feet.		Sa	fe load	in Tons	of 2000	lbs.	
10	17.5	20.4	23.4	26.3	29.2	32.1	35.0
$\begin{array}{c} 11 \\ 12 \end{array}$	16.2 15.1	18.9 17.6	$\frac{21.6}{20.0}$	$\frac{24.3}{22.6}$	27.0 25.1	29.7 27.6	32.4
13	14.2	16.6	19.0	21.3	$\frac{23.1}{23.7}$	26.1	32.2 28.4
14	13.5	15.8	18.0	20.3	22.5	24.8	27.0
15	12.9	15.1	17.2	19.4	21.5	23.7	25.8
16 17	12.3 11.8	14.4 13.7	16.4 15.6	18.5 17.6	20.5 19.6	$\frac{22.6}{21.6}$	24.6 23.6
18	11.3	13.1	15.2	17.0	18.9	20.8	22.6
19	10.9	12.7	14.6	16.4	18.2	20.0	21.8
20	10.5	12.2	14.0	15.8	17.5	19.3	21.0
$\begin{array}{c} 21 \\ 22 \end{array}$	10.0 9.6	$\frac{11.7}{11.2}$	13.4 12.8	15.0 14.4	16.7 16.0	18.4 17.6	20.0 19.2
	11×6	11.2 11×7	11×8	11×9	11×10	11×11	13.2   11×12
12	18.0	21.0	24.0	27.0	30.0	33.0	36.0
13	16.9	19.7	22.6	25.4	28.2	31.0	33.8
14	16.0	18.7	21.0	24.0	26.8	29.4	32.0
15 16	15.4 14.7	17.9 17.2	20.4 19.6	23.0 22.0	25.6 24.6	28.1 26.9	30.8 29.4
17	14.2	16.5	18.8	21.2	23.6	25.9	28.4
18	13.5	15.8	18.0	20.3	22.6	24.9	27.0
19	13.0	15.2	17.4	19.5	21.8	23.9	26.0
$\frac{20}{21}$	12.5 12.0	14.6 14.0	16.8 16.0	18.8 18.0	$\begin{array}{c c} 21.0 \\ 20.0 \end{array}$	$\frac{23.0}{22.0}$	25.0 24.0
22	11.6	13.5	15.4	17.4	19.4	21.2	23.2
23	11.2	13.0	14.8	16.7	18.6	20.5	22.4
24	10.8	12.6	14.4	16.2	18.0	19.8	21.6
	12×6	12×7	12×8	12×9	12×10	12×11	12×12
12 13	21.0	$\begin{bmatrix} 24.5 \\ 23.2 \end{bmatrix}$	28.0 26.4	31.5 29.8	35.0	38.5 36.4	42.0 39.7
14	18.8	21.9	25.0	28.1	31.4	34.4	37.6
15	17.9	20.9	23.8	26.8	29.8	32.8	35.8
16	17.1	20.0	22.8	25.7	28.6	31.4	34.2
17 18	16.4 15.7	19.1 18.3	$\frac{21.8}{21.0}$	$24.6 \\ 23.6$	27.4 26.2	30.0 28.8	32.7 31.4
19	15.1	17.6	20.2	22.7	25.2	27.7	30.2
20	14.6	17.0	19.4	21.9	24.4	26.7	29.2
$\frac{21}{22}$	14.1	16.5	18.8 18.2	21.2	23.6	25.8 25.0	28.2
22 23	13.6 13.1	15.9 15.3	18.2	19.6	22.8	$\frac{25.0}{24.0}$	26.2
$\frac{23}{24}$	12.6	14.7	16.8	18.9	21.0	23.1	25.2
-							

The strength of pillars, as well as of beams of timber, depend much on their degree of seasoning.

Well seasoned timber will stand 1½ to 2 times the weight that green timber will. In the same class of timber the slower the growth or the narrower the annular rings the better. In the same class the heavier the better. If the wood has color, deepness of color indicates strength and durability. The freshly-cut surface of wood should be firm, shining, and somewhat translucent. A dull, chalky appearance is a sign of bad timber. In resinous timber, those with least resin in their pores are strongest and most durable. In non-resinous timber, those with least sap or gum are best.

Weight that can be borne with safety by Cast-Iron Columns in 1000 lbs. (Trenton Iron Co).

American Iron.

Length			Diame	eter in 1	inches.	1	
in Feet.	2	3	4	5	6	7	8 -
5 6 7 8 9 10 12 14 16 18 20	12.4 9.4 7.2	36 30 24 20 18	102 88 76 66 56 48 38 28	184 164 146 130 114 102 80 64 52 44	288 264 242 218 198 180 136 122 100 84 72	414 386 360 332 306 282 238 200 170 144 124	560 532 502 470 440 410 354 304 262 226 196
Length			Diame	ter in 1	Inches.	_	
Feet.	9	10	11	12	13	14	15
5 6 7 8 9 10 12 14 16 18 20	728 698 660 630 596 560 494 432 378 332 292	916 884 850 812 774 739 658 586 520 462 410	1126 1082 1056 1016 974 932 846 774 686 616 552	1354 1320 1282 1240 1196 1152 1056 966 878 796 720	1570 1530 1486 1440 1392 1292 1192 1094 1000 912	1798 1754 1706 1656 1550 1440 1332 1228 1130	2086 2040 1992 1940 1828 1712 1596 1482 1372

## SAFE LOAD for HCLLOW CAST-IRON PILLARS. (Tons 2240 lbs).

Thickness	of	$Metal=\frac{1}{2}$ Inch.
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External Diam.		LENG	TH IN FE	ET.	
in Ins.	8	10	12	14	16
3 31/2 4 41/2 5 51/2 6	Tons. 4.0 5.9 8.1 10.6 13.3 15.3 19.0	Tons. 3.2 5.1 6.1 8.1 10.4 12.9 15.5	Tons. 2.3 3.6 4.7 6.5 8.3 10.5 12.7	Tons. 1.8 2.7 3.6 5.0 6.7 8.5 9.5	Tons. 1.4 2.3 3.4 4.4 5.4 7.0 8.7
	Thickr	ness of Met	al=5/8 Inch		
3 31/2 4 41/2 5 51/2 6 61/2 7	4.7 7.1 9.2 12.8 16.1 18.7 23.2 26.9 30.7	3.5 5.3 7.3 9.9 12.7 15.7 19.0 22.4 26.0	2.6 4.2 5.6 7.7 9.1 12.8 15.6 18.7 21.9	2.0 3.2 4.4 6.1 8.1 10.4 12.8 15.2 18.5	1.6 2.5 3.9 5.5 7.0 8.8 10.6 13.0 15.6
	Thic	kness of M	etal=¾ Inc	eh.	
3 31/2 4 41/2 5 51/2 6 61/2 7	5.4 8.1 11.3 14.9 18.8 21.8 27.2 31.6 36.1	3.8 6.2 8.5 11.5 14.8 18.4 22.3 26.3 30.6	2.8 4.4 6.5 8.9 11.7 14.9 18.3 21.9 25.8	2.2 3.5 4.8 7.2 9.0 12.1 15.0 17.8 21.7	1,7 2.6 3.8 6.0 7.7 10.2 12.5 15.3 18.4
	Thi	ckness of M	Ietal=1 Inc	eh.	
4 41/2 51/2 6 61/2 7 71/2 8	13.9 18.5 23.6 27.6 34.5 40.3 46.2 52.2 58.3 70.5	10.4 14.3 18.6 23.2 28.3 33.6 39.1 44.9 50.7 62.7	8.0 11.1 14.8 18.9 23.2 28.0 33.0 38.3 43.8 55.3	6.4 8.8 11.9 15.3 19.1 22.8 27.8 32.6 37.7 48.1	4.8 7.1 9.6 12.7 15.9 19.6 23.6 27.9 32.5 42.3

#### STRENGTH OF ROLLED IRON BEAMS.

Depth	Size of		Spans in	feet.	
of Beam in	Flange	10	15	20	25
Inches.	Inches.	Brea	king Weig	ght in To	ns.
5	2 by 1/2	6.6	1		
6	21/2** 1/2	10. 14.	6.6	5	5
8	3 " 3/2	20.		10	1 8
9	4 " 34	36.	13. 24.	18	14
10	41/2" 1	60.	40.	30	24

Table to show the Weight or Pressure a column of Cast-Iron will sustain with Safety in Cwts. (112 lbs). (English Iron).

Diam.					Heig	ht in	feet	•			
Inches.	4	6	8	10	12	14	16	18	20	22	24
2	72			40	32	26			15	13	11
$21/_{2}$	119	105	91	77		55	47	40	34	29	25
3	178		145		111	97	84	73	64	56	49
31/2	247	232		191	172	156		119	106		83
4	326				242				160	144	130
41/2	418		379		327	301	275	251	229	208	189
5	522	501	479		427	394			310	285	262
5 6 7	607	592	573	550	525				413	386	360
7	1032	1013	989	959	924	887	848	808	765	725	686
8 9	1333	1315	1289	1259	1224	1185	1142	1097	1052	1005	959
9	1716	1697	1672	1640	1603	1561	1515	1467	1416	1364	1311
10	2119	2100	2077	2045	2007	1964	1916	1865	1811	1755	1697
11							2358				
12							2830				

If the columns are hollow, the area to the given diameter is to be converted into the ring, or the difference of the outer and inner diameters multiplied by 23, because hollow Cast-Iron, columns are stronger than solid ones in that proportion.

#### RELATIVE STIFFNESS OF MATERIALS TO RESIST A TRANSVERSE STRAIN.

Cast-Iron.	1. Oak*	195
Ash	.089 White Pine	
Beech	.089 White Pine	}
Elm	.073 Yellow Pine	87

Table of short-linked Crane Chains and Ropes, showing the Dimensions and Weight of each and the proof of the Chain in Tons.

Diameter' of Chains.	Weight per Fathom.	Strain.	Circum. of Rope.	W'g't of Rope per Fathom.
Ins.	l fbs. l	Tons.	Ins.	lbs.
3-16	6.	.75	21/2	1.5
	8.5	1.5	31/4	2.5
- <del>3</del> /8 7-16	11.	2.5	4	3.75
	14.	3.5	43/4	5.
1/ <sub>2</sub> 9-16	18.	4.5	51/2	7.
5/8	24. 28. 30. 36. 44. 50.	5.25	$61/\bar{4}$	8.7
5/8 11-16	28.	6.5	7	10.5
3/4	30.	7.75	71/2	12.
13-16	36.	9.25	81/4	15.
7/8	44.	10.75	9	17.5
15-16	50.	12.5	91/2	19.5
1	56.	14.	10	22.

### APPROXIMATE WEIGHT AND STRENGTH OF MANILLA CORDAGE.

Size	Size	Weight	Length	Strain
Circum'ce		_of_100	of	Borne by
Inches.	Inches.	Fathoms.	One Ib.	New Ropes.
	1	Ibs		l lbs.
3/4	14	15	38 ft.	450
1 ′ *	5-16	25	28 "	750
11/8	- 3/8	29	22 "	900
114	7-16	31	17 "	1,250
11/2	1/2	44	12 "	1,700
13/4	9-16	60	10 ''	2,250
2'	5/8	79	71/2 ''	3,000
21/4	3/4	99	6'-"	4,000
$ \begin{array}{c} \overline{21/2} \\ 23/4 \\ 3 \end{array} $	13-16	122	6 " 5 " 4 "	5,000
$23\overline{4}$	7/8	146	4 "	6,000
3	l ĩ	176	33/8 ''	7,000
31/4	1 1-16	207	3 "	8,500
31/2	11/8	240	21/2 ''	9,500
$33\sqrt{4}$	11/4	275	21-6	11,000
4 '	1 5-16	305	2 "	12,500
41/4	13/8	355	12/3 ''	14,000
41/2	11/2	395	11/2 "	16,000

For Ropes in use deduct one-half from these figures to allow for Chafing, &c.

Relative Value of Various Woods, their Crushing Strength and Stiffness being Combined. Ash, 5. Beech, 4.4 Cedar, 1. Elm, 4.9 English Oak, 5.7 Mahogany, 3.7 Quebec Oak, 4.6 Spruce, 3.6 Sycamore, 2.6 Teak, 9.3 Walnut, 3.2 Yellow Pine 3.

Comparative Weight and Strength of Ropes and Chain Cables length of Cables and Weight of Anchors for Vessels.

Tonnage of Ship's	of	Len'th of Cabl's.	Average Weight per fat- hom.	strain of	Anchor	Approx Equiv't Circum of rope
Tens.	Ins. 1	Fath.	lbs.	Tons.	Cwt.	Ins.
25		120	14	41/2	2	43/4
25 35	1/2 9-16	120	17	51/2	21/2	51/2
45	5/8	120	$\overline{21}$	7'-	234	61/4
50	11-16	120	25	81/2	3	61/4 7
75	3/4	120	30	101/8	31/2	73/4
100	13-16	150	35	1334 18	5	81/2
125	7/8	180	41	18	61/2	91/2
150	15-16	180	48	2234	$7\sqrt{2}$	10
150 175	1	180	54	281/8	9	103/4
200	1 1-16	180	61	34	101/2	111/4
250	11/8	210	68	401/2	121/2	12
300	1 3-16	210	76	471/2	15	123/4
350	11/4	240	84	551/8	17	131/2
400	1 5-16	240	93	631/4	19	141/4
450	13/8	270	102	72	21	15
500 600	1 7-16	270	110	811/4	23	151/2
600	11/2	270	122 132	911/8	26	16
700 •	1 9-16	300	132		30	171/4
800	15/8	300	143		-32	181/2
900	1 11-16	300	154		35	
1000	13/4	300	166		38	
1200	1 13-16	300	178		40	
1400	178	300	191		43	
1600	1 15-16	300	201 217		46	
1800	2 2 1-16	300			48	
2000 2500		300 330	230 244		50	
3000 -	21/8	360	268		53 57	
3000 -	21/4	500	200	l	1 91	1

#### FLAT ROPES.

Jron Wi	re Rope	e Steel W	Rope.	Hemp	Rope.	n. ng ng tbs
Size in	Weigh	Size in	Weight	Size in	Weight	
Inches.	in lbs	Inches	in lbs.	Size in Inches.	per ft. in lbs.	Breal Stra Work Load
21/2×1/2	2 1-5	21/8×3/8	1 2-5	5×11/4	4 1-12	23 ⊨   5.800
3×5/8 4×11-16	23/4	2×1/2	12/3	53/4×11/2		280 7.150
45/8×3/4		31/2×5/8	$\frac{21/2}{31/3}$	$10 \times 21/2$	72/3 101/4	$\begin{array}{c c} 45 =  12.300 \\ 60 =  15.000 \end{array}$

ROUND ROPES.

	n Wire opes.		eel Wire Ropes.	He Ro	mp pe.	Ch	ain.	ing ons.	ng lbs.
Cir-	W'g't per 100	an	W'g't per 100	H H	per eet lbs.	K of	00 Ibs	n T	orki ad L
fer-	feet in	Circum	Feet in	Circum	1007 1051	Size	t.1	Brea	Worl
ence	libs.	0	fbs.	0 1	<b>5</b> = -	[ 005,]	¥±	1 201	
13/4	40	11/2	25	3	63	7-16	183	5	1.666
2	52	15/8	33	5	100	1/2	266	7	2.333
21/4	66	17/8	50	51/2	117	9-16	300	81/2	2.666
21/2 $23/4$	83	2	59	6	130	19-32	341	111	3.700
23/4	110	21/8	67	61/2	145	5/8	400	13	4.300
3	139	23/8	83	71/4	185	11-16	466	15	5.000
33/8	170	21/2	91	8	236	3/4	533	19	6.300
33/4	240	31/8	130	9	297	13-16	650	24	8.000
4	260	33/8	153	91/2	330	7/8	750	28	9.400
41/2	285	31/2	166	101/2	428	1	933	36	12.000

### 

External Diameter.	Thickness.	Bursting per Sq. inch of Internal Surface.	Collapsing per Sq Inch of External Surface.
Ins. 1.25 1.375 1.5 1.625 1.75 1.875 2.125 2.25 2.25 2.75	Ins. .083 .083 .083 .083 .083 .083 .083 .095 .095		
3.25 3.25 3.75 4.25 4.75 4.75 5.25 5.75 6.	.102 .12 .134 .134 .134 .134 .134 .134 .134 .148 .148 .148	4300 4400 4200 3900 3600 3400 3200 3000 2800 2800 2700 2600	3000 2700 2700 2400 2100 1900 1700 1600 1400 1400 1200 1100

Table of Areas and Circumferences from 1 foot to 9 feet (advancing by an inch), or from 1 to 9 Inches (advancing by a twelfth).

(advancing by a twelfth).									
Diam.	Area.	Circum.	Diam.	Area.	Circum.				
1 ft.	.7854	3.1416	5 ft.	19.635	15.708				
1	.9217	3.4034	1 1	20.2949	15.9698				
2	1.069	3.6652	2	20.9658	16.2316				
3	1.2272	3.927	3	21.6476	16.4934				
1 2 3 4 5 6 7 8 9	1.3963	4.1888	1 2 3 4 5 6 7 8	22.3403	16.7552				
5	1.5763	4.4506	5	23.0439	17.017				
6	1.7671	4.7124	6	23.7583	17.2788				
7	1.969	4.9742	7	24.4837	17.5406				
8	2.1817	5.236	8	25.201	17.8024				
9	2.4053	5.4978	9	29.9673	18.0642				
10	2.6398	5.7956	10	26.7254	18.326				
11 '	2.8853	6.0214	11	27.4944	18.5878				
2 ft.	3.1416	6.2832	6 ft.	28.2744	18.8496				
1	3.4088	6.545	1 1	29.0653	19.1114				
2	3.687	6.8068	2	29.867	19.3732				
3	3.9761	7.0686	3	30.6797	19.635				
4	4.2761	7.3304	4	31.5033	19.8968				
2 3 4 5 6 7 8 9	4.5869	7.5922	2 3 4 5 6 7	32.3378	20.1586				
Ď	4.9087	7.854	p	33.1831	20.4204				
7	5.2415	8.1158		34.0394	20.6822				
8	5.5852	8.3776	8	34.9067	20.944				
10	5.9396	8.6394 8.9012	9 10	35,7848	21.2058				
10	6.305 6.814			36.6738	21.4676				
11		9.163 9.4248	11 7 ft.	37.5738	21.7294				
3 ft.	7.0686 7.4668	9.4248		38.4846 39.4064	21.9912 22.253				
1 2 3 4 5 6 7 8 9	7.8758	9.9484	1 2 3 4 5 6 7 8	40.339	22.203				
4	8.2958	10.2102	4	41.2826	22.7766				
2	8.7267	10.472		42.2371	23.0384				
5	9.1685	10.7338	1 5	43.2025	23.3002				
e	9.6211	10.7556		45.2025	23.562				
, P	10.0848	11.2574	1 7	45.1659	23.8238				
é	10.5593	11.5192	6	46.1641	24.0856				
á	11.0447	11.781	9	47.1731	24.0050				
10	11.541	12.0428	10	48.193	24.6092				
11	12.0483	12.3046	<b>i</b> ĭ	49.2238	24.871				
4 ft.	12.5664	12.5664	8 ft.	50.2656	25.1328				
	13.0955	12.8282	1	51.3183	25.3946				
2	13.6354	13.09	2	52.3818	25.6564				
3	14.1863	13.3518	3	53.4563	25.9182				
4	14.7481	13.6136	4	54.5417	26.18				
5	15.3208	13.8754	1 5	55.638	26.4418				
6	15.9043	14.1372	6	56.7451	26.7036				
1 2 3 4 5 6 7 8 9	16.4989	14.499	2 3 4 5 6 7 8 9	57.8632	26.9654				
8	17.1043	14.6608	1 8	58.9923	27.2272				
ğ	17.7206	14.9226	š	60.1322	27.489				
10	18.3478	15.1844	10	61.283	27.7508				
îĭ	18.9859	15.4462	11	62.4448	28.0126				
	-		9 ft.	63.6174	28.2744				

Table of Circumferences, Areas, Squares, Cubes, Square Root, Cube Root, from 1 to 10 Advancing by 1-16 etc.

7: 10:								
Diam. or No.	Circum-  ference.	Area.	Square.	Cube.	Square Root.	Cube Root.		
1	3.14	.785	1.	1.	1.	1.		
1-16	3.34	.886	1.13	1.19	1.031	1.020		
1/2	3.53	.994	1.27	1.42	1.069	1.040		
1/8 3-16	3.73	1.107	1.41	1.67	1.089	1.059		
1/4	3.93	1.227	1.56	1.95	1.118	1.077		
1/4 5-16	4.12	1.353	1.72	2.26	1.146	1.095		
3/2	4.32	1.485	1.89	2.60	1.173	1.112		
3/ <sub>8</sub> 7-16	4.52	1.623	2.07	2.97	1.199	1.129		
1/2	4.71	1.767	2.25	3.38	1.225	1.145		
9-16	4.91	1.917	2.44	3.82	1.250	1.161		
	5.11	2.074	$\tilde{2}.64$	4.29	1.275	1.176		
5/ <sub>8</sub> 11-16	5.30	2.236	$\overline{2.85}$	4.80	1.299	1.191		
3/4	5.50	2.405	3.06	5.36	1.323	1.205		
3/4 13-16	5.69	2.580	3.29	5.95	1.346	1.219		
7/0	5.89	2.761	3.52	6.59	1.369	1.233		
7/8 15-16	6.09	2.948	3.75	7.27	1.392	1.247		
2	6.28	3.142	4.	8.	1.414	1.260		
1-16	6.48	3.341	4.25	8.77	1.436	1.273		
16	6.68	3.547	4.52	9.59	1.458	1.286		
1/8 3-16	6.87	3.758	4.78	10.47	1.479	1.298		
1/4	7.07	3.976	5.06	11.39	1.500	1.310		
1/4 5.16	7.26	4.200	5.35	12.36	1.521	1.322		
36	7.46	4.430	5.64	13.40	1.541	1.334		
3/8 <b>7-1</b> 6	7.66	4.666	5.94	14.48	1.561	1.346		
1/2	7.85	4.909	6.25	15.63	1.581	1.358		
9-16	8.05	5.157	6.57	16.83	1.600	1.369		
5/8	8.25	5.412	6.89	18.08	1.620	1.380		
11-16	8.44	5.673	7.22	19.41	1.639	1.391		
3/4	8.64	5.940	7.56	20.79	1.658	1.402		
13-16	8.84	6.213	7.91	22.25	1.677	1.412		
76	9.03	6.492	8.27	23.76	1.695	1.422		
78 15-16	9.23	6.777	8.63	25.34	1.714	1.432		
3	9.42	7.07	9.	27.	1.732	1.442		
1/8	9.82	7.67	9.77	30.52	1.768	1.462		
1/4	10.21	8.30	10.56	34.32	1.803	1.482		
3/8	10.60	8.95	11.39	38.44	1.837	1.5		
1/2	11.00	9.62	12.25	42.88	1.871	1.518		
5/8	11.39	10.32	13.14	47.63	1.904	1.535		
3/4	11.78	11.05	14.06	52.73	1.936	1.553		
78	12.17	11.79	15.02	58.17	1.968	1.570		
4	12.57	12.57	16.	64.	2.	1.587		
1/4	13.35	14.19	18.06	76.78	$\frac{5}{2.061}$	1.619		
1/2	14.14	15.90	20.25	91.13	2.121	1.651		
$3\overline{4}$	14.92	17.72	22.56	107.16	2.179	1.681		
5	15.71	19.63	25.	125.	2.236	1.710		
1/4	16.49	21.64	27.56	144.70	2.291	1.738		
71	, ==120	,	,00			2.100		

Table of Circum. Areas, Squares, Etc,. (Continued).

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Circum.	Areas.	Square.	Cube.		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	51/2	17.28	23.76	30.25	166.37	2.345	1.765
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3/4	18.06	25.07	33.06	190.11	2.398	1.792
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6	18.85	29.29	36.	216.	2.449	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1/4	19.64	30.68	39.06	244.14	2.500	1.832
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1/2	20.42	33.18	42.25	274.63	2.550	1.866
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$3\overline{4}$	21.21	35.78	45.56	307.55	2.599	1.890
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	21.99	38.48	49.	343.	2.646	1.913
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1/4	22.78	41.28	52.56	381.08	2.692	1.935
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1/2	23.56	44.18	56.25	421.88	2.739	1.957
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	34	24.35	47.17	60.06	465.48	2.784	1.979
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8′	25.13	50.26	64.	512.	2.828	2.
9   28,27   63,62   81,   729,   3,   2,080   1/4   29,06   67,20   85,56   791,45   3,041   2,098   1/2   29,85   70,88   90,25   857,37   3,082   2,118   34   30,63   74,66   95,06   926,86   3,122   2,136	1/4	25.92	53.46	68.06	561.52	2.872	2.021
9   28,27   63,62   81,   729,   3,   2,080   1/4   29,06   67,20   85,56   791,45   3,041   2,098   1/2   29,85   70,88   90,25   857,37   3,082   2,118   34   30,63   74,66   95,06   926,86   3,122   2,136	1/2	26.70	56.75	72.25	614.12	2.915	2.041
9   28,27   63,62   81,   729,   3,   2,080   1/4   29,06   67,20   85,56   791,45   3,041   2,098   1/2   29,85   70,88   90,25   857,37   3,082   2,118   34   30,63   74,66   95,06   926,86   3,122   2,136	$3\overline{4}$	27.49	60.13	76.56	669.92	2.958	2.061
1/4         29.06         67.20         85.56         791.45         3.041         2.098           1/2         29.85         70.88         90.25         857.37         3.082         2.118           34         30.63         74.66         95.06         926.86         3.122         2.136           34         31.41         75.54         100         100         9.16         3.122         2.186           34         31.41         75.54         100         100         9.16         3.122         2.186           34         36.63         74.66         95.06         926.86         3.122         2.186	9	28.27	63.62	81.	729.	3.	2.080
1,5 29.85 70.88 90.25 857.37 3.082 2.118 34 30.63 74.66 95.06 926.86 3.122 2.136 10.2 1.41 78.54 1000 926.86 3.122 2.136	1/4	29.06	67.20	85.56	791.45	3.041	2.098
34 30.63 74.66 95.06 926.86 3.122 2.136	1/2	29.85	70.88	90,25	857.37	3.082	2.118
10 21 41 79 54 100 1000 2 169 2 154	3/4	30.63	74.66	95,06		3.122	2.136
10   31.41   78.54   100.   1000.   3.102   2.154	10	31.41	78.54	100.	1000.	3.162	2.154

TABLE OF CIRCUMFERENCES, AREAS, SQUARES, CUBES, SOUARE ROOT AND CUBE ROOT. Advancing by Decimals from .1 to 10.

Diam. or No.	Circum.	Areas.	Square.	Cube.	Square Root.	Cube Reot.
.1	.314	.00785	.01	.001	.316	.464
.2	.628	.0314	.04	,008	.447	.585
.3	.942	.0706	.09	.027	.548	.669
.4	1.26	.1256	.16	.064	.633	.737
.5	1.57	,1963	.25	.125	.707	.794
.6	1.88	.2827	.36	.216	.775	.843
.7	2.20	.3848	.49	.343	.837	.888
.8	2.51	.5026	.64	.512	.894	.928
.9	2.83	.6362	.81	.729	.949	.965
1.	3.14	.7854	1.	1.	1.	1.
.1	3.46	.9503	1.21	1.33	1.049	1.032
.2	3.77	1.131	1.44	1.73	1.095	1.063
.3	4.08	1.327	1.69	2.20	1.140	1.091
.4	4.39	1.539	1.96	2.74	1.183	1.119
.5	4.71	1.707	2.25	3.37	1.225	1.145
6	5.02	2.011	2.56	4.10	1.265	1.170
.7	5.34	2.270	2.89	4.91	1.304	1.193
.8	5.65	2.545	3.24	5.83	1.342	1.216
.9	5.96	2.835	3.61	6.86	1.378	1.239
2.	6.28	3.142	4.	8.	1.414	1.260
.1	6.59	3.464	4.41	9.26	1.449	1.281
.2	6.91	3.801	4.84	10.65	1.483	1.301

# $TABLE\ OF\ CIRCUMFERENCES,\ AREAS,\ SQUARES,\\ CUBES,\ SQUARE\ ROOT\ AND\ CUBE\ ROOT.$

Advancing by Decimals from .1 to 10. (TABLE CONTINUED).

		(				
Diam. or No.	Circum.	Areas.	Square.	Cube.	Square Root.	Cube Root.
2.3	7.22	4.155	5.29	12.17	1.517	1.320
	7.53					1.020
.4		4.524	5.76	13.82	1.549	1.339
.5	7.85	4.909	6.25	15.63	1.581	1.357
.6	8.16	5.309	6.76	17.58	1.612	1.375
.7	8.48	5.726	7.29	19.68	1.643	1.392
			7.84			
.8	8.79	6.158		21.95	1.679	1.409
.9	9.11	6.605	8.41	24.39	1.703	1.426
3.	9.42	7.069	9.	27. 32.77	1.732	1.442
.2	10.05	7.548	10.24	32.77	1.789	1.474
.4	10.68	8.553	11.56	39.30	1.844	1.504
.7						
.6	11.30	10.18	12.96	46.66	1.897	1.533
.8	11.93	11.34	14.44	54.87	1.949	1.560
_4,	12.56	12.57	16.	64.	2.	1.587
.2	13.19	13.85	17.64	74.09	2.049	1.613
.4	13.82	15.21	19.36	85.18	2.098	1.639
.7		16.62		97.34		
.6	14.45		21.16		2.145	1.663
.8	15.08	18.10	23.04	110.6	2.191	1.687
5.	15.70	19.63	25.	125.	2.236	1.710
.2	16.33	21.24	27.04	140.6	2.280	1.732
.4	16.96	22.90	29.16	157.5	2.324	1.754
.6	17.59	24.63	31.36	175.6	2.366	1.776
.0						
.8	18.22	26.42	33.64	195.1	2.408	1.797
6.	18.84	28.27	36.	216.	2.449	1.817
.2	19.47	30.19	38.44	238.3	2.490	1.837
$\overline{.4}$	20.10	32.17	40.96	262.1	2.530	1.856
$\ddot{.6}$	20.73	34.21	43.56	287.5	2.569	1.876
•0	21.36	36.32	46.24	314.4	0.000	1.895
8					2.608	
7.	21.99	38.48	49.	343.	2.646	1.913
.2	22.61	40.72	51.84	373.2	2.683	1.931
.4	23.24	43.01	54.76	405.2	2.720	1.949
$.\overline{6}$	23.87	45.36	57.76	439.	2.757	1.966
.8	24.50	47.78	60.84	474.6	2.793	1.983
0						
8.	25.13	50.27	64.	512.	2.828	2.
.2	25.76	52.81	67.24	551.4	2.864	2.017
.2	26.38	55.42	77.56	592.7	2.898	2.033
.6	27.01	58.09	73.96	636.1	2.933	2.049
.8	27.64	60.82	74.44	681.5	2.966	2.065
9.	28.27	63.62	81.	729.	3.	2.080
<i>J</i> .				778.7	3.033	2.095
.2	28.90	66.48	84.64			
.4	29.53	69.40	88.36	830.6	3.066	2.110
,6	30.15	72.38	92.16	884.7	3.098	2.125
.8	30.78	75.43	96.04	941.2	3.130	2.140
10.	31.41	78.54	100.	1000.	3.162	2.154
20.				1 20001		

Tables of Diameters, Areas, Circumferences of Circles, Squares, Cubes, Square Root, Cube Root, and Reciprocals of Numbers (From 1 to 250).

	of Numbers (From 1 to 250).								
No.	Cir.		Sq're.	Cube.	S.Root.		Recip.		
1	3.14	0.79	1	1	1.000	1.000	1.00000		
2 3 4 5 6 7	6.28	3.14	4	8	1.414	1.260	.50000		
3	9.42	7.07	9	27	1.732	1.442	.33334		
4	12.57	12.57	16	64	2.000	1.587	.25000		
5	15.71	19.62	25	125	2.236	1.710	.20000		
6	18.85	28.27	36	216	2.450	1.817	.16667		
7	21.99	38.48	49	343	2.646	1.913	.14285		
8 9	25.13	50.27	64	512	2.828	2.000	.12500		
	28.27	63.62	81	729	3.000	2.080	.11112		
10	31.41	78.54	100	1000	3.162	2.154	.10000		
11	34.56	95.03	121	1331	3.317	$2.224 \\ 2.289$	.09091		
12	37.70	113.10	144	1728	3.464	2.289	.08333		
13	40.84	132.73	169	2197 2744	3.605	2.351 2.410	.07692		
14 15	43.98 47.12	153.94 176.72	196 225	3375	3.741 3.872	2.410	.07142		
10	50.27	201.06	256	4096	4.000		.06250		
16 17	53.41	226.98	289	4913	4.123	2.519 $2.571$	.05882		
18	56.55	254.47	324	5832	4.125	$\frac{2.571}{2.620}$	.05556		
19	59.69	283.53	361	6859	4.358	2.668	.05263		
19	62.82	314.15	400	8000	4.472	2.000	.05203		
20 21	65.97	346.36	441	9261	4,582	2.714 2.758	.04761		
22	69.12	380.13	484	10648	4.690	2.802	.04545		
23	72.26	415.48	529	12167	4.795	2.843	.04347		
24	75.40	452.39	576	13824	4.898	2.884	.04167		
25	78.54	490.87	625	15625	5.000	2.001	.04000		
26	81.68	530.93	676	17576	5.099	$\begin{vmatrix} 2.924 \\ 2.962 \end{vmatrix}$	.03846		
27	84.82	572.56	729	19683	5.196	3.000	.03703		
<b>2</b> 8	87.96	615.75	784	21952	5.291	3.036	.03571		
29	91.11	660.52	841	24389	5.385	3.072	.03448		
30	94.25	706.86	900	27000	5.477	3.107	.03334		
31	97.36	754.77	961	29791	5.567	3.141	.03225		
32	100.53	804.25	1024	32768	5.657	3.174	.03125		
33	103.67	855.30	1089	35937	5.744	3 207	.03031		
34	106.82	907.92	1156	39304	5.830	3.239	.02941		
35	109.96	962.11	1225	42875	5.916	3.239 3.271 3.301	.02857		
36	113.10	1017.88	1296	46656	6.000	3.301	.02666		
37	116.24	1075.21	1369	50653	6.082	1 3.332	.02702		
38	119.38	1134.11	1444	54872	6.164	3.361	.02631		
39	122.52	1194.59	1521	59319	6.244	3.391	.02564		
40	125.66	1256.64	1600	64000	6.324	3.419	.02500		
41	128.81	1320.25	1681	68921	6.403	3.448	.02439		
42	131.95	1385.44	1764	74088	6.480	3.476	.02380		
43	135.09	1452.20	1849	79507	6.557	3.503	.02325		
44	138.23	1520.53	1936	85184	6.633	3.530	.02272		
45	141.37	1590.43	2025	91125	6.708	3.556	.02222		
46	144.51	1661.90	2116	97336	6.782	3.583	.02173		
47 48	147.66	1734.94	2209	103823	6.856	3.609	.02127		
48 49	150.80	1809.56	2304	110592	6.928	3.634	.02083		
50	153.94 157.08	1885.74 1963.50	2401 2500	117649	7.000	3.659	.02040		
90	1 101.00	1300.00	1 2000	125000	7.071	+3.684	1.02000		

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

No.	Cir.	Areas.	Sq're.	Cube.	S.Root.	C.R't.	Recip.
51	160.22	2042.82	2601	132651	7.141	13.708	.01960
52	163.36	2123.72	2704	140608	7.211	3.732	.01923
* 53	166.50	2206.18	2809	148877	7.280	3.756	.01886
54	169.65	2290.22	2916	156464	7.348	3.779	.01851
55	172.79	2375.83	3025	166375	7.416	3.802	.01818
56	175.93	2463.01	3136	175616	7.483	3.825	.01785
57	179.07	2551.76	3249	185193	7.549	3.848	.01754
58	182.21	2642.08	3364	195112	7.615	3.870	.01724
59	185.35	2733.97	3481	205379	7.681	3.892	.01694
60	188.50	2827.43	3600	216000	7.746	3.915 3.936	.01667
61	191.64	2922.47	3721	226981	7.810	3.936	.01639
62	194.78	3019.07 3117.25	3844	238328	7.874	3.957 3.979	.01612
63	196.94	3117.25	3969	250047	7.936	3.979	.01587
64	201.06	3216.99	4096	262144	8.000	4.000	.01562
65	204.20	3318.31	4225	274625	8.062	4.020	.01538
66	207.35	3421.19	4356	287496	8.124	4.041	.01515
67	210.49	3525.65	4489	300763	8.185	4.061	.01492
68	213.63	3631.68	4624	314432	8.246	4.081	.01470
69	216.77	3739.28	4761	329509	8.306	4.101	.01449
70	219.91	3848.45	4900	343000	8.367	4.121	.01428
71	223.05	3959.19	5041	357911	8.426		.01408
72 73	226.19 $229.34$	4071.50 4185.09	5184 5329	373248 399017	8.485	4.160	.01389
74	234.48	4300.84	5476	405224	8.602	4.179	.01351
75	235.62	4417.86	5625	421875	8.660	4.217	.01333
76	238.76	4536.46	5776	438976	8.717	4.235	.01315
77	241.90	4656.63	5929	456533	8.775	4.254	.01298
78	245.04	4778.36	6084	474552	8.831	4.272	.01282
79	248.19	4901.67	6241	493039	8.888	4.290	.01265
80	251.33	5026,55	6400	512000	9.944	4.309	.01250
81	254.47	5153.00	6561	531441	9.000	4.326	.01234
82	257.61	5281.02	6724	551368	9.055	4.344	.01219
83	260.75	5410.61	6889	571787	9.110	4.362	.01204
84	263.89	5541.77	7056	592704	9.165	4.379	.01190
85	267.04	5674.50	7225	614125	9.219	4.396	.01176
86	270.18	5808.80	7326	636056	9.273	4.414	.01162
87	273.32	5944.68	7569	658503	9.327	4.431	.01149
88	276.46	6082.12	7744	681472	9.380	4.447	.01136
89	279.60	6221.44	7921	704969	9.433	4.461	.01123
90	282.74	6361.72	8100	729000	9.487	4.481	.01111
91	285.89	6503.88	8281	753571	9.539	4.497	.01098
92	289.03	6647.61	8464	778688	9.591	4.514	.01086
93	292.17	6792.91	8649	804357	9.643	4.530	.01075
94	297.31	6939.78	8836	830584	9.695	4.546	.01063
95	298.45	7088.22	9025	857375	9.746	4.562	.01052
96	301.59	7238.23	9216	884736	9.797	4.578	.01041
97	304.73	7389.81	9409	912673	9.848	4.594	.01030
98	307.87	7542.96	9604	941192	9.899	4.610	.01020
99	311.02	7697.69	9801	970299	9.949	4.626	.01010
100	314.16	7853.98	10000	1000000	10.000	4.642	.01000

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

No.	Cir.	Areas.	Sa're.	Cube.	S.Root.	C P't	Regin
	317.30	8011.85	10201	1030301	10.049	4.657	,00990
$\frac{101}{102}$	320.44	8171.28	10404	1061208	10.049	4.672	.00990
102	323.58	8332.29	10609	1092727	10.033	4.687	.00970
103	326.73	8494.87	10816	1124864	10.148	4.702	.00970
105	329.87	8659.01	11025	1157625	10.196	4.717	.00951
	333.01	8824.73	11236	1191016	10.240	4.732	.00932
106 107		8992.02	11449	1225043	10.255	4.747	
107	336.15 339.29	9160.88	11664	1259712	10.392	4.762	.00933
	342.43	9331.32	11881	1295029	10.332	4.776	.00923
109		9503.32	12100	1331000	10.440	4.791	.00917
110	345.58			1367631	10.400	4.806	.00909
111 112	348.72 351.86	9676.89 9852.03	12321	1404928	10.583	4.820	.00892
		10028.75	12544 12769		10.5630	4.834	.00884
113	355.00		12709	1442897	10.650		
114 115	358.14 361.28	10207.03	13225	1481544		4.848	.00877
		10386.89		1520875	10.723	4.862	.00869
116	364.42	10568.32	13456	1560896	10.770	4.876	.00862
117	367.56	10751.32	13689	1601613	10.816	4.890	.00854
118	370.70	10935.88	13924	1643032	10.862	4.904	.00847
119	373.85	11122.02	14161	1685159	10.908	4.918	.00840
120	376.99	11309.73	14400	1728000	10.954	4.932	.00834
121	380.13	11499,10	14641	1771561	11.000	4.946	.00826
122	383.27	11689.87	14884	1815848	11.045	4.959	.00819
123	386.41	11882.29	15129	1860867	11.090	4.973	.00813
124	389.56	12076.28	15376	1906624	11.135	4.986	.00806
125	392.70	12271.85	15625	1953125	11.180	5.000	.00800
126	395.84	12468.98	15876	2000376	11.224	5.013	.00793
127	398.98	12667.69	16129	2048383	11.269	5.026	.00787
128	402.12	12867.96	16384	2097152	11.314	5.039	.00781
129	405.27	13069.81	16641	2146689	11.357	5.052	.00775
130	408.41	13273.23	16900	2197000	11.401	5.065	.00769
131	411.55	13478.22	17161	2248091	11.445	5.078	.00763
132	414.69	13684.78	17424	2299968	11.489	5.091	.00757
133	417.83	13892.91	17689	2352637	11.532	5.104	.00751
134	420.97	14102.61	17956	2406104	11.575	5.117	.00746
135	424.12	14313.88	18225	2460375	11.618	5.129	.00740
136	427.26	14526.72	18496	2515456	11.661	5.142	.00735
137	430.40	14741.14	18769	2571353	11.704	5.155	.00729
138	433.54	14957.12	19044	2600872	11.747	5.166	.00724
139	436.68	15174.68	19321	2685619	11.789	5.180	.00719
140	439.82	15393.81	19600	2744000	11.832	5.192	.00714
141	442.96	15614.50	19881	2803221	11.874	5.204	.00709
142	446.11	15836.77	20164	2863288	11.916	5.217	.00704
143	449.25	16060.61	20449	2924207	11.958	5.229	.00699
144	452.39	16286.02	20736	2985984	12.000	5.241	.00694
145	455.53	16513.00	21025	3048625	12.041	5.253	.00689
146	458.67	16741.55	21316	3112136	12.083	5.265	.00684
147	461.81	16971.67	21609	3176523	12.124	5.277	.00680
148	464.96	17203.36	21904	3241792	12.165	5.289	.00675
149	468.10	17436.62	22201	3307949	12.206	5.301	.00671
150	471.24	17671.46	22500	3375000	12.247	5.313	1.00667

Tables of Diameters, Areas, Circumfer'ces, etc., (Continued).

						, (00,,,,,	
No.			Sq're.		S.Root.	-	
151	474.38	17907.86	22801	3442951	12.288	5.325	.00662
152	477.52	18145.84	23104	3511808	12.328	5.336	.00657
153	480.66	18385.39	23409	3581577	12.369	5.348	.00653
154	483.81	18626.50	23716	3652264	12.409	5.360	.00649
155	486.95	18869.19	24025	3723875	12.449	5.371	.00645
156	490.09	19113.45	24336	3796416	12.489	5.383	.00641
157	493.23	19359.28	24649	3869893	12.529	5.394	.00636
158	496.37	19606.68	24964	3944312	12.569	5.406	.00632
159	499.51	19855.65	25281	4019679	12.609	5,417	.00628
160	502.65	20106.19	25600	4096000	12.649	5.428	.00625
161	505.80	20358.31	25921	4173281	12.688	5.440	.00621
162	508.94	20611.99	26244	4251528	12.727	5.451	.00617
163	512.08	20867.19	26569	4330747	12.767	5.462	.00613
164	515.22	21124.07	26896	4410944	12.806	5.473	.00609
165	518.36	21382.47	27225	4492125	12.845	5.484	.00606
166	521.50	21642.43	27556	4574296	12.884	5.495	.00602
167	524.65	21904.0	27889	4657463	12.922	5.506	.00598
168	527.79	22167.1	28224	4741632	12.961	5.517	.00595
169	530.93	22431.8	28561	4826809	13.000	5.528	.00591
170	534.07	22698.0	28900	4913000	13.038	5.539	.00588
171	537.21	22965,8	29240	5000211	13.076	5.550	.00584
172	540.36	23235.2	29584	5088448	13.114	5.561	.00581
173	543.50	23506.2	29929	5177717	13.152	5.572	.00578
174	546.64	23778.7	30276	5268024	13.190	5.582	.00574
175	549.78	24052.8	30625	5359375	13.228	5.593	.00571
176	552.92	24328.5	30976	5451776	13.266	5.604	.00568
177	556.06	24605.7	31329	5545233	13.304	5.614	.00564
178	559.20	24884.6	31684	5639752	13.341	5.625	.00561
179	562.34	25164.9	32041	5735339	13.379	5.635	.00558
180	565.49	25446.9	32400	5832000	13.416	5.646	.00555
181	568.63	25730.4	32761	5929741	13.453	5.656	.00552
182	571.77	26015.5	33124	6028578	13.490	5.667	.00549
183	574.91	26302.2	33489	6128487	13.527	5.677	.00546
184	578.05	26590.4	33856	6229504	13.564	5.687	.00543
185	581.19	26880.3	34225	6331625	13.601	5.698	.00540
186	584.34	27171.6	34596	6434856	13.638	5.708	.00537
187	587.48	27464.6	34969	6539203	13.674	5.718	.00534
188	590.62	27759.1	35344	6644672	13.711	5.728	.00531
189	593.76	28055.2	35721	6751269	13.747	5.738	.00529
190	596.90	28352.9	36100	6859000	13.784	5.748	.00526
191	600.04	28652.1	36481	6967871	13.820	5.758	.00523
192	603.19	28952.9	36864	7077888	13.856	5.768	.00520
193	606.33	29255.3	37249	7189057	13.892	5.778	.00518
194	609.47	29559.2	37636	7301384	13.928	5.788	.00515
195	612.61	29864.8	38025	7414875	13.964	5.798	.00512
196 197	615.75	30171.9	38410	7529536	14.000	5.808	.00510
	618.89	30480.5	38809	7645373 7762392	14.035	5.818 5.828	.00507
198 199		30790.7 31102.6	39204 39601	7880599	14.071	5.838	.00505
	$\begin{vmatrix} 625.18 \\ 628.32 \end{vmatrix}$	31415.9	40000	8000000	14.106	5.848	.00502
200	1 028.32	51410.9	1 40000	1 0000000	14.142	0.048	000000

Tables of Diameters, Areas, Circumferices, etc., (Continued).

Tab	les of Di	ameters,	Areas,	Circumfer	ces, etc.	, (Cont	nuea).
No.	Cir.	Areas.	Sq're.		S.Root.		Recip.
201	631.46	131730.9	40401	8120601	14.177	5.857	.00497
202	634.60	32047.4	40804	8242408	14.212	5.867	.00495
203	637.74	32365.5	41209	8365427	14.247	5.877	.00492
204	640.88	32685.1	41616	8489664	14.282	5.886	.00490
205	644.03	33006.4	42025	8615125	14.317	5.896	.00487
206	647.17	33329.2	42436	8741816	14.352	5.905	.00485
207	650.31	33653.5	42849	8869743	14.387	5.915	.00483
208	653.45	33979.5	43264	8998912	14.422	5.924	.00480
209	656.59	34307.0	43681	9123329	14.456	5.934	.00478
210	659.63	34636.1	44100	9261000	14.491	5.943	.00476
211	660 07	34966.7	44521	9393931	14.525	5.953	.00473
212	666.01	35298.9	44944	9528128	14.560	5.962	.00471
213	669.16	35632.7	45369	9663597	14.594	5.972	.00469
214	672.30	35968.1	45796	9800344	14.628	5.981	.00467
215	675.44	36305.0	46225	9938375	14.662	5.990	.00465
216	678.58	36643.5	46656	10077696	14.696	6.000	.00462
217	681.73	36983.6	47089	10218313	14.730	6.009	.00460
218	684.87	37325.3	47525	10360232	14.764	6.018	.00458
219	688.01	37668.5	47961	10503459	14.798	6.027	.00456
220	691.15	38013.3	48400	10648000	14.832	6.036	.00454
221	694.29	38359.6	48841	10793861	14.866	6.045	.00452
222	697.43	38707.6	49284	10941048	14.899	6.055	.00450
223	700.57	39057.1	49729	11089567	14.933	6.064	.00448
224	703.71	39408.1	50176	11239424	14.966	6.073	.00446
225	706.86	39760.8	50625	11390625	15.000	6.082	.00444
226	710.00	40115.0	50876	11543176	15.033	6.091	.00442
227	713.14	40470.8	51529	11697083	15.066	6.100	.00440
228	716.28	40828.1	51984	11852352	15.099	6.109	.00438
229	719.42	41187.1	52441	12008989	15.132	6.118	.00436
230	722.57	41547.6	52900	12167000	15.165	6.126	.00434
231	725.71	41909.6	53361	12326391	15.198	6.135	.00432
232	728.85	42273.3	53824	12487168	15.231	6.144	.00431
233	731.99	42638.5	54289	12649336	15.264	6.153	.00429
234	735.13	43005.3	54756	12812904	15.297	6.162	.00427
235	738.27	43373.6	55225	12977874	15.329	6.171	.00425
236	741.42	43743.5	55696	13144256	15.362	6.179	.00423
237	744.56	44145.8	56169	13312053	15.394	6.188	.00421
238	747.70	44488.1	56644	13481272	15.427	6.197	.00420
239	750.84	44862.7	57121	13651919	15.459	6.205	.00418
240	753.98	45238.9	57600	13824000	15.491	6.214	.00416
241	757.12	45616.7	58081	13997521	15.524	6.223	.00414
242	760.27	45996.1	58564	14172488	15.556	6.231	.00413
243	763.41	46377.0	59049	14348907	15.588	6.240	.00411
244	766.55	46759.5	59536	14526784	15.620	6.248	.00409
245	769.69	47143.5	60025	14706125	15.652	6.257	.00408
246	772.83	47529.2	60516	14886936	15.684	6.265	.00406
247	775.96	47916.4	61009	15069223	15.716	6.274	.00404
248	779.11	48305.1	61504	15252992	15.748	6.282	.00403
249	782.26	48695.5	62001	15438249	15.779	6.291	.00401
250	785.40	49087.4	62500	15625000	15.811	6.299	.00400

TABLE of AREAS of SQUARES and CIRCLES, SIDE of SQUARE both in DECIMALS and FRACTIONS.

From 1-16 to 12.

F 1011t 1-10 to 12.									
Diam.	Area	Area	Side of	Square.					
	of □ in Ins,	in O Ins.	In decim'ls.	In fracti'ns.					
12	.0039	.0031	.0553	16 in. 15 " 128 "					
į	.0156 .0351	.0123	.1108 .1662	15 "					
3 16	.0351	.0276	.1662	100					
14	.0625	.0491	.2216	77 "					
10 00 14 6 00 00 00 00 10 00 00 00 00 00 00 00 00	.0976	.0767	.2769						
38	.1406	.1104	.3325	• 21 ••					
16	.1406 .1914 .25	·1503	.3877	7 66					
2	.3166	*.1963	.4431	17.0					
ฐัช		.2485	.4985	1 " 2 35 " 64 77 " 128					
¥	.3906 .4727	.3068 .3712	.5539 .6093	64					
16	.5625	.4418	.6646	128					
7 13	.6603	.5185	.72	31 44 32					
76	.7656	.6013	.7754	49 66					
8 15	.879	.6903	.8308	64					
116	1.	.7854	.8862	7 66					
	1.129	.8868	.9416	8 66					
16 96 14 56 688 7 1 2 9 6 6 1 6 8 4 1 7 7 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1.266	.994	.997	63 "					
3.	1.409	1.107	1.052	04					
į	1.562	1.227	1.108	1.7 "					
5 16	1.723	1.353	1.163						
38	1.891	1.485	1.218	137 "					
176	2.067	1.623	1.274	121 66					
· 2	2.25	1.767	1.329	121 "					
<u>ร</u> ัธ	2.439	1.916	1.385	17 "					
ž	$2.641 \\ 2.864$	2.764	1.44	176 "					
16	3,063	$2.25 \\ 2.405$	1.495 1.551	135 ((					
13	3.287	2.581	1.606	139 (1					
16 7	3.516	2.761	1.661	121 4					
15	3.752	2.948	1.717	123 "					
216	4.	3.142	1.772	1354 " 1354 " 1364 " 1362 " 13722 " 13722 "					
	4.516	3.546	1.883	<b>-</b> 32					
i	5.062	3,976	1.994	163 "					
3	5.640	4.430	2.105	267 "					
1/2	6.25	4.908	2.215	27 "					
58	6.889	5.412	2.326	251 "					
-(a -(4 0)0 -(2 10)0 0)47-10	7.56	5.939	2.437	2,7					
78	8.264	6.492	2.548	235 "					
3 ,	9.	7.069	2.659	231 "					
8.	9.764	7.67	2.769	235 "					
3	10.561	8.296	2.88	263 "					
- CONTROLS	11.388 12.25	8.946 9.621	2.991 3.102						
2	12.20	9.021	3.102	3 7 "					

TABLE OF AREAS OF SQUARES and CIRCLES, SIDE OF SQUARE both in DECIMALS and FRACTIONS.

(Continued).

		(0011111111		
Diam.	Area	Area	Side of	Square.
	of $\square$ in Ins,	in O Ins.	In decim'ls.	In fracti'ns.
35834478	13.138	10.321	3.213	37 in. 321 ···
3	14.065	11.045	3.323	321 "
Ž	15.01	11.793	3.434	3.7 "
48	16.	12,566	3.545	335 "
	17.012	13.364	3.656	321 "
i	18.058	14.186	3.766	349 "
3	19.141	15.033	3.877	37 "
î	20.254	15.904	3.987	363 "
14(R 144 D)B 14(P 15)B D)4(P 15)	21.385	16.8	4.098	47 "-
3	22.556	17.721	4.208	4.7. "
7	23,748	18,655	4.321	421 "
5°	25.	19.635	4.431	47 "
	26.26	20.629	4.542	435 "
ĩ	27.557	21.648	4.653	421 66
3	28,884	22.69	4.764	449 "
î	30.25	23.758	4.875	47 "
5	31.641	24.851	4.985	463 "
16143612563476	33.06	25.967	5.096	532 "
7	34.516	27,109	5.317	513 "
6	36.	28.274	5,207	521 "
1	39.063	30.679	5.538	564 517 532
14 1 2 3 4	42.25	33.183	5.76	53 "
. 3	45.562	35.785	5.982	563 "
7	49.	38.485	6.203	67 "
1	52.562	41.282	6.425	627 "
14 12 3	56.25	44.179	6.646	641 "
34	60.062	47.173	6.868	655 "
8	64.	50.266	7.09	73 "
14	68.062	53.456	7.311	75 "
14 15 34	72.25	56.745	7.533	7.7. "
34	76.562	60.132	7.754	749 "
9	81.	63.617	7.976	763 "
4	85.563	67.201	8.198	813 "
1 1 2 3 4	90.25	70.882	8.419	827 "
3 4	95.062	74.662	8.641	841 "
10	99.98	78.54	8.862	855 "
14 12 34	105.04	82.516	9.084	911 "
- 1/2	110.23	86.59	9.304	919 "
34	115.55	90.763	9.527	984
11]	121.	95.033	9.748	93 "
4	126.54	99.402	9.975	10 "
. 1/2	132.22	103.87	10.19	1013 "
104	138.06	108.43	10.42	1013 "
12	144.	113.1	10.64	1041 "

### ELECTRICITY.

### Conductors.

Most Perfect.

All known Metals. Well-burned Charcoal. Plumbago.

Burning Gaseous Matter or flame.

Smoke.

Less Perfect.

Concentrated Acids.
Dilute. Acids
Saline Fluids.
Living Animals.
" Vegetables.

Wood, in the ordinary state

Snow, and Ice from 32° to 0° Water.

Imperfect.

Common Earth and Stone.

Dry Chalk and Lime. Marble and Porcelain. Paper.

Alkaline matter. Aqueous vapor. Non-Conductors.

Less Perfect.

Ice at 0° Farht. Dry Vegetable sub-

stances.
Dry Animal substan-

ces generally.
Parchment, Leather,
Feathers.

Baked Wood. [ces. Oil and Fatty substan-Silk.

Most Perfect.

Fur and Hair.

Dry gases including air. Pure Steam of highpressure.

Glass and all [vitrifac-

Diamonds and transparent Gems.

Talc.
Amber.
All Resinous Bodies.

Brimstone.
Shell-lac.
Bees-Wax.

The following is a short list of substances which may be used to receive the deposit of metal.

In all metallic solutions, acid,

Silver. In all alkaline, in all but the preceding,

Copper. do. do. do. Lead. do. do. do. Bismuth. do. do. do. Antimony. do. do. do. Tin. do. do. do. Iron. do. do.

Zinc. In some alkaline and acid.

NON-METALLIC SUBSTANCES.

In all saline or acid solutions; but not in alkaline. Sealing Wax. White Wax. Bees Wax and Rosin, Stearine, Spermaceti, Plaster of Paris prepared, some Animal substances. Most vegetables substances.

## DEPOSITION of METALS. GOLD BATHS.

### FOR SILVER, COPPER, or ALLOYS RICH IN THESE.

Distilled water, 1 gallon.
Phosphate of soda, cryst,
Bisulphite of soda 1 3-5 "
Cyanide of potassium, pure,
Gold Chloride, 160 grains,

Dissolve in a portion of the water, heated, phosphate of soda. Dissolve in another portion of the water the bisulphite of soda and cyanide of potassium. Dissolve the gold choloride in the remaining water, stir the solution slowly into the cold phosphate of soda solution, and finally add the solution of cyanide bisulphite. The bath, now ready for use, should be colorless. Used at a temperature of from 120° to 175° Fah.

### BATH FOR IRON OR STEEL UNCOATED.

Distilled water
Phosphate of Soda,
Bisulphite of Soda.
Cyanide of potassium, pure.
Gold chloride.

1 gallon.
7 4-5 oz.
9 4-5 oz.
9 4-5 oz.
160 grains.

Dissolve as before. Heat to 175° or 180° Fah. Pass the second metal through the hot potash, then through dilute muriatic acid (acid 1, water 15), brush, and connect at once. Requires a very intense current at first.

### COLD ELECTRIC-GILDING BATH.

Water, distilled.
Potassium Cyanide, pure.
Gold Chloride.

1 gallon.
3 1-5 oz.
3 1-10 "

Dissolve the Cyanide in a part of the water, then gradually add the gold chloride dissolved in the remainder. Boil for half an hour before using. (Use cold).

### ZINC BATH.

Zinc is used for the preservation of iron, by electro-depostion. The iron is first rendered perfectly clean and free from oxide, by placing it in a bath of heated sulphuric acid and water; then in a cold solution of sulphate of zinc. The positive pole of a galvanic battery is attached to a zinc plate, and the negative to the iron to be covered; the pure metal is deposited, and the zinc and the iron are amalgamated.

#### PLATINUM.

The best solution to be employed is the nitro-muriate of platinum, to which sufficient soda is added to render it neutral. The object to be coated should be smooth, and thoroughly cleansed by potash before the process is com-

menced. Having proceeded thus far, and the solution of platinum being ready, a fine platinum wire in connection with the silver or positive pole of the battery, must be placed so as to dip into the solution, but must not be immersed beyond a very short distance. The object to be platinated is now ready for connection with the zinc or negative pole of the battery; after this is effected it is to be dipped in the solution.

### SILVER BATH.

For electro-silver plating the double salt of silver and potassium cyanide is almost universally employed. The following are the proportions viz:

Water (soft), Cyanide of Potassium (pure), Nitrate of Silver,

Dissolve the nitrate of silver in a sufficient quantity of pure water (soft), and add to it gradually, with constant stirring hydrocyanie (prussie) acid until all the silver has been precipitated as cyanide, which may be known by the formation of no cloud in a portion of the clear liquid when a drop of the acid is added to it, avoid adding an excess of the acid. Throw the precipitate upon a fine cotton cloth filter, and as the liquid runs through wash the precipitate on the cloth several times with pure water. Dissolve the cyanide of potassium in the water, and stir in the cyanide of silver carefully removed from the cloth. If it does not dissolve in the liquid entirely, add more cyanide of potassium until it does, stirring continually. Let the impurities settle, and the bath is ready for use.

### NICKEL BATH.

The nickel salts commonly used are the nickel ammonium sulphate (called double sulphate) and the corresponding chloride, Other salts, such as the nickel potassium cyanide, the acetate and sulphate, have been used, but not successfully as these.

The double sulphate bath may be prepared by dissolving three-fourths of a pound of the salt in each gallon of water, (soft). It should be kept neutral and up to about six

degrees of hydrometer.

The double chloride bath requires about four ounces of the salt per gallon, and works better slightly acid, the tendency in working being towards alkalinity. The bath should be filtered when freshly prepared, and should be kept in a separate room, or at least away from the apartment in which the buffing or polishing is performed, to avoid contamination by dust as much as possible. Exposed to the air the bath (the water) evaporates, and the water thus lost must be replaced from time to time. Keep out dust as much as possible. It is well to cover the bath when not in use.

#### BRASS BATH.

Where the ordinary cheap commercial cyanide is employed the following answers very well:

Sulphate of Copper, 4 oz. Sulphate of Zinc, 4 to 5 ": 1 gal.

Dissolve and precipitate with 30 ounces of carbonate of soda; allow to settle, and decant the clear liquid, and wash the precipitate several times with fresh water—after as many settling add to the washed precipitates:

Carbonate of Soda, 15 oz. Bisulphite of Soda, 71/2."
Water, 1 gal.

Stir to effect solution of these last two, then stir in ordinary cyanide of potassium until the liquid becomes clear and colorless. Filter if much iron or iron oxide (derived from impure zinc salt and cyanide) remains suspended in the liquid. An additional half ounce or so of the cyanide improves the conductivity of the solution.

### COLD BRASS BATH FOR ALL METALS.

Carbonate of Copper (recently prepared). 2 oz. Corbonate of Zinc, 2 oz. Carbonate Soda 4 oz. Bisulphite of Soda, 4 oz. Cyanide of Potassium (pure), 4 oz. Arsenious Acid, 1-20 oz. Water, 1 gal.

Filter if necessary.

The arsenious acid is added to brighten the deposit, an excess is apt to give the metal a grayish-white color.

### STEEL BATH.

In order to render copper-plates, which are used in printing, more durable, they can be covered with an electrolytic deposit of iron, which possesses an unusual degree of hardness, almost superior to steel. The salt usually employed has been the double sulphate of iron and ammonia. Professor Böttger, who first used this combination of salts in the process, has recently devised an improvement in the bath employed. He dissolves ten parts of ferrocyanide potassium (yellow prussiate of potash) and twenty parts of the double tartrate of soda and potash (Rochelle salts) in 200 parts of water, and to this he adds three parts of persulphate of iron dissolved in fifty parts of water. A large precipitate of prussian blue is formed; to the whole is added, drop by drop, with constant stirring, a solution of caustic soda until the blue precipitate entirely disappears, leaving a perfectly clear, light yellow liquid, which is now ready for use.

### TIN BATH.

The following is one of the best solutions for plating with tin by the battery process;

> Potassium pyrophosphate, 12 oz. Protochloride of tin, 41/2" 20 Water.

The anode or feeding plate used in this bath consists of pure Banca tin. A moderately strong battery is required, and the work is finished by scratch-brushing.

### COPPER BATH FOR ELECTROTYPING.

Dissolve sulphate of copper in water until the solution registers 15° by an acid hydrometer, then add enough sulphuric acid to make the hydrometer register 18°. This bath need not be filtered. It should be stirred about once or twice a week when using.

### COPPER:-Cold Bath for Iron, Steel, Etc.

Acetate of Copper. 3 oz. Carbonate of Soda, 6 1-5" 3 1-5" Bisulphite of Soda. Cyanide of Potassium. 314 " Water. 1 gallon. 2 1-5 fl oz. Aqua Ammonia,

### WARM BATH.

Acetate of Copper. 3 1-5 oz. Carbonate of Soda, 3 1-5 " Bisulphite of Soda, 1 1-5 " Cyanide of Potassium. 41/2 Water. 1 gallon. 1 4-5 fl. oz. Aqua Ammonia,

In the preparation of these baths the salts are all dissolved together, except the copper acetate and ammonia which are added after dissolving together in a small quantity of the water.

The deep blue color of the ammonia-copper solution should entirely disappear on mixing it with the other solution: otherwise, it becomes necessary to add more cyanide.

### Cleansing Copper and Copper Alloys.

Potash. Caustic. 1 pound. Water. Soft. 1 gallon.

Heat nearly to boiling in a cast iron pot provided with a cover. If the articles are much oxidized, pickle in a bath composed of-

Water. 1 gallon.

Sulphuric Acid, 1 pint, until the darker portion is removed. Rinse in running water and dip in the following solution:

Water, soft. Cyanide of Potassium, 8 ounces.

Remove from the bath, and quickly go over every part with a brush and fine pumice stone powder moistened with the cyanide solution.

### CLEANSING CAST-IRON.

Cast-iron is freed from grease, etc., by dipping in hot alkali solution used for a similar purpose with copper, and after rinsing thoroughly it is pickled in water containing one per cent of sulphuric acid for several hours; then rin-sed in water and scoured with a fine sharp sand or pumice powder and a fiber brush.

It is then rinsed and returned to the acid pickle for a short time, rinsed again, and put into the plating bath

directly.

### CLEANSING WROUGHT-IRON.

The cleansing of wrought-iron, if much oxidized, is effected in the same manner as cast-iron; but it will bear a stronger pickle and a longer exposure. Whitened, filed, or polished iron may be treated like steel.

### CLEANSING STEEL.

Dip in the caustic lye used for copper, etc., rinse thoroughly, scour with pumice powder moistened, rinse, and pass through the following dip:

> Water, 1 gallon. Hydrochloric Acid. 4 lbs.

Rinse quickly (but thoroughly) and plunge in the bath. Clean wrought-iron and steel gild well without an intermediary coating in hot electro-gliding baths. It is difficult to obtain an adhering coating of silver on these metals without interposing an intermediate coating of copper or brass, which renders the further operation of silver plating easy.

### Cleansing Zinc, Tin and Lead.

Zinc is cleansed by dipping a few moments only (as the alkali quickly attacks the metal) in the hot potash lye, rinsing, and dipping into water containing about 10 per cent of sulphuric acid for a few minutes. Rinse in plenty of hot water, and, if necessary, scour with pumice stone powder and a stiff brush, moistened with a weak cyanide solution, or scratch brush. This last operation is especially useful when parts have been united with tin solder.

Tin, lead, and the alloys of these metals are more diffi-

cult to cleanse perfectly than zinc or iron.

Scour rapidly with the hot potash and brush, rinse quickly and brush, or dress with a piece of soft clean wood.

It is very difficult to obtain a satisfactory deposit of gold

or silver directly upon these metals or their alloys. The results are much better if a coating of purecopper is interposed.

### GOLD PLATING BY SOLUTION.

A solution of gold is made in nitro-muriatic acid, and there is added to it twice as much sulphuric ether. The mixture must be shaken and allowed to repose when the ether with the chloride of gold will separate from the remaining liquid and rest above it. This dark colored ethereal solution is poured off from the light colored liquid beneath, and can be preserved for use in tight bottles, excluded from light. When applied it is with a very fine brush, or camels hair pencil the ether evaporates immediately leaving a coating of gold. This is burnished after being heated. The adhesion is more perfect, however, if the article be raised to a temperature approaching redness.

### GILDING BRASS AND COPPER.

Brass and copper may be readily gilt, by being dipped in a dilute *neutral* solution of chloride of gold, and then washed and burnished.

### GILDING BRASS AND COPPER.

A process was patented in 1836 by an English toy maker, and is well adapted for small articles. It consists in immersion them in hot solution of chloride of gold, to which has been added a considerable excess of bicarbonate of soda.

### COPPER DEPOSITS BY DIPPING.

This is seldom practiced except on iron, as the deposits thus obtained are generally wanting in lasting qualities, since, from the thinness of the coating, the iron is but imperfectly protected from atmospheric influences. If the iron is dipped in a solution of—

Sulphate of Copper,  $3\frac{1}{2}$  oz. Sulphuric Acid,  $3\frac{1}{2}$  "Water, 1 to 2 gal,

it becomes covered with a coating of pure copper, having a certain adhesion; but should it remain there a few minutes, the deposit becomes thick and muddy, and not stand any rubbing. Small articles such as pins, hooks, and nails, are thus coppered by tumbling them for a few moments in sand, bran, or sawdust impregnated with the above solution diluted with 3 or 4 volumes of water.

### TIN DEPOSIT BY DIPPING.

When immersed in a hot solution of tin properly prepared the metal is precipitated upon their surfaces. One of the best solutions for this purpose is the following:

Ammonia Alum,	171/4	oz.
Boiling Water,	121/2	
Protochloride of Tin.	1 "	6.6

The articles to be tinned, first thoroughly cleaned, are put into the hot solution until properly whitened. A better coating can be obtained by using the following bath, and placing the pieces in contact with a strip of clean zinc also immersed:

Bitartrate of Potassa,	14 oz.
Water (soft)	24
Protochloride of Tin.	1 "

It should be boiled for a few minutes before using.

#### BRONZE DIP.

Nitrie Acid,	8 oz.   Alum,	1 oz.
Muriatic Acid,	1 qt.   Salt,	2 "
Sal-Ammoniae	2 oz.   Water.	2 gal
Add the salt after	boiling the of	her ingredients, and
use hot		

### BROWN BRONZE DIP.

Iron scales, 1lb; Arsenic, 1 oz; Muriatic Acid, 1 lb: A piece of solid Zinc, 1 oz. in weight to be kept in while useing.

### NICKEL-PLATING DIP.

Into the plating vessel which may be of porcelain, or copper, is placed a concentrated solution of zinc chloride, which is diluted with from 1 to 2 volumes of water and heated to boiling. (If any precipitate separates, it is to be redissolved by adding a few drops of hydrochloric acid). As much powdered zinc as can be taken on the point of a knife is thrown in, by which the vessel becomes covered internally with a coating of zinc. The nickel salt for which purpose either the chloride or sulphate may be used—is then added until the liquid is distinctly green; and the articles to be plated, previously thoroughly cleaned, are introduced, together with some zinc fragments. The boiling continues for fifteen minutes, when the coating of nickel is completed, and the process is finished. The articles are well washed with water and cleaned with chalk. If a thicker coating be desired, the operation may be repeated.

#### SILVERING POWDER.

Silver powder may be prepared in the following manner: Precipitate] silver from its solution in nitric acid, by dropping into it some plates of clean copper. Take 20 grs. of this powder and mix with it 2 drachms of cream of tartar the same quantity of common salt, and half a drachm of alum. These articles must be finely pulverized, and inti-

mately mixed in a mortar. If a little of this powder be moistened, and rubbed on a clean surface of brass or copper, the silver will be precipitated, and the surface of the metal will be covered with it.

#### STONE-WORK.

Stone walls are measured by the perch. A perch of stone is 24.75 cubic feet. When built in the wall, 234 cubic feet are allowed for the mortar and filling; hence, 22 cubic feet of stone make one perch of wall.

Masons estimate 3 pecks of lime and 4 bushels of sand

to a perch of wall.

To find the number of perches of stone in a wall, multiply together the length, height and thickness, in feet, and

divide by 22.

Openings less than 3 feet wide are counted solid; over 3 feet deducted, but 18 inches are added to the running measure for each jamb. Built arches are counted solid from their spring. Corners of buildings are measured twice. Pillars less than 3 feet are counted on 3 sides, as lineal, multiplied by fourth side and depth.

A cord of stone, 3 bushels of lime and a cubic yard of sand will lay 100 cubic feet of wall.

It is customary to measure all foundations and dimension of stone by the cubic foot. Water tables and base courses by lineal feet. All sills and lintels or ashlar, by superficial feet, and no wall less than 18 inches thick.

### The Greatest Load per Superficial foot.

Granite Piers.	=	40 Tons
Lime Stone Piers.	=	35 "
Sand " "	=	15 "
Brickwork in Cement.	=	3 "
Rubble Masonry.	=	2 "
Lime Concrete foundation.	=	21/2 "

The height of brick or stone piers should not exceed 12 times their least thickness at base.

#### BRICK-WORK.

Brick work is generally measured by 1000 bricks laid in wall. In consequence of variation in size of bricks, no rule for volume of laid brick can be exact. The following scale is, however, a fair average.

7 15	common	bricks	to a	superficial	foot	t 4	inch	wall.
23	66	64	66	66	+6	12	6.6	66
30	61	66	44	6.	66	16	6.0	6.6
38	44	+4	44	61	66	20	66	6.6
45	44	44	6-6	66	6.6	24	6.6	6.6

Corners are not measured twice as in stone work. Openings over two feet square are deducted. Arches are counted from the spring. Fancy work counted 1½ bricks for 1. Pillars are measured on their face only.

A cubic yard of mortar requires one cubic yard of sand and 9 bushels of lime, and will fill 30 hods.

One thousand bricks, closely stacked, occupy about 56 cubic feet.

One thousand old bricks, cleaned and loosely stacked, occupy about 72 cubic feet.

Five courses of brick will lay one foot in height on a chimney.

Nine bricks in a course will make a flue eight inches wide and twenty inches long, and eight bricks in a course will make a flue eight inches wide and 16 inches long.

One superficial foot of gauged arches requires 10 bricks. Common bricks are 734 to 8 inches long by 414 wide and 216 thick. Front bricks are 14 inch longer and wider.

It requires 20 common bricks to lay one cubic foot. In an 8 inch wall 15 common bricks make one foot of wall.

Stock bricks commonly measure 834 inches by 414 inches, by 234 inches, and weigh from 5 to 6 pounds each.

Paving-bricks should measure 9 inches, by 4½ by 1¾ inches, and weigh about 4½ pounds each.

One yard of paving requires 36 stock bricks, of above dimensions, laid flat, or 52 on edge; and 35 paving laid flat. or 82 on edge.

To find the number of bricks in a wall 12 inches or more in thickness, multiply together the length, height and thickness, in feet, and that 'gagain by 20. For an 8 inch wall, multiply the length by the height, and that by 15, and the product will be the number of bricks in the wall. If the wall is perforated by openings, such as door, windows, etc., multiply the length of such openings by the width, and that by the thickness, and deduct from the cubic contents of the wall before multiplying by 15 or 20 as above.

Bricks should be well wetted before use. Sea sand should not be used in the composition of mortar.

### RED WASH FOR BRICKS.

To remove the green that gathers on bricks, pour over them boiling water in which any vegetables, (not greasy), have been boiled. Repeat for a few days, and green will disappear. For the red wash melt one ounce of glue in one gallon of water; while hot add alum size of an egg, one-half pound Venetian red, one pound Spanish brown. Try it; if too light add more red and brown. If too dark, water.

Number of Brick required to Construct any Building. (Reckoning 7 bricks per superficial foot).

Super. ft. of	Number of Bricks to Thickness of Wall.											
Wall.	4 inch.	8 inch.	12 inch.	16 inch.	20 inch.	20 inch. 24 inch						
1	7	15	23	30	38							
2	15	30	45	60	75	90						
3	23	45	68	90	113	135						
4	30	60	90	120	150	180						
2 3 4 5 6 7 8 9	38	75	113	150	188	225						
6	45	90	135	180	225	270						
7	53	105	158	210	263	315						
8	60	120	180	240	300	360						
9	68	135	203	270	338	405						
10	75	<b>1</b> 50	225	300	375	450						
20	150	300	450	600	750	900						
30	225	450	675	900	1125	1350						
40	300	600	900	1200	1500	1800						
50	375	750	1125	1500	1875	2250						
60	450	900	1350	1800	2250	2700						
70	525	1050	1575	2100	2625	3150						
80	600	1200	1800	2400	3000	3600						
90	675	<b>1</b> 350	2025	2700	3375	4050						
100	750	1500	2250	3000	3750	4500						
200	1500	3000	4500	6000	7500	9000						
300	2250	4500	6750	9000	11250	13500						
400	3000	6000	9000	12000	15000	18000						
500	3750	7500	11250	15000	18750	22500						
600	4500	9000	13500	18000	22500	27000						
700	5250	10500	15750	21000	26250	31500						
800 ·	6000	12000	18000	24000	30000	36000						
900	6750	13500	20250	27000	33750	40500						
1000	7500	15000	22500	30000	37500	45000						

### PLASTERING.

### Estimate of Material for 100 square yards.

MATERIALS.	Two coats, slipped coat finished.	Three coats with hard finish.
Quick Lime, " for fine stuff,	3½ casks,	4 casks.
Plaster of Paris,		1/2 "
Laths,	2000	2000
Hair,	3 bushels,	4 bushels.
Common Sand,	6 loads,	7 loads.
White Sand,	•	21/2 bushels.
Nails,	13 pounds,	13 pounds.
Masons Labor,	31/2 days,	4 days.
Laborer,	2 days.	3 days.
Cartage.	34 days	1 day.

Plastering laths are usually of white or yellow pine, 1½ inches wide, ¼ inch thick, and 3 or 4 feet long. They are nailed up horizontally, about ½ inch apart, the upright stud or partitions are spaced at such distance apart (usually about 15 inches, centre to centre), that the ends of the laths may be nailed to them.

Laths are sold in bundles of 50 to 100 each. A square foot of surface requires, 11/2 four-feet laths, or 1000 such laths will cover 74 square yards, and 12 pounds of nails will lay them on.

A carpenter can nail up the laths for from 40 to 60 square yards of plastering in a day of 10 hours, depending on the number of angles in the room, etc.

Plastering is always measured by the square yard for plain work, by the superficial foot for cornices or plain members, and by lineal foot for enriched members or carved mouldings in cornices.

The mortars used for inside plastering are termed course, fine, gauge or hard finish, and stucco.

Course stuff-Lime 1 part, sand 2 parts, hair 1-6 part.

Fine stuff (lime putty). Lump lime sclacked to a paste with a moderate volume of water. and afterwards diluted to the consistency of cream, and then to harden by evaporation to the required consistency for working.

Gauge stuff or Hard finish, is composed of from 3 to 4 volumes of fine stuff and one volume plaster of Paris, in proportions regulated by the degree of rapidity required in hardening; for cornices etc., etc., the proportions are equal volumes of each, fine stuff and plaster.

Stucco is composed of from 3 to 4 volumes of white sand, and one volume of fine stuff, or lime putty,

#### SHINGLES.

The best shingles are of white cedar.

When of good quality, they will last about 45 years in our northern State. Cypress and white pine are much used for shingles, but will not last half as long as white cedar.

Shingles are packed 250 in the bundle, or 4 bundles to 1000. One bundle 16-inch shingles will cover 30 square feet.

One bundle 18-inch shingles will cover 33 square feet. When laid 51/2 inches to the weather, 5 fbs., (4p) or 33/4 fbs. (3p) nails will lay them on.

#### COST of TIN ROOFING.

The following table shows the cost per square and sq. foot of tin roofing laid with 14 by 20 tin and 20 by 28 tin both flat and standing seam.

(A square is 100 square feet).

		(21 0	2 50 CT C 00 10	o nquare jece	7.					
	Flat S	eam Roo	fing.	Standing Seam Roofing.						
C	ost wi	ith 14×20	Tin.	Cost with 14×20						
T. pe	r box	Per sq.	Per sq.ft.	T.per box.	Per sq. Per sq.ft					
\$4.		\$2.21	.0221	\$4.25	\$2.37	.0237				
	.50	2.34	.0234	4.50	2.51	.0251				
4.	75	2.47	.0247	4.75	2.65	.0265				
	.00	2.60	.0260	5.00	2.79	.0279				
5.	25	2.73	.0273	5.25	2.93	.0293				
5.	50	2.86	.0286	5.50	3.06	.0306				
5.	.75	2.99	.0299	5.75	3.20	.0320				
6.	.00	3.12	.0312	6.00	3.34	.0334				
6.	25	3.25	.0325	6.25	3.48	.0348				
6.	.50	3.38	.0338	6.50	3.62	.0362				
6.	75	3.51	.0351	6.75	3.76	.0376				
7.	.00	3.64	.0364	7.00	3.90	.0390				
C	ost w	ith $20\times28$	3 Tin.	Cost wi	th $20\times2$	8 Tin.				
\$8.	.00	\$2.01	.0201	\$8.00	\$2.15	.0215				
8.	.50	2.13	.0213	8.50	2.28	.0228				
9.	.00	2.26	.0226	9.00	2.41	.0241				
9.	50	2.38	.0238	9.50	2.55	.0255				
10.	.00	2.51	.0251	10.00	2.68	.0268				
10.		2.63	.0263	10.50	2.82	.0282				
11.	.00	2.76	.0276	11.00	2.95	.0295				
11.	50	2.88	.0288	11.50	3.09	.0309				
12.		3.00	.0300	12.00	3.21	.0321				
12.		3.13	.0313	12,50	3.35	.0335				
13.		3.25	.0325	13.00	3.48	.0348				
13.		3.38	.0338	13.50	3.62	.0362				

For solders see page 210

### SLATING.

A square of slate or slating is 100 superficial feet. In measuring, the width of the eaves is allowed at the

In measuring, the width of the eaves is allowed at the widest part. Hips, valleys, and cutting are to be measured lineal, and 6 inches width extra is allowed.

The thickness of slates, ranges from 3-16 to 5-16 of an inch, and their weight varies from 2.6 to 4.5 lbs per square foot.

The lap of slates varies from 2 to 4 inches. The standard is assumed to be 3 inches.

The pitch of a slate roof should not be less than 1 inch in height to 4 inches in length.

### DIMENSIONS OF SLATES AND NUMBER REQUIRED TO A SOUARE, (AMERICAN).

	SIZE		No. of Slate.	Weight per Sq. about.	5	SIZE.	No. of Slate.	Weight per Sq. about.
12	by	6	533	lbs.	18	by 11		Dis.
12		7	457	<b>≻</b> 850	20	1(		
12 12	66	8	400	IJ II	20	" 1		<b>  } 650</b>
14	66	7	374		20	" 12		
14 14	4.6	8	327	≻ 750	22	" 1	138	1 1
14	64	9	291		22	" 12	126	K
16	66	8	277	1	22 22	" 13		
16	66	9	246	l i i	24	" 12	114	F 675
16	64	10	221	<b>650</b>	24	" 1	3 105	1
18	6.6	-ğ	213		24	" 1		
18	46	10	192					

To compute the number of slates of a given size required per square. Subtract the lap from the length of the slate, and half the remainder will give the length of the surface exposed, which, when multiplied by the width of the slate, will give the surface required, and for which the party requiring the slating only pays.

Divide 14400 (the area of a square in inches) by the sur-

face thus obtained, and the quotient will give the number

of slates required for a square.

Illustration:—A slate is 24×12 inches, and the lap is 3 inches.

24-3=21, and 21+2=10.5, which  $\times 12=126$  inches;  $14400 \div$ 126=144.29 slates.

Good American slate weighs about 174 pounds per cubic foot. Hence-

Slabs 34 inch thick weigh 10.86 pounds per square foot. 

66	11/4	66	66	66	18.12	66	66	6.6	66
6.6	11/4 11/2 2	66	66			66	66	66	6.6
66	2'4	66	66	66		66	66	66	6.6

### CORRUGATED IRON ROOFING.

Birmingham Wire Gauge.	W'g't per Square (100 Sq. feet). Plain or Painted.	GALVANIZED IRON.*
No. 28 26 24 22	97 fbs. 105 '' 128 '' 150 ''	Galvanized iron weighs from 5 to 15 per cent. heavier than plain, accord-
20 18	185 " 270 "	ing to the No. Birmigham Wire Gauge.

<sup>\*</sup>See page 38 for sizes.

Lighter than No. 22 is not recommended, for a good durable roof.

Corrugated iron is usually made in sheets from 2 to 3

feet wide, and from 6 to 8 long.

The sheets when used for roofing should overlap about 6 inches in girth, and be double-riveted at the joints.

One-third of the net width may be allowed approximate-

ly for lappage and corrugations.

From 21/2 to 31/2 pounds of rivets will be required for a square.

#### PAINTING. \*

For outside wood-work, paint made from white lead ground in linseed oil is most used. If the oil is raw, or unboiled, dryer is added: if boiled no dryer is necessary. Not less than four coats should be applied,—five are better.

Paint, ready mixed, put up in cans or kegs, may be procured from manufacturers or dealers. These paints have to be thinned by adding 1 pint of oil to about 2½ pounds of paint. When thinned, 1 pound will cover about 2 square yards; of first coat, 3 yards of second, and 4 yards of each subsequent coat; or 138 pounds, to the square yard will be required for 4 coats, and 158 for 5 coats.

For inside work, either white lead or oxide of zinc is

used, and for good work 4 coats are necessary.

For iron exposed to the weather, metallic paint, such as vellow and red iron ochres or brown hematite ore, finely pulverized and mixed with oil or dryer, are best. If to the action of the water red lead is best.

Plastered walls should stand a year before painting.
Painting is measured by the square yard, girding every
part of the work that is covered by paint and allowing an
addition to the actual surface for the difficulty of covering deep quirk of mouldings and for "cutting in" as in
sash and shelving, or where there is a change of color,
on some work. Painters putty is made of spanish whiting, pulverized, 80 parts; boiled oil 20 parts; make into a stiff paste. If not intended for immediate use, raw oil shuld be used. One pound of putty for stopping every 20 yards.

#### GLAZIERS PUTTY.

Whiting, 70 pounds; boiled oil, 30 pounds; water 2 gals. If too thin add more whiting; if too thick add more oil.

#### TO SOFTEN PUTTY.

To remove old putty from broken windows, dip a small brush in nitro-muriatic acid or caustic soda (concentrated lye), and with it anoint or paint over the dry putty that adheres to the broken glass and frames of your windows; after an hours interval the putty will have become so soft as to be easly removable.

\* For mixing colors see page 109.

#### WASHES.

FOR OUTSIDE WORK.—In a tight box, slack half a bushel of fresh lime by pouring over it boiling water sufficient to cover it 4 or 5 inches deep, stir until slacked; add 2 lbs. of sulphate of zinc dissolved in water, add water enough to bring all to the consistency of thick white-wash

FOR INSIDE WORK.—Add 2 quarts of thin size to a pailful of wash just before using. The common practice of mixing salt with white-wash should not be permitted.

WHITE-WASH.--Whiting 4 pounds; common glue. two ounces; stand glue in cold water over night; mix whiting with cold water, heat glue till dissolved, and pour it hot into the former. Make of consistency to apply with common white-wash brush.

WHITE-WASH that will not rub off.—Mix up half pail full of lime and water, ready to put on the wall; then take one-fourth pint of flour, mix it with water, then pour on it a sufficient quantity of boiling water to thicken it, and pour it while hot into the white-wash; stir all well together, and it is ready for use.

FOR BRICK OR STONE WORK.—Slack 1/2 bushel of lime, as before in a barrel; then fill the barrel 2/3 full of water and add a bushel of hydraulic cement; add 3 pounds sulphate of zinc dissolved in water. The washes may be colored by adding powdered ochre, umber, etc.

### DYEING.

### GENERAL REMARKS.

Everything should be clean. The goods should be scoured in soap and the soap rinsed out. They are often steeped in soap lye over night. Dip them into water just before putting them into preparations, to prevent spotting. Soft water should be used, sufficient to cover the goods well—this a always understood where quantity is not mentioned. When goods are dyed, air, rinse well, and hang up to dry. Do not wring silk or merino dresses when scouring or dyeing them. If cotton goods are to be dyed a light color, they should be bleached.

### SILKS.

BLACK.—Make a weak dye as for black on woolens; work goods in bichromate of potash a little below boiling heat, then dip in the logwood in same way; if colored in blue vitriol dye, use about the same heat.

ORANGE.—For one pound goods—annotto, one pound; soda, one pound; repeat as desired.

GREEN.-Very Handsome—For one pound goods—yellow oak bark, eight ounces; boil one half hour; turn off liquor from bark and add alum, six ounces; let stand until cold; while making this, color goods in blue dye-tub a light blue; dry and wash; dip in the alum and bark dye. If it does not take well, warm the dye a little.

PURPLE.—For one pound goods.—First obtain a light blue, by dipping in home-made dye-tub; then dry; dip in alum, four ounces, with water to cover, when little warm. If color is not full enough add chemic.

YELLOW.—For one pound goods—alum, three ounces; sugar of lead, three-fourths ounce; immerse goods in solution over night; take out; drain, and make a new dye with fustic. one pound; dip until required color is obtained.

CRIMSON.—For one pound goods—alum, three ounces; dip at hand heat one hour; take out and drain while making new dye by boiling ten minutes, cochineal, three ounces, bruised nut-galls, two ounces, and cream-tartar, one-fourth ounce, in one pail of water; when little cool, begin to dip, raising heat to boil; dip one hour; wash and dry.

SKY BLUE ON SILK OR COTTON.—Very beautiful.—Give goods as much color from a solution of blue vitriol, two ounces, to water, one gallon. as it will take up in dipping fifteen minutes, and then run it through lime water. This will make a beautiful and durable sky blue.

Brown on SILK OR COTTON.—Very beautiful—After obtaining a blue color as above, run goods through a solution of prussiate of potash, one ounce, to water, one gallon

LIGHT BLUE.—For cold water, one gallon, dissolve alum, one-half tablespoon, in hot water, one tea-cup, and add to it, then add chemic, one teaspoon at a time to obtain the desired color—the more chemic, darker the color.

### WOOLEN GOODS.

CHROME BLACK.—Best in use.—For five pound goods, blue vitriol, six ounces; boil a few minutes, then dip goods three-fourths hour, airing often; take out goods, make a dye with three pounds logwood, boil one-half hour, dip three-fourths hour and air goods, and dip three-fourths hour more. Wash in strong suds. This will not fade by exposure to sun.

WINE COLOR.—For five pound goods, camwood, two pounds; boil fifteen minutes and dip goods one-half hour; boil again and dip one-half hour; then darken with blue vitrioi, one and one-half ounces; if not dark enough, add copperas, one-half ounce.

SCARLET.—Very fine.—For 'one pound goods—creamtartar, one-half ounce; cochineal, well pulverized, one-half ounce; muriate of tin, two and one-half ounces; boil up the cye and enter the goods; work them briskly for ten or fifteen minutes, then boil one and one-half hours, stirring goods slowly while boiling. Wash in clean water and dry in the shade.

PINK.—For three pound goods—alum, three ounces; boil and dip the goods one hour; then add to the dye, creamtartar, four ounces; cochineal, well pulverized, one ounce; boil well and dip the goods while boiling until the color suits.

BLUE.—Quick Process.—For two pound goods—alum, five ounces; cream-tartar, three ounces; boil goods in this one hour, then put goods in to warm water which has more or less extract of indigo in it, according to the depth of color desired, and boil again until it suits, adding more of the blue if needed.

MADDER RED.—To each pound of goods—alum, five ounces; cream-tartar, one ounce. Put in goods and bring kettle to a boil, for one-half hour, then air them and boil one-half hour longer; empty kettle and fill with clean water; put in bran, one peck; make it milk-warm, and let is stand until bran rises, then skim off the bran and put in one-half pound madder; put in goods and heat slowly until it boils and is done. Wash in strong suds.

GREEN.--For each pound of goods-fustic, one pound; with alum, three and one-half ounces; steep until strength is out, and soak goods therein until a good yellow is obtained; then remove the chips and add extract of indigo or chemic, one tablespoon at a time, until color suits.

SNUFF BROWN, DARK,—For five pound goods—camwood, one pound; boil it fifteen minutes, then dip goods three-fourths hour; take out goods, and add to the dye, two and one-half pounds fustic; boil ten minutes and dip goods three-fourths hour; then add blue vitrol, one ounce; copperas, four ounces; dip again one half hour. If not dark enough, add more copperas.

ANOTHER METHOD.—Any shade.—Boil goods in a mordant of alum, two parts; copperas, three parts; then rinse them through a bath of madder. The tint depends on the relative proportions of the copperas and alum; the more copperas, the darker the dye. Joint weight of both should not be more than one-eighth of weight of goods, Mixtures of reds and yellows with blues and blacks, or simple dyes, will make any shade.

ORANGE.—For five pound goods—muriate of tin, six tablespoons; argal, four ounces; boil and dip one hour, and add again to the dye one tea-cup madder; dip again one-half hour. Cochineal, about two ounces, in place of madder, makes a much brighter color.

PURPLE.—For each pound goods—two ounces cudbear; rinse goods well in soap suds, then dissolve cudbear in hot suds—not quite boiling—and soak the goods until of required color. The color is brightened by rinsing in alum water.

YELLOW.—Rich.—Work five pound goods one-half hour in a boiling bath with three ounces bichromate of potassa and two ounces alum; lift and expose till well cooled and drained, then work one-half hour in another bath with five pounds fustic. Wash out and dry.

CRIMSON.—Work for one hour in a bath with one pound cochineal paste; six ounces dry cochineal; one pound tartar, one pint protochloride of tin. Wash out and dry.

SALMON.—For each pound goods—14th pound annotto; one-fourth pound soap; rinse goods in warm water, put them into mixture and boil one-half hour. Shade will be according to amount of annotto.

DOVE and SLATE COLORS—of all shades.—Boil in iron vessel a teacup of black tea with teaspoon of copperas, and sufficient water. Dilute till you get the shade wanted.

### COTTON GOODS.

BLACK.—For five pound goods—boil them in a decoction of three pounds sumach one-half hour, and steep twelve hours; dlp in lime water one-half hour; take out and let them drip one hour; run them through the lime water again fifteen minutes. Make a new dye with two and one-half pounds logwood (boiled one hour), and dip again three hours; add bichromate potash, two ounces to the logwood dye, and dip one hour. Wash in clear cold water and dry in shade. Only process for permanent black.

SKY BLUE.—For three pound goods—blue vitriol, four ounces; boil few minutes, then dip goods three hours; then pass them through strong lime water. A beautifut BROWN can be obtained by next putting goods through a solution of prussiate of potash.

GREN.—Dip goods in home-made blue; dye until blue enough is obtained to make the green as dark as required; take out, dry and rinse a little. Make a dye with fustic, three pounds, logwood, three ounces to each pound goods, by boiling dye one hour; when cooled so as to bear hand, put in goods, move briskly few minutes, and let lie one hour; take out and thoroughly drain; dissolve and add to the dye for each pound of cotton, blue vitriol, one-half ounce, and dip another hour. Wring out and let dry in the shade. By adding or diminishing the logwood and fustic, any shade may be had.

YELLOW.—For five pound of goods—seven ounces sugar of lead; dip goods two hours; make new dye with bichromate of potash, four ounces; dip until color suits; wring out and dry. If not yellow enough, repeat.

ORANGE:-For five pound goods-sugar of lead, four

ounces; boil few minutes; when a little cool, put in goods; dip two hours; wring out; make a new dye with bichromate of potash, eight ounces; madder, two ounces; dip until it suits; if color istoored, take small sample and dip into lime water and choose between them.

RED.—Muriate of tin, two-thirds teacup; add water to cover goods; raise to boiling heat; put in goods one hour; stir often; take out, empty kettle, put in clean water with nicwood, one pound; steep one-half hour at hand heat; then put in goods and increase heat one hour—not boiling. Air good and dip one hour as before. Wash without soan.

### PRINTING.

#### EXPLANATION OF POINT SYSTEM.

1 F	oint																		12	2 to 1	oica
2	+ 6	- 1																	6	6 to 1	oica
3	66																		4	to p	oica
316	64.																			Brilli	ant
4	46																		3	to r	oica
41/9	, "																			Diam	
5																			_		earl
51/3	. 66							i				Ċ		i		Ċ			·		ate
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24	4.6																4	line	N	onpa	reil
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36	64																6	+6		66	
42	6.																7			6.6	
48	+6							ľ				ľ		ľ		ĺ	8	66		6.6	
60	-6.												Ť		•		10	6.		66	
72	16			•		•				•							12	6.6		66	
• 4																	14				

### SIZES OF PRINTING TYPES.

0.220 0								
NAME OR BODY.	Size in dec.of a lin. inch.	ger than	Ems& dec of an em in a lineal foot.	dec. of				
Diamond.	.0595	lineal in.	201.587	40,637.46				
Pearl.	.0668	.0072	179.593	32,253.97				
Agate.	.075	.0081	160.	25,600.				
Nonpareil.	.0841	.0091	142.543	20,318.73				
Minion.	.0994	.0103	126,992	16,126.98				
Brevier.	.1060	.0115	113.137	12,800.				
Bourgeois.	.1190	.0129	100.793	10,159.36				
Long Primer.	.1336	.0145	89.796	8,063,49				
Small Pica.	.15	.0163	80.	6,400.				
Pica.	.1683	.0183	71.271	5.031.74				
English.	.1889	.0206	63,496	4.031.74				
Columbian.	.2121	.0231	56,568	3,200.				
Great Primer.	.2381	.0259	50.396	2,539.84				
Paragon.	.2672	.0291	44.898	2,015.87				
Double Small Pica.		.0327	40.	1.600.				
Double Pica.	.3367	.0367	35,635	1,269.92				
Double English.	.3779	.0412	31.748	1.007.93				
Double Columbian.		.0462	28.284	,800.				

American and British Types are cast 92-100 the of an inch in height. The European Printing Types are of many different heights.

### SIZES AND WEIGHTS OF PAPER.

Owing to the variations in sizes and weight of paper made by different mills, it is almost impossible to give a perfect scale. The following, however, are the sizes and weights most generally used.

### NEWS PAPER.

Imperial223	<3222, 25 lbs.
Small Double Medium 24	' 3625, 28, 30 lbs.
Double Medium24	38.28, 30, 32, 36, 40, 44, 50.
Double Royal25	$39 \text{ and } 26 \times 40.36, 40.50, 60.$
Double Super Royal28	42 and 29×4336, 40 lbs.
Double Imperial32	46 and 33×4645, 50, 53

#### ROOK PAPER

BO	OK PAPER.	
†Medium	$19 \times 24 \dots 25, 30, 35$ lb	s.
* "	20" 24 20, 25, 30, 40 lb	S.
†Super Royal	22" 2830, 40 lb	s.
* "	22" 2835, 40, 50, 60, 70, 80 11	s.
Medium-and-half		
+Double Medium		
* ''	24" 3835, 40, 45, 50, 60, 70, 8	30.
*Double Royal	26" 40 40, 50, 60 lb	S.

\*Double Super Royal, Double Imperial, \*Sized and calendered.

### FLAT PAPER.

	Letter,	10×16	7, 8, 9, 10, 12, 14 lbs.
66	Small Cap,	13" 16	12, 14,16 lbs,
6.6	Cap.	14" 17	10, 12, 14, 16, 18 lbs.
6.6	Crown,	15" 20	21 lbs.
4.6	Demy,	16" 21	16, 18, 20 22, 24, 28 lbs.
66	Folio,	17" 22	14, 16, 18, 20, 22, 24 lbs.
6.6	Double Cap.	17" 28	24, 28, 32, 36 lbs.
6.6	Medium.	18" 23	24, 28, 32, 36, 40 lbs.
46	Royal.	19" 24	42 lbs.
4.6	Super Royal,	20" 28	52 lbs.
6.6	Imperial	2211 30	65 lbs.

### MISCELLANEOUS.

Bond Paper, 14 by 17, 17 by 22, 19 by 23. Blotting Paper, 19 by 24, 60, 80, 100, 120 lbs. Card Sheets, 22 by 28. Cover Papers, 20 by 25. 25, 95 lbs, Glazed, Plated, and Enameled Papers, 20 by 24.

### UPPER CASE.

1	t	İ	8	H	1	fist		•		2m	İb	報	@
1/2	1/4	3/4	⅓	3/3	1/8	3/8	5%	3/8	2m	3 m	-	~	-
&	Æ.	Œ	æ	œ	£	\$			2m	3т	Æ	Œ	&
Λ	В	C	D	E	F	G	Α	B	C	D	E	F	G
Н	1	К	L	M	N	0	H	I	K	L	M	N	O
P	Q	R	8	T	ν	W	P	Q	R	S	T	V	W
X	Y	7.	J	U		)	X	Y	Z	J	U	n	m

### LOWER CASE.

笽	h:r	5m 4m	'lk		1   2	3 4	5	Q	7	8
j	b	С	d	е	j	8	f	o	ff	9
1	Ľ	·					_	<u>ь</u>	fi	0
Z	1	m	n	h	0	ур	w	٦	n od	m
X				3m			٦	٦	25	
q	Y	u	t	spc	.a	r	Ħ		qua	ds.

### Average Daily Performance of Presses.

The estimates of the following table are for miscellaneous work, done in the usual manner, with little making ready, and under the favorable conditions of a brisk season. It is supposed that the presses are at work full ten hours; that feeders and pressmen are expert and diligent; that paper, rollers, steam power, ink, etc., are in perfect order, and that there are no detentions or accidents:

Make		Time of	Rate	Daily
	Style of PressNo. of Forms.	Press	per	perf'r-
	Divide of Tress.—No. of Forms.			
Time.		Work.	hour.	ance.
Hours.		Hours.		Impr.
	~	ourb.		arrap
	Card Press.			
1	1 form of 7.500 impressions.	9	833	7.500
4	4 " 1.000 "	6	666	4.000
1 4 6	8 " 250 "	6	500	2.000
U		- 7	000	2.000
	Small Machine Press.			
1	1 form of 6.000 impressions.	9	666	6,000
5	5 " 500 "	5	500	2.500
1 5 8	18 " 100 "	9 5 2	400	800
O	100	4	400	600
	Hand Press.			
1	1 form of 1.500 impressions.	9	156	1.500
1 4	4 '' 250 ''	9 -	166	1.000
•			100	1.000
	Medium Cylinder.	1	1	1
1	1 form of 7.500 impressions.	9	833	7.500
5	5 " 750 "	5	750	3.750
1 5 7	5 " 750 " 8 " 250 "	9 5 3	666	2.000
•			000	2.000
	Double Medium Cylinder.		1	
2	1 form of 5,000 impressions.	8	666	5.000
5	3 " 1.000 "	5	600	3.000
2 5 7	6 " 250 "	8 5 3	500	1.500
4		) 0	300	1.000
	Mammoth Cylinder.		1	
3	1 form of 4.000 impressions.	7	570	4.000
5	2 " 1.250 "	5	500	2.500
3 5 7	4 " 250 "	5 3	333	1.000
-	11 400	1 0	1 000	1 1.000

### MEASURING TYPE OR MATTER.

The measurement is made by multiplying the number of solid ems contained in the length of any body of type, by the number contained in the width of the measure. The gauge for measurement is an em of the type in which the matter calculated is set.

In book offices it is usual to count the matter appearing below the head line in the above manner, counting three ems in addition for the head line with its blank and the foot line, without regard to the size of the type in which they are set. In measuring the subject matter, anything in excess of an em and less than a half em is not counted, while an en, or an excess making less than an em, is counted as a full em.

Chapter heads, blank spaces, or cuts occurring in the dimensions of pages are rated the same as though the space occupied consisted of type. It is also customary to count as type a cut occupying a whole page when backed

by printed matter.

Quotations, poetry, and matter set in smaller type than the body of the work, are always counted according to the size of type in which they are set, distinct from the larger type in the same page or body of matter, commencing at the first line and extending to the first line of the larger type.

Pages set in columns, include all spaces between the columns and bordered pages are measured from outside to outside of border by the ems of the type which they

enclose.

Side and centre notes, in Bibles or law works, are measured by the full width of the note and the full length of the page, in the type of which they are composed.

The mode of acertaining the number of ems in a line is by laying as many of the letter m flatwise in the stick as

will make the measure.

It is customary in many newspaper offices to count the rule set between the advertisements as a line of type, although it may not be of the required depth. This necessitates counting the lines where a number are set together.

### COMBINATION LEADS.

The following table shows the combinations that can be formed by leads or slugs of six lengths only, not more than three pieces being required at one time.

LENGTH IN EMS OF THE PIECES EMPLOYED, 4, 7, 9, 13, 15, 20.

			4, 7	, 9, 15,	15, 20.			
4,	4	8	13,	13 7 13	26 27	15,	15. 9	39
7,	4	11	20,	7	27	20,	20	40
4,	4, 4	12	15,	13	28	15,	13, 13	41
7,	4, 4 7 7	12 14 16 17 18 19	13, 20, 15, 20, 15, 20, 15, 20, 15, 20, 15,	15 7. 4 13, 4	29	15, 20, 15, 20, 15, 20, 15, 20, 20, 20, 20,	20 13, 13 15, 7 15, 13	40 41 42 43 44 45 46 47 48 49 50
9,	7	16	15,	15	29 30 31 32 33 34	15,	15 <b>, 1</b> 3	43
13,	4	17	20,	7. 4	31	20,	29. 4	44
9,	9	18	15,	13, 4	32	15,	15, 15	45
15,	4	19 -	20,	13	33	20,	15, 15 13, 13	46
7.	7, 7	21	15,	13 15, 4	34	20,	20, 7	47
15,	4 9 4 7, 7	$\frac{21}{22}$ $\frac{23}{23}$	20,	15 9, 7	35	20,	20, 7 15, 13 20, 9	48
15,	4, 4	23	20,	9, 7	36	20,	20, 9	49
4, 7, 4, 7, 9, 13, 9, 15, 7, 15, 15, 20, 9,	4, 4 4 9, 7	24	15,	15, 7	35 36 37	20,	15, 15	50
9,	9, 7	25	20,	9, 9	38			

The printer has also at command the six single pieces used, viz: 4, 7, 9, 13, 15 and 20 ems. By using four, five, or six pieces together, the above combinations may be extended, consecutively to one hundred ems. Fonts of these leads, of suitable proportions, are put up and for sale by the different type founders.

#### CASTING OFF COPY.

The first step necessary is to take a comprehensive view of the copy, noticing whether it has been written even or has many interlineations, etc., and observing also the number of break-lines, and whether the work be divided into chapters and sub-heads, in order that the allowance may be made for them in the calculation. These observations may be noted on a separate piece of paper, to assist the memory and save the trouble of re-examining the This preparation being made, we ascertain manuscript. the number of words contained in the line by counting several separate lines in various parts of the copy, so that the one we adopt may be a fair average. We then take the number of lines in a page, and multiply by the number of words found in the average line. The quotient we then multiply by the quantity of folios the manuscript copy may contain, and thus we get the amount of words contained in the work, with a tolerable degree of accuracy. The necessary allowances should be made for breaklines chapters, insertions, etc., according to the observations previously made on the memorandum. If information has been furnished as to the size of letter the work is to be done in and the width of the page, we make our measure accordingly, and, by composing a few lines of the manuscript copy, we ascertain what number of words will come into each printed line. We then take the length of our page in lines, and multiply the one by the other, thus getting the number of words in the printed page. The quotient gives the number of pages the manuscript will make. If too many, the page must be enlarged; if too few, the page must be diminished in width and length. For example: We take the number of words in a line of manuscript at 20, the lines in a page at 50; we multiply 50 by 20, which will produce 1,000 words in a page; we then multiply 1,000 by 422, the number of the folios in the manuscript, and we find it contains 422,000 words. The work being printed in Pica octavo, 20 ems measure, and each line containing 10 words, each page 40 lines, the case will stand thus.

Manuscript.	Printed.
50 20 1000	40 10
422	400)422000 words in MS. 1055 pages.
2000 2000	Divide
4000 422000 words in MS	16)1055(65 sheets. 15 pages.

#### HOW TO BEND BRASS RULE.

By taking brass rule and heating it until about to turn red, and then immersing it in cold water, it can be easily bent to any desired shape.

#### RILEY'S INDISPENSABLE.

No. 1—For Fine Job Work. Dumar Varnish, 6 oz; Bergamot, 2 drachms; Balsam Copaiba, 2 drachms; Balsam of Fir, 3 oz., Creosote, 1 drachm; Copal Varnish one drachm. To enough ink for 1.000 ordinary business cards, add from 8 to 12 drops of the "Indispensable," and to larger quantities in proportion. When used for Bronze, Dry Colors, Diamond Printing, etc., take twice the quantity; and where an extra quick dryer is desired, add a few drops of dissolved Gum Arabic to the ink, after it has mixed with No. 1. In all cases, mix well with the ink before applying to the rollers.

#### HOW TO ESTIMATE THE QUANTITY OF TYPE.

To ascertain the quantity of Plain Type required for a Newspaper or Magazine, or any other work, find the number of square inches and divide the same by four, the quotient will be the approximate weight of matter: But as it is impossible to set the cases entirely clear it is necessary to add 25 per cent. to large fonts, and 33 per cent. to small fonts for dead matter.

Rule and figure work double price matter.

#### ROMAN NUMERALS.

Capitals are chiefly employed in designating the order of succession of kings, in chapter headings, and in indicating dates; while lower case are used as folios of a book, or to indicate chapter or verses referred to in the text.

The Following is a Complete System of Roman Enumeration.

1 I.	60 LX.
2 II.	70 LXX.
3 III.	80 LXXX, or XXC.
4 IIII or IV.	90 LXXXX, or XC.
5 V.	100 C.
6 Vi.	200 CC.
7 VII.	300 CCC.
	400 CCCC.
8 VIII. or IIX.	
9 VIIII. or IX.	500 D, or IQ.
10 X.	600 DC, or IQC.
11 XI.	700 DCC, or IDCC.
12 XII.	800 DCCC, or In CCC.
13 XIII. or XIIV.	900 DCCCC, or InCCCC.
14 XIIII. or XIV.	1,000 M. or CIO.
15 XV.	2,000 CIOCIOTICIC.
16 XVI.	
17 XVII.	5,000 IV or IOO.
18 XVIII. or XIIX.	10,000 X or CCIOO.
	,
19 XVIIII or XIX.	50.000 L or IDDD.
20 XX	100,000 C or CCCIOOO.
30 XXX	
40 XXXX or XL.	1,000,000 M or CCCCIDDDD.
50 L.	2,000,000 MM.

As often as a character is repeated, so many times is its value repeated.

A less character before a greater diminishes its value, as IV=V-I, or 1 subtracted from 5=4.

A less character after a greater increases its value, as XI=X+I, or 1 added to 10=11.

For every 3 annexed, the sum is increased 10 times.

For every C and O, placed one at each end, the sum becomes 10 times as many.

A bar thus —, over any number, increases it 1,000 times. Illustration.—1840, MDCCCXL. 18560, XVIIIDLX.

#### FOLDING PAPER.

FOLIO.—The standard size of this is 25 by 38. The half sheet folded in two leaves, having four pages, makes a book called a folio.

 $\ensuremath{\textit{QVARTO}}.-$  When the half sheet is folded in four leaves, making eight pages, it forms a quarto.

OCTAVO.—The half sheet folded again, eight leaves, sixteen pages, forms an octavo; or folded in sixteen leaves forms a 16 mo.

DUODECIMO.—By folding the same into twelve leaves, making twenty-four pages, we have a duodecimo. Folded into eighteen leaves, we form an 18 mo., into twenty-four leaves, and we have a 24 mo., etc.

The words, Post, Crown, Demy, Royal, etc., used in connection, as Royal Octavo, designate the size of paper of

which the book is made.

Modern facilities for the manufacture of paper enable publishers to have any desired size made to order,

Marks occasionally found at the bottom of a page are termed signatures (such as a, b, c; or 1, 2, 3; or 1\*2\*3\*), and are used for the direction of the pressman and binder in printing, folding and gathering sheets.

Amount of Paper Required for a Book of any Size.

No. of form.	_	_	ber of				0.1.25	Amount for 1000 cop's in
			16 10	18 MO	24 MO	32 MO	36 Mo	R. & qr.
1	8	12	16	18	24	32	36	1 R 2qr
2	16	24	32	36	48	64	72	2-4
3	24	36	48	54	72	96	108	3 6
2 3 4 5	32	48	64	72	96	128	144	4 8
5	40	60	80	90	120	160	180	510
6	48	72	96	108	144	192	216	612
6 7 8 9	56	84	112	126	168	224	252	714
8	64	96	128	144	192	256	288	816
9	72	108	144	162	216	288	324	918
10	80	120	160	180	240	320	360	11
11	88	132	176	198	264	352	396	12 2
12	96	144	192	216	288	384	432	13 4
13	104	156	208	234	312	416	468	14 6
14	112	168	224	252	336	448	504	15 8
15	120	180	240	270	360	480		1610
- 16	128	192	256	288	384	512		1712
17	136	204	272	306	408			1814
18	144	216	288	324	432			1916
19	152	228	304	342	456			2018
20	160	240	320	360	480			22
21	168	252	336	378	504			23 2
22	176	264	352	396				24 4
23	184	276	368	414				25 6
24	192	288	384	432				26 8
25	200	300	400	450				2710

EXAMPLE:—How many reams will be required for a 16 mo. book of 320 pages? Find the number of pages (320) in the 16 mo column; and on the same line in the outer column we find 22 reams. For books with a greater number of forms than is given in the table find the quantity for half the forms and multiply by 2. If the forms are odd subtract 1 from its number and find  $\frac{1}{2}$  multiply by 2 then add the first figures in the outer column (1 R. & 2 grs).

TABLE SHOWING THE QUANTITY OF PAPER REQUIRED for ANY JOB OF FROM 50 to 10,000 COPIES.

0000000000000 grs SILE SIP STUS copies) sip w spts waste or over SIP spys STP S 80247284078872887245082744 spts SIP forspts (No allowance is made grs spts 4-4110 0018 0011 021 024 00 001 gib spts 8980182929292 898018292 a 000011122222222 SIP spts 025240128010271490558cr5225148 000111222888446089188886 SIP SHEET. spts では184425m2345m23m2143 grs Slas 0108093446440810480881 to a 00112228442000085222522 SIP spts 2 to 48 SIP spęs F065445888085368689415 01284708800112812222444388 SIP FROM sprs -24c08024c080-01522848 SIP Red, eq 

#### COMPOSITION ROLLERS, for Summer Use.

Are made of a mixture of the best glue and refined syrup, in the proportion of 10 pounds glue to 5 quarts of syrup. Soften, but not over soak, the glue with water; then melt it; then add the syrup and let the mixture boil briskly for 30 minutes.

#### WINTER USE.

Composition Rollers for winter use, or for extreme cold weather, are made in the proportions of five pounds of glue to five quarts of syrup. This makes a tender roller, which may be stiffened by adding 2 ounces of tar.

Roller composition should not be over cooked: If it is boiled 40 or 50 minutes, or more, the syrup will candy, and the composition will be spoiled.

#### How to MIX PRINTING INK (and Paints) FOR TINTS.

Mi

ixing	Red and Black makes	Brown.
	Lake and White makes	Rose.
	Umber and White makes	Drab.
	White and Brown makes	Chestnut.
	Yellow and Brown makes	Chocolate.
	Red with Light Blue makes	Purple.
	Carmine with Straw makes	Flesh color.
	Blue with Lead color makes	Pearl.
	Carmine with White makes	Pink.
	Lamp-Black with Indigo makes	Silver Gray.
	Lamp-Black with Indigo makes " " White makes	Lead color.
	Paris Green with White makes	Bright Green.
	Yellow-Ochre and White makes	Buff.
	White tinted with Purple makes	French White.
	Black with Chrome Green makes	
	Emerald Green with White makes	
	Vermillion with Chrome Yellow n	primant dreen.
	Chrome Yellow and White Lead ma	lzog Strawgol'r
	White tinted with Red and Yellow	
	Chrome Yellow, Blue, Black and R Chrome Green with White makes	Doe Cross
	Vollow and Comming on Deep Ded	rea Green.
	Yellow and Carmine or Deep Red	makes Scarlet.
	Carmine and Blue makes Deep L	nac, violet Pur-
	ple and Plum.	
	Blue and Black makes Deep Blu	ie or Blue-Black.
	Vermillion and Black makes	Rich Brown.

Orange Mineral and White make beautiful Flesh Tints. Violet and White makes pale Lilac or Layender.

Bronze Green.

Deep Green.

Yellow and Black makes

Yellow Blue and Black makes

Mixing Yellow and Blue makes bright or a Light Green.
Ultramarine, White and Carmine form the various

tones of Lilac, etc. Red, yellow and black makes Copper. Red, umber and black makes Claret. White, vermillion, blue and yellow makes White, yellow and red makes Dove. Fawn. Red, black, yellow ochre and white, Free stone. French Gray. White, Prussian blue and gray, White, stone other and red makes Gold. White and chrome vellow makes. Lemon. White, yellow ochre, black and red, Limestone. White and vermillion, makes, White, vermillion and Lake makes. Peach. Pink. White, yellow ocher, black and red. Sandstone. Red, blue and white makes. Violet.

#### COMBINATION of INK that HARMONIZE WELL.

Two Colors.—Scarlet Red and Deep Green; Orange and Violet; Light Blue and Deep Red; Yellow and Blue; Black and Salmon; Black and Light Green; Dark and Light Blue; Carmine and Emerald; Brown and Carmine; Purple and Green. Three Colors.—Red, Yellow and Blue; Orange. Black and Light Blue; Light Salmon, Dark Green and Scarlet; Brown, Light Orange and Purple; Dark Brown, Orange Yellow and Blue; Crimson Lake, Greenish-Yellow and Black. Four Colors.—Black, Green, Dark Red, and Sienna; Scarlet, Dark Green, Lavender and Black; Ultramarine or Cobalt Blue, Vermillion, Bronze Green, and Lilac; Sienna, Blue, Red and Black.

# NEWSPAPER MEASUREMENT.

Table showing number of ems of the different Newspaper Type in a line, the number of lines necessary to make 1.000 ems, and the length in inches. Also the number of ems in the regular length of (13 em Pica wide) columns.

	Aga- te.	Nonp.	Min- ion.	Bre- vier.	Bourg	Long Prim.
No. ems in line. No. lines 1.000 ems. No. In. 1.000 ems.	281/ <sub>3</sub> 351/ <sub>3</sub> 22/ <sub>3</sub>	26 381/ <sub>2</sub> 31/ <sub>4</sub>	221/4 45 43/8	191/ <sub>2</sub>  511/ <sub>3</sub>  52/ <sub>3</sub>	171/ <sub>3</sub>   572/ <sub>3</sub>   71/ <sub>4</sub>	151/ <sub>2</sub> 641/ <sub>2</sub> 9
No. Columns.	N	o. ems	in C	ol. Fo	lio or C	uarto.
4 5	$\begin{bmatrix} 5.040 \\ 6.505 \end{bmatrix}$	5.615	4.115	3.200		1.610 2.085
6 7	7.180 7.900	6.785	4.970	3.510 3.865	3.050	2.290 2.520
8	8.630 9 310			4.220	3.330	2.755

#### LEADS FOR NEWSPAPER.

Table showing the number of Leads 13 ems Pica long, contained in one pound and the number required to lead 1.000 ems of matter, together with the number of leads in a single column of matter regular size newspaper.

Size of Body Type to be Leaded with 6-to-Pica Leads.

	Aga- te.	Non- pareil			Bour- geois.	Long Prim
No. Leads to fb. "1.000 ems.	60 26	60 29	60 34	60 40	60 45	60 52
No. of Columns.	No.	Leads	in Col.	Folio	or Qua	arto.
4	132	125	108	99	88	84
5	170	162	140	128	114	108
6	185	179	154	141	125	119
7	206	197	169	155	138	131
8	224	215	185	169	150	143
9	241	233	201	183	163	154

# STANDARD SIZES OF NEWSPAPERS.

The following are the regular size, adopted by the auxiliary printers. We would advise parties planning new newspaper to adopt one of these sizes. The width of column is 13 ems.

No. Col-		FOL10.		
umns.	Size of Paper	Size of Form	Head Rule.	Col.Rule.
5	20 by 26	1734. by 2334	111/8	173/4
6	22 " 31	1934 " 2814	1338	193/4
7	24 " 35	2134 " 33	153/4	213/4
8	26 " 40	233/4 " 371/2	18	233/4
9	28 * 44	253/4 ** 42	201/4	253/4
		QUARTO.		
4	22 by 31	1834 by 29	87/8	1 133/4
5	26 " 40	231/4 " 37	111/8	1734
6	30 ** 44	2734 " 41	133/8	193/4
7	35 " 48	321/2 " 45	153/4	213/4

#### STANDARD NEWSPAPER MEASURE.

The STANDARD newspaper measure, as recognized and now in general use, is 13 Ems PICA. The Standard of Measurement of all sizes of Type is the Em QUAD, not the letter m.

#### LEADS and SLUGS.

Leads are designated as "—to-Pica," the number being that fraction of a Pica which the lead is, viz: a 6-to-Pica lead is one-sixth of a Pica in thickness, or six 6-to-Picas are equal to one Pica; four 4-to-Picas one Pica, and so

with other sizes or thickness of leads.

SLUGS.—Leads of Nonpareil thickness and greater are called Slugs, viz: Nonpareil Slugs, Brevier Slugs, Pica Slugs, etc., a Pica is one-sixth of an inch nearly.

#### AVERAGE WEIGHT OF MATTER.

A piece of solid matter 13 Ems Pica wide and 6 inches long will weigh *about* 33g pounds, but in order to allow for the sorts usually remaining in the case, 43g pounds of Type would be required to set that amount of solid matter.

When the matter is to be *leaded* the weight of the Type may be reduced about one quarter.

A piece of solid matter 12 inches square will weigh about 40 pounds. One pound of Type will therefore, measure 33/8 square inches. A piece of leaded matter 12 inches square will contain about 30 pounds of Type.

#### Leads Required for Newspaper and Book Work.

To lead 1 lb., of Pearl requires 6 ounces of 6-to-Pica leads, Agate 51/2 ounces, Nonpareil 5 ounces, Minion 41/2 ounces, Brevier 4 ounces. Bourgeois 31/2 ounces, Long Primer 3 ounces, Small Pica 23/4 ounces, Pica 21/2 ounces, English 21/4 ounces.

#### COLORED PRINTING-PAPER.

Are made either by adding coloring-matter to the pulp, or, when peculiarly brilliant colors are required, by painting or staining the paper. By the use of both processes a great variety of shades is produced. In printing on colored papers, it should be remembered that the appearance of the ink is affected by the color of the paper. When black letters appear on a colored surface-ground, they lose the intense hue they have when printed on white paper. On blue they are a failure; on orange (red lead) they are telling and brilliant, and assume a greenish bronze, on violet they are rich, in a Greenish-Yellow tone; the majority of yellows are weakened by black, which is thus rendered more intense. It should be remembered that—

- 1. Black Ink upon Red appears Dark Green.
- 2. Black Ink upon Orange, Bluish-black.
- 3. Black Ink upon Yellow is Black, with a slight tinge of Violet.
  - 4. Black Ink upon Blue is Orange-gray.
  - 5. Black Ink upon Green appears Reddish-gray.
  - 6. Black Ink upon Violet appears Greenish-yellow-gray.

#### MARKS OR PUNCTUATIONS.

-	Commo	4	Cedilla.
,	Comma.		
- ;	Semicolon.	Λ	Caret.
:	Colon.	" "	Quotation Marks.
	Period.		
_	Dash.	}	Brace.
?	Interrogation.	(	
1	Exclamation.	***	Ellipsis.
()	Parenthesis.		Ellipsis; also leaders.
É	Brackets or Crotchets		Ellipsis.
-	Hyphen.	*	Asterisk.
,	Apostrophe.	†	Dagger, or Obelisk.
1	Acute Accent.	1 1	Double Dagger.
1	Grave Accent.	S	Section.
^	Circumflex Accent.		Parallels.
47	Circumflex or Tilde.	T	Paragraph.
-	The Long or Macron.	1250	Index.
U	The Short or Breve.	*** or ***	Asterism.
•••	Diæresis.		

#### CORRECTIONS OF THE PRESS.

a, or a, (dele) Delete, take out, or expunge.

9 Turn a reversed letter.

- \* A space, or more space between words, letters, or lines. Less space, or no space, between words or letters.
- L or I carry a word further to the left or to the right.

□ Indent.

- Elevate a letter, word, or character that is sunk below the proper level.

Sink or depress a letter, word, or character raised above

the proper level.

Shows that a portion of a paragraph projects laterally beyond the rest. L Directs attention to a quadrat or space which improp-

erly appears.

 $\times$ , or + directs attention to a broken or imperfect letter. Bring a words or words to the beginning of a line; also, make a new paragraph.

¶ Make a new paragraph. — Change from Italic to Roman, or from Roman to Italic, as the case may be.

= Put in small capitals.

Put in Capitals.

Note.—The other marks are self-explanatory; but the following observations used in correcting proof-sheets,

require explanation:-

wf. Wrong font; -used when a character is of a wrong size or style; tr., Transpose; l.c., Lower-case; i. e., put in small or common letters a word or letter that has been printed in capitals or small capitals; s. caps, or sm. c., Put in small capitals; Qu., Qy., or? Query; Out, s. c. words are wanting, see copy.

#### FIRST PROOF FROM THE TYPE.

#### THE CROWNING OF PETRARCH.

Nothing can be conceived more affecting or noble than that ceremony. The superbe palaces and porticos by which had rolled the ivory chariots of Marius and and Caesar had long mouldered into dust. The laureled fasces, the golden eagles, the shouting Legions, the cap tives, and the pictured cities were indeed wanting to his victorious procession. The sceptre had passed away from Rome. But she still retained the mightier influence of an empire intellectual and was now to conter the prouder reward of an intellectual trinmph. To the man who had extended the dominion of her ancient language who had erected the trophies of philosophy and imagination in the haunts of ignorance and fervency. whose captives were the he arts of admiring nations; enchained by the influence of his songwhose spoils were the treasures of ancient genius-the Eternal City offered the glorious and just tribute of her gratitude.

Amid the ruined monuments of ancient, and the infant eructions of modern art, he who had restored the broken link between thetwo ages of human civilization was crowned with the wreath which he had deserved from the moderns who owde to him their refinement—from the ancients who owed to him their fame Never was a coronation so august witnessed by westminister or Rheims.

MACAULAY.

#### A CORRECTED PROOF SHEET.

# Caps. THE CROWNING OF PETRARCH. D Nothing can be conceived more affecting or a capon noble than that ceremony. The superbe palmaces and porticos by which had rolled the ivory chariots of Marius and and Caesar had long at mouldered into dust. The laureled fasces, the golden eagles, the shouting Legions, the capa Itives, and the pictured cities were indeed wanting to his victorious procession. The sceptre had passed away from Rome. But she still retained the mightier influence of an emby pirelintellectual, and was now to conter the stel prouder reward of an intellectual trimmph. To a the man who had extended the dominion of her ancient language who had erected the trophies of philosophy and imagination in the L haunts of ignorance and fervence Collean whose captives were the he arts of admiring shore bel. nations; enchained by the influence of his songwhose spoils were the treasures of ancient gen-Rom ius the Eternal City offered the glorious and & just tribute of her gratitude. Not Amid the ruined monuments of ancient, and the infant eructions of modern art, he ! who had restored the broken link between # [thetwo ages of human civilization was crowned with the wreath which he had deserved from the modern's who owde to him their refinement to. -from the ancients who owed to him their x O tame Never was a coronation so august witnessed by westminister or Rheims. Leaved from obscurty and decay

#### PROOF SHEET CORRECTED.

#### THE CROWNING OF PETRARCH.

Nothing can be conceived more affecting or noble than that ceremony. The superb palaces and porticos by which had rolled the ivory chariots of Marius and Cæsar had long mouldered into dust. The laureled fasces, the golden eagles, the shouting legions, the captives, and the pictured cities were indeed wanting to his victorious procession. The scepter had passed away from Rome. But she still retained the mightier influence of an intellectual empire and was now to confer the prouder reward of an intellectual triumph. To the man who had extended the dominion of her ancient language who had erected the trophies of philosophy and imagination in the haunts of ignorance and ferocity, whose captives were the hearts of admiring nations, enchained by the influence of his song-whose spoils were the treasures of ancient genius rescued from obscurity and decay-the "Eternal City" offered the just and glorious tribute of her gratitude. ruined monuments of ancient, and the infant erections of modern art, he who had restored the broken link between the two ages of human civilization was crowned with the wreath which he had deserved from the moderns who owed to him their refinement.-from the ancients who owed to him their fame. Never was a coronation so august witnessed by Westminister or Rheims.

Macauleu.

# COMPLETE TABLE OF SIGNATURES.

# EIGHT VO.

				IGHI	<b>v</b> O .			
1	1	A	369	47	2 W	729	 92	4 R
1 9 17 25 33	1 2 3 4 5 6	B	377	48	2 X	737	93	4 R 4 S 4 T 4 U
17	ទី	č	385	10	5 V	745	94	$\hat{4}  \widetilde{\mathbf{T}}$
95	Ä	ň	393	49 50	57	745 753	95	$\frac{1}{4}$ $\hat{\mathbf{U}}$
90	ž	두	401	51	9 4	761	96	4 77
00	อ	井	401	51	O A	701	90	4 V
41	Ď	E.	409 417	52	2 B	769	97 98	4 W
49	7	G	417	53 54 55 56 57 58	3 C	777	98	4 X
57	8	H	425	54	3 D	785	99 100 101 102	4 Y
65	9	1	433 441	55	3 E	793	100	4 Z
73	10	K	441	56	3 F	801	101	5 A
81	11	L	449	57	3 G	809	102	5 B
89	12	M	457	58	3 H	817	103 104 105	5 C
97	13	N	465	59	3 T	825	104	5 D
105	14	0	473	60	3 K	833	105	5 E
113	15	Ď	491	59 60 61	3 T.	841	106	517
121	16	5	400	62	3 M	840	106 107	5 G
190	17	ď	449 457 465 473 481 489 497 505	63	9 M	057	100	5 11
107	10	n.	194	03	9 74	001	100	ភូក
157	10	2	900	64 65 66 67	3 U	605	109	9 I
140	19	T.	513	60	3 P	873	110	ãϔ
153	20	Ū	521	66	3 Q	881	111	5 L
161	21	V	529	67	3 R	889	112	5 M
169	22	W	537	68	3 S	897	113	5 N
177	23	X	513 521 529 537 545 553 561 569 577 585 593 601	68 69	3 T	761 769 777 785 793 801 809 817 825 833 841 849 857 865 873 881 889 905	114	50
185	24	Y	553	70	3 U	913 921 929 937 945 953 961 969 977 985 993 1001	115	5 P
193	25	Z	561	71	3 V	921	116	5.0
201	26	2 A	569	72	3 W	929	117	5 Ř
209	27	$\tilde{2}\tilde{B}$	577	73	3 X	937	118	5.5
217	58	2 č	585	74	š V	945	110	5 7
225	20	2 D	509	75	37	053	120	5 11
222	20	5 TF	601	76	1 1	061	120	5 17
941	91	4 E	600	70	4 D	901	160	5 W
040	91	2 F	009	17	4 D	909	122	9 W
249	34	2 (7	017	78	40	977	125	9 A
Z07	55	ZН	625	79	4 D	985	124	ĐΥ
265	34	21	633	80	4 E	993	125	5 Z
273	35	2 K	641	81	4 F	1001	126	6 A
281	36	$2\mathrm{L}$	649	82	4 G	1009	127	6 B
289	37	2 M	657	83	4 H	1017	128	6 C
297	38	2 N	665	84	41	1025	129	6 D
305	39	20	673	85	4 K	1033	130	6 E
313	40	2 P	609 617 625 633 641 649 657 665 673 681 689 697	72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88	4 T.	1009 1017 1025 1033 1041	131	6 F
321	41	20	689	87	4 M	1049	132	6 G
329	4.2	2 B	697	88	4 N	1057	133	6 H
337	43	25	705	89	4.0	1065	134	6 T
345	4.1	2) m	705 713	90	4 D	1073	195	6 V
41 49 57 65 78 81 89 97 105 113 121 129 137 145 153 161 193 201 225 233 241 249 225 273 2265 273 2265 305 305 313 329 337 345 365 365 365 365 365 365 365 365 365 36	8 9 10 11 12 14 15 16 17 18 19 22 22 24 25 6 27 28 30 31 32 33 34 35 36 36 39 40 44 44 44 44 44 44 44 44 44 44 44 44	BCDEFGHIKLMNOPQRSTUVWXYZABCDEFGHIKLMNOPQRSTUV 222222222222222222222222222222222222	721	91	WXYZABCDEFGHIKLMNOPQKSTUVWXYZABCDEFGHIKLMNOPQ	1073	108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 131 132 133 134 135 136 131 131 132 133 134 135 136 137 138 139 139 139 139 139 139 139 139 139 139	VWXYZABCDEFGHIKLMNOPQRSTUVWXYZABCDEFGHIKL
361	46	2 V	121	91	4 Q	1001	190	OT
201	46	ZV	1			1		

# 12 MO AND 18 MO.

***************************************						
1	1 A	301	26 2 A	601	51 3 A	
5	1* A2	305	26* 2 A <sup>2</sup>	605	51* 3 A2	
13	2 B 2* B <sup>2</sup> 3 C 3* C <sup>2</sup>	313	$\overline{27}$ $\overline{2}$ $\overline{B}$	613	52 3 B	
17	2* B2	317	27* 2 B2	617	52* 3 B <sup>2</sup>	
25	3 C	325	20 20	625	53 3 C	
$\frac{29}{29}$	3* C2	900	00+ 0 C2	029	52* 3 B <sup>2</sup> 53 3 C 53* 3 C <sup>2</sup> 54 3 D	
29	4 D	329	28° 2 0°	629	53* 3 C <sup>2</sup>	
37	4 D	337	29 Z D	637	54 3 D	
41	4* D <sup>2</sup>   5 E E <sup>2</sup>	341	27* 2 B2 28 2 C 28* 2 C <sup>2</sup> 29 2 D 29* 2 D <sup>2</sup> 30 2 E	641	54* 3 D <sup>2</sup>	
49	5 E	349	30 2 E	649	55 3 E	
49 53	5* E <sup>2</sup>	353	30* 2 E <sup>2</sup> 31 2 F	653	55 3 E 55* 3 E² 56 3 F 56* 3 F² 57 3 G 57* 3 G²	
61	6 F	361	31 2 F	661	56 3 F	
61 65	6* F <sup>2</sup>	365	31* 2 F <sup>2</sup>	665	56* 3 F2	
73 77	$egin{array}{cccc} 6 & \overline{F} \\ 6* & F^2 \\ 7 & G \\ 7* & G^2 \\ 8 & H \end{array}$	373 377 385	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	673 677	57 ' 3 G	
77	7* G2	377	32* 2 G <sup>2</sup>	677	57* 3 (3)	
85 89 97	k H	385	33 2 H 33* 2 H <sup>2</sup>	685	50 9 11	
80	8* H <sup>2</sup>	389	93* 9 112	680	50x 9 H	2
07	9 I	397	34 2 1	689 697	90. 9 U	
101	4 D 4* D <sup>2</sup> 5 E 5* E <sup>2</sup> 6 F 6* F <sup>2</sup> 7 G 7* G <sup>2</sup> 8* H 9* I <sup>2</sup> 9* I <sup>2</sup> 10* K 10* K <sup>2</sup>		$\frac{34}{34}$ * $\frac{21}{21^2}$	097	58 3 H 58* 3 H 59 3 I 59* 3 I <sup>2</sup> 60 3 K	
101	9* 12	401	34* 21'	701	59* 3 12	
109	10 K	409	35 2 K 35* 2 K <sup>2</sup>	709	60 3 K	
113	10* K <sup>2</sup>	413	35* 2 K <sup>2</sup>	713	60* 3 K	
121	11 L	421	36  2  L	721	61 3 L	
125	11* L <sup>2</sup>	425	36* 2 L <sup>2</sup>	721 725	61* 3 L <sup>2</sup>	:
133	12 M	433	37 2 M	733	62 3 M	
137	9* 12 10 K 10* K <sup>2</sup> 11 L 11* L <sup>2</sup> 12 M 12* M <sup>2</sup>	437	37* 2 M <sup>2</sup>	733 737	62* 3 M	2
145	13 N	445	38 2 N	745	63 3 N	
149	13 N 13* N²	449	36 2 L 36* 2 L <sup>2</sup> 37 2 M 37* 2 M <sup>2</sup> 38 2 N 38* 2 N <sup>2</sup>	749	58 3 H 58* 3 H; 59* 3 I² 60* 3 K; 61* 3 L; 62* 3 M 62* 3 M 63* 3 N; 64* 3 O; 64* 3 O; 65* 3 P; 66* 3 Q; 67* 3 R;	2
157	14 0	457	39 20	757	64 3 0	
161	14 O 14* O <sup>2</sup> 15 P 15* P <sup>2</sup> 16 Q 16* Q <sup>2</sup>	461	$\frac{39}{39} \times \frac{20}{20^2}$	761	64* 3 03	
169	15 D	469	40 2 P	769	65 9 D	
173	10 I 15* D2	473	40* 2 P2	773	00 0 F	5
	10. 1.	410	41 2 0	7701	09. 9 1.	
181	16 Q	481 485	41 Z Q	781 785	66 3 Q	
185	19* Öz	485	$41* 2 Q^{2}$	785	66* 3 Q	2
193	17 Ř 17* R²	493	42 2 R 42* 2 R <sup>2</sup>	793 797	67 3 R	_
197	17* R <sup>2</sup>	497	42* 2 R <sup>2</sup>	797	$67*$ 3 $\mathbf{R}^3$	s
205	18 S 18* S <sup>2</sup>	505	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	805	68  3  S	
209	18* S <sup>2</sup>	509	$43* 2 S^2$	809	$68* 3 S^{2}$	
217	19 T 19* T <sup>2</sup>	517	44 2 T 44* 2 T <sup>2</sup>	817	68 3 S 68* 3 S <sup>2</sup> 69 3 T 69* 3 T <sup>2</sup> 70 3 U	
221	19* T2	521	44* 2 T <sup>2</sup>	821	69* 3 T	ž
229	20 U	529 533	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	829	70 3 U	
233	20* U2	533	45* 2 II2	833	70* 3 U	ž
$\frac{241}{241}$	21 V	541	$\frac{16}{46}$ $\frac{5}{2}$ $\overset{\circ}{V}$	841	71 3 V	
$\frac{511}{245}$	21 V 21* V2	545	$46* 2 \mathbf{\hat{V}}^2$	845	71* 3 V	ŗ
253	99 107	553	47 9 707	853	79 9 W	
257	99* W	557	47 2 W 47* 2 W <sup>2</sup>	857	51* 3 A B B C C 51* 3 B C C 52* 3 B C C 52* 3 B C C 53* 3 B C C 54* 3 B E F 55* 3 E F 55* 3 E F 55* 3 E F 60* 3 K K K C C 61* 3 B M N N O C C 61* 3 B M N N O C C 61* 3 B M N N O C C 61* 3 B M N N O C C 61* 3 B M N N O C C 61* 3 B M N N O C C 61* 3 B M N N O C C C C C C C C C C C C C C C C C	7
$\frac{297}{265}$	09 V	565	40 9 W	865	72" 3 W	
	22 W 22* W2 23 X 23* X2		48 2 X 48* 2 X <sup>2</sup>		10 5 A	
269	13 N N 1 14* N O 14* P P 15* P Q 2 11* P P 16* Q 2 11* R 2 19* T 2 20* U 20* U 20* U 20* W 22* W 22* X 23* X 24* Y 2 24* Y 24*	569	40° Z X²	869	72 3 W 72* 3 W 73 3 X 73* 3 X <sup>2</sup> 74 3 Y 74* 3 Y <sup>2</sup>	
277	24 Ŷ 24* Ŷ	577	49 2 Y	877	74 3 X	
281	24* Y <sup>2</sup>	581	49* 2 Y <sup>2</sup>	881	74* 3 Y <sup>2</sup>	
289	25 Z 25* Z <sup>2</sup>	589	26* 2 A 2 2 B 2 2 C 2 A 2 2 T 2 T 2 B 2 2 C 2 D 2 2 E F 2 2 C 2 D 2 2 E F 3 3 2 2 E F 3 2 E E E E E E E E E E E E E E E E E E	889	75 3 Z	
293	25* Z <sup>2</sup>	593	$50* 2 \mathbb{Z}^2$	893	75* 3 Z <sup>2</sup>	

I 6MO AND 24MO.

		5 /			
	16 MO.		24 I	MO.	
1		1	1 A 1	401	PZ
1 17	1 A 2 B 3 C 4 D 5 E 6 F 7 G 8 H 9 I	o d	1 A	409	18 S
17	ZB	9 17		409	18 S
33	3 C	17	A2	417	18*
49 65	4 D	25	2 B	425	19 T
65	5 E	33	2*	433	19 T
00	9 E			400	19 1
81	6 F	41	B <sup>2</sup>	441	19*
97 113	7 G	49	3 C	449	Τž
112	8 H	57	2*	457	20 Ū
110	0 1				20 Ū 20*
129	9 I	65	C <sup>2</sup>	465	20*
145	10 K 11 L	73	4 D	473	$\Pi_{\bar{2}}$
161	11 L	81	4*	481	21 V
177	12 M 13 N	89	$D^2$	489	21*
111	14 11			405	41"
193	13 N	97	5 E	497	V 2
209	14 0	105	5*	505	22 W 22*
225	15 P	113	$\mathbf{E}^{2}$	513	99*
241	16 Q	121	6 F	521	W₹
241	10 Q	1.21	O F		OC T
257	17 Ř	129	6*	529	23 X 23*
273	18 S	137	$\mathbf{F}^2$	537	23*
289	15 P 16 Q 17 R 18 S 19 T 20 U	137 145	7 G 7*	545	24 X <sup>2</sup>
200	20 Ū	153	7 U	550	- 24 7
305	20 0	193		553	24 Y
321	21 V	161	G <sup>2</sup>	561	24*
337	22 W 23 X	169	8 H	569	25 Z
353	23 X	177	Q*	577	95 7
999	- 04 X	107			25 <b>Z</b> 25*
369	24 Y	185	$H^2$	585	25*
385	24 Y 25 Z	193	9 I 9*	593 601	26 2 A
401	26 2 A 27 2 B 28 2 C 29 2 D	201	9*	601	26 2 A
417	97 9 D	209	$I^2$	609	26*
	41 4 D	217	10 77	003	40"
433	28 2 C	217	10 K	617	2 A <sup>2</sup>
449	29 2 D	225	10 K 10*	625	$\begin{array}{ccc} 2 & \mathbf{A^2} \\ 27 & 2 & \mathbf{B} \end{array}$
465	30 2 E	233	K <sup>2</sup>	633	27 2 B 27*
481	31 2 F	241	11 L	641	0 De
	01 4 F		11 11		2 B <sup>2</sup> 28 2 C
497	$3\overline{2}$ $\overline{2}$ $\overline{G}$	249	11*	649	28 2 C
513 529	33 2 H	257	$L^2$	657	28 2 C 28*
529	34 2 T	265	12 M	665	2 C <sup>2</sup>
545	34 2 I 35 2 K 36 2 L 37 2 M	273	12*	665 673	29 2 D
501	00 4 IX	210		075	29 2 D 29*
561	36 2 L	281	M <sup>2</sup>	681 689 697 705	29*
577	37 2 M	289	13 N 13*	689	$2 D^2$
593	38 2 N	297	13*	697	30 2 F
609	39 20	305	NT9	705	30 2 E 30*
	99 4 U	505	N2	700	5U <sup></sup>
625 641 657 673 689 705 721	40 2 P	313	14 O 14*	713	31 2 E <sup>2</sup> 31 2 F
641	41 2 Q	321	14*	721	31 2 F
657	$\hat{42}$ $\hat{2}$ $\hat{R}$	329	O <sup>2</sup>	720	$\begin{array}{cc} 31 & \overline{2} \ \overline{\mathbf{F}} \\ 31 \end{array}$
672	43 2 S	997	15 D	729 737	O T20
073	45 45	337	15 P 15*.	131	32 · 2 F <sup>2</sup> 32 · 2 G
689	44 2 T	345	15*.	745	32 2 G
705	45 2 U	353	$P^{\overline{2}}$	753	32 2 G 32*
721	46 2 V	361	16 Q	761	2 G <sup>2</sup>
727	47 O W	901	16 Q 16*	101	20"
737	47 2 W	369	16*	769 777	$\frac{33}{33*}$ $\overline{\overset{\circ}{2}}$ $\overline{\overset{\circ}{H}}$
753	48 2 X	377	O.z	777	33*
769	Ž A B C D E F G H I K L M N O P Q R S T U V W X Y Z 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	385	17 R	785	$2 H^{z}$
785	$50\ 2\ z$	393	17*	793	34 2 Î
100	00 4 L	030	11"	193	34 Z I

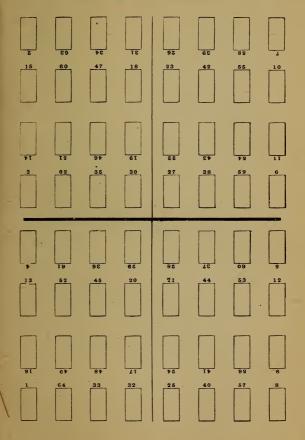
# IMPOSITION OF FORMS.

	11110	SITION	OFFO	RMS.	
A HALF-S	SHEET OF	SEVENTY-TY	vcs, with	THREE SIGI	NATURES.
49	9 8	9 5	3.5	7	•
72	9	4	14	18	200
6.0	89	\$50	4	19	51
57	10 10	80	3.9	c	e
63	92	39	æ	13	9
558	66	34	35	12	<b>a</b>
57	09	. ω ω	98	11	10
57	61	33	37	11	16
64	61	40	25		
0.0 4	6.6	40 27	30	14	10

# POCKET COMPANION.

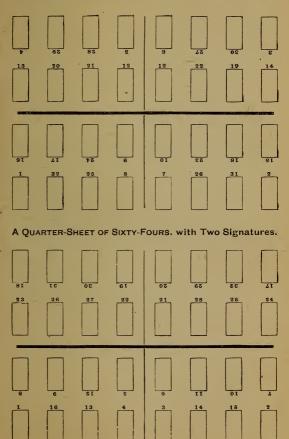
121

A HALF-SHEET of SIXTY-FOURS.



122 HANDY MECHANICAL,									
A HALF-SHEET of FORTY-EIGHTS, with Two Signatures.									
7	18	19	£	92	42	91	30		
11	14	15	10	35	38	39	34		
žī	ET	91	9	98	75	05	23		
8	21	02	9	28	T.F.	<b>₽₽</b>	62		
1	24	21	4	25	48	4.5	28		
A F	HALF-SH	EET of	TWENTY	-Fours,	withou	t Cutti	ng.		
8	20	17	8	7	18	19	6		
,	TZ	9 î	6	ot	ğī	22			
	24	13	12		14	23	2		

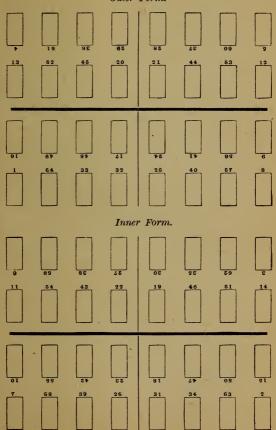
A COMMON QUARTER-SHEET of SIXTY-FOURS,



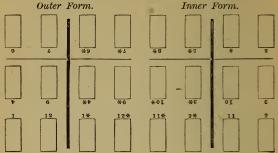
124	HANDY MECHANICAL,								
'A HALF-SHEET of FORTY-EIGHTS, with Three Signatures.									
7E 39	42	97	38	98	97	81	£ € € €		
81	18	30	61	20	62	35	41		
23	26	27	22	21	28	25	24		
8	6	12	9	9	11	01	4		
		13	4	3		15	2		
Α	HALF-S	HEET O	f TWENT	Y-Fours	s, witho	ut Inse	t.		
81	23	5.5	61	20	Tz	Ŧ 5	LI		
8	6	13	9	9	TT.	ot			
1	16	13	4	3	14	15	2		

# A SHEET of THIRTY-TWOS.

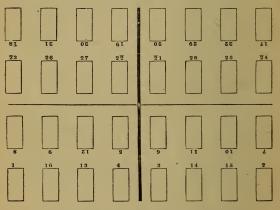
Outer Form.



Two Half-Sheets of Twelves Worked Together.



A HALF-SHEET of THIRTY-Twos with Two Signatures.



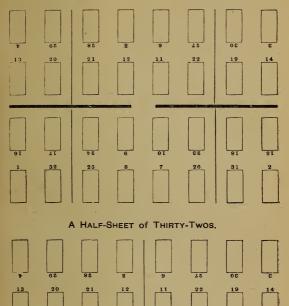
Six Page Leaflet. First Page to the Left.

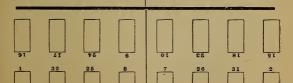


A SHEET OF SIXTEENS, With one Signature.

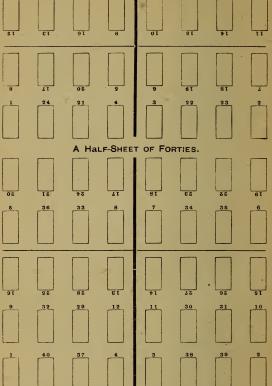
Outer Form.

Inner Form.



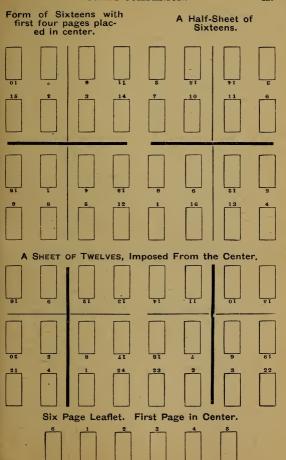


# A HALF-SHEET OF TWENTY-FOURS.



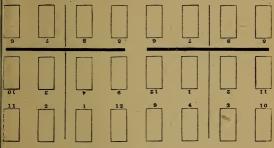
Six Page Leaflet. First Page to the Right.





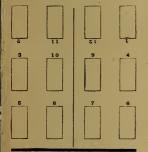
Outer Form of a Sheet of Twelves.				Inner Form of a Sheet of Twelves.				
Zī	E 1	īe	6	oi	gī	71	II	
8	LT	02	9	9	61	81		
	24	21		3	22	23	2	
A SHEET OF TWENTIES. Outer Form. Inner Form.								
50	12	54	21	st	\$3	22	61	
5	36	33	8	7	34	35	6	
91	5.6	88		+1		92	91	
9	32	29	12	11	30	31	10	
1	40	37	4	3	38	39	2	

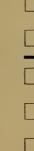
Different Method of Imposing Half-Sheets of Twelves, from the Center.



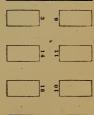
A Half-Sheet of Twenties, with Two Signatures.





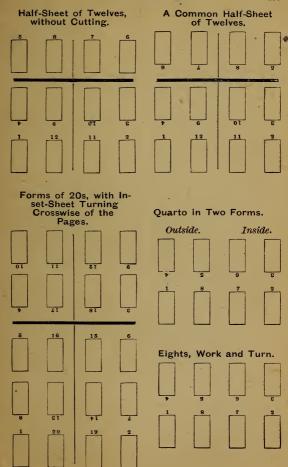






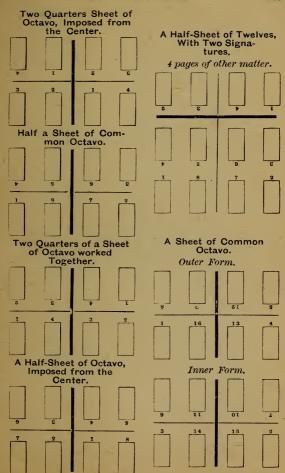
A SHEET OF TWELVES With Two Signatures.

	Outer.		Inner Form.				
02	12	54	21	SI	23	22	6
. 8	6	21	9	9	II	ot	
1	16	13	4	3	14	15	
Α	HALF-SI	HEET OF	THIRTY	-Sixes,	Withou	t Cutti	ng.
	2	38	9 <u>c</u>	Į, i	Fi	23	
	3	. 34	27	10	15	27	
	9	T E	30		81	61	
	5	32	29	8	17	20	
		EE	88		197	12	
	1	36	25	1 2	13	24	



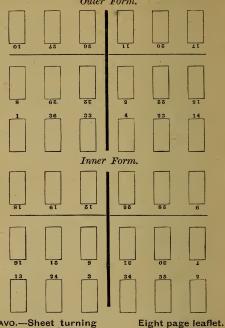
# HANDY MECHANICAL,

# A SHEET OF TWELVES Without Cutting. Outer Form. Inner Form. A HALF-SHEET OF THIRTY-SIXES.

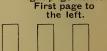


A SHEET OF EIGHTEENS, with One Signature.

Outer Form.

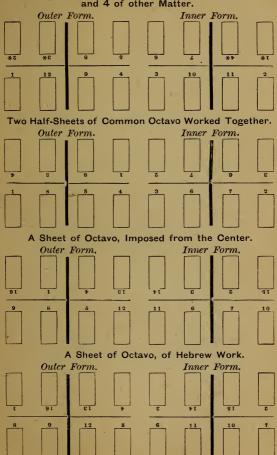


OCTAVO.---Sheet turning lengthwise of the pages.



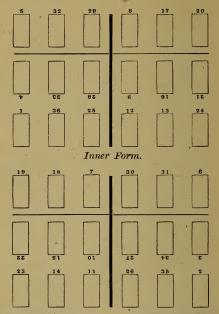


A Sheet of Octavo, 12 of the Work and 4 of other Matter.



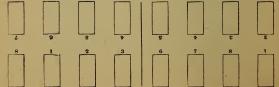
A SHEET OF EIGHTEENS to be Folded Together.

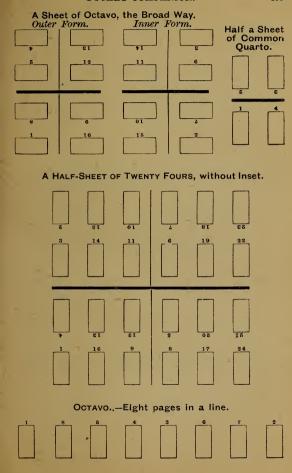
Outer Form.



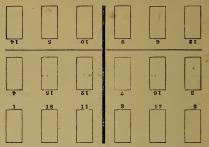
Eight page leaflet. First Page next to the left.

Eight page leaflet. First page to the right.



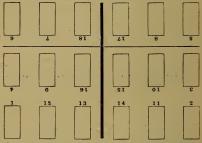


#### A HALF-SHEET OF EIGHTEENS.



When the paper is worked off, transpose the pages 11 and 8 in the place of 7 and 12, and pages 7 and 12 in place of 11 and 8.

# A Half-Sheet of Eighteens, without Transposition.



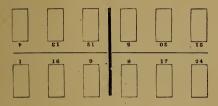
This form of imposition will give three single leaves when the sheet is cut, and should therefore be avoided where possible.

# Broad Eights, in Two Forms. Outside. Inside.

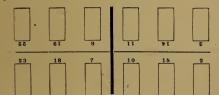


## A SHEET OF LONG TWELVES.

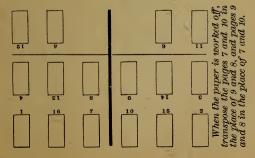
Outer Form.



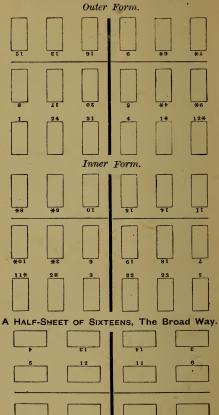
Inner Form.



A HALF-SHEET OF EIGHTEENS, (Containing 16 pages).



A SHEET OF EIGHTEENS, with Two Signatures.

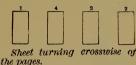


16

#### QUARTO. Sheet turning lengthwise of the page.



### QUARTO.



Convenient for Leaflets,
Price Lists etc.

# AMERICAN AND GERMAN TYPE.

GERMAN NAME. AMERICAN NAME. 811 1 1/2 petit American 14 541 German 1/2 cicero 23 14 petit Saxon 405 Brilliant 1/4 cicero 203 45678 Diamant Diamond 162 Perl Agate Nonpareille Nonpariel 135 115 Colonel Brevier 101 Petit Bourgeois Long-primer  $\tilde{9}$ 90 90 Borgis Garmond Small-pica 10 81 80 Cicero Pica 12 68 14 58 57 Mittel English 16 51 Tertia Great-primer Doppelborgis Paragon 18 45 45 Double S. pica Text 20 41 40 Double pica "Columbian 34 Doppelcicero  $\bar{28}$ Doppelmittel Kleine canon Gr't Primer 32 36 Canon or dreicicero Paragon Grobe canon 40 Meridian 31/2 cicero 3 line Columbian 42 19 Kleine missal or viercicero 48 18 Canon 41/2 cicero 3 line Paragon 54 15 15 "S. pica Grosse missal 14 13 60 Kleine sabon 11 11 Paragon

# DECIMAL APPROXIMATIONS FOR FACILI-TATING CALCULATIONS.

Avoirdupois pounds	s multipl	ied by .009	equals	Cwts.
	• • • • • • • • • • • • • • • • • • • •	.304		Tons.
Lineal feet		.000	119	Miles.
" yards		.000		uare feet.
Square Inches.	66	" .111		"Yds.
" Feet. " Yards.	66		2067 '	" Acres
Circular Inches	6.6			" Feet.
Cylindrical "	66			Cubic "
" Feet	44	" .029		" yds.
Cubic Inches	66	" .000		" Feet.
" Feet.	4.6	.037		" Yds.
	. 66	" .623	2 "In	iper'l g'ls.
" Inches	'66	.0036		44 -46
Cylindrical Feet	4.6	4.895		66 66
" Inches	66	" .0028		"
Cubic "	66	" .263		bs. Avoir.
" "	44		( )	Cast-Iron.
" "	**	".281 ".283	"	r'gt Iron.
"	"	" .3225	4.6	Steel. Copper.
"	**	.3037	66	Brass.
"	66	".26	6.6	Zinc.
	66		66	Lead.
"	• 6	" .2636	6.6	Tin.
	66	4908	4.6	Mercury.
Cylindrical Inches	44	.2065	4.6	Cast-Iron.
- 44 44	44	" .2168	" W	r'gt Iron.
**	4.6	" .2223	_ "	Steel.
"	4.6	.2533	66	Copper.
**	66	.2385	66	Brass.
16 66	46	.2042	**	Zinc.
	"	.3223	• •	Lead.
		".207 ".3854	- 66	Tin.
	ıltiplied	3.1416	44	Mercury. Circum.
Diameter of a o mi	mapned	".8862	++ C;	de of=sq.
· 66 '66	4.6		=Side of in	ue ul=sq.
" Sphere	66	" .806		of = Cube.
" Delicio	44 =	" .6667	"Length	
Square of diamet	$\operatorname{er}  imes$ .	7854	" Area o	f a Circle.
Circum. of a Circle	66	31831		Diameter.
Side of a square	66	1.128	" Diam of	f = Circle.
Sq. Root of Area	44,	1.12837	** **	' Square.
Sq. of the diam.				
of a sphere.	. "	3.1416	" Conve	x surface.
Cube. do. do.		.5236		Solidity.
183.346 Circular inc	enes		" 1 Sq	uare foot.

2,200 Cylindrical inches		equals	1 Cubic foot.
Acres	× .4840	) og Garans	Square yards.
Links	.22	44	Yards.
"	" .66	66	Feet.
Feet	" 1.5	66	Links.
Width in chains	" 8.	** <u>1</u>	Acres per Mile.
Cubic feet	" 7.48	**	U. S. gallons.
" Inches	" .0043		U. S. "
Cymnumcal reet.	" 5.874	4.6	U. S. "
тиспер	" .0034		U. S. "
U. S. gallons	.1336		Cubic feet.
U. D. ganons	" 231.	66	Cubic Inches.
Capic reer	.0050	66 44	U. S. Bushels.
" Inches		166 "	U. S. Bushels.
U. D. DUBLIELS	.0490	• • • • • • • • • • • • • • • • • • • •	Cubic yards.
U. D.	1.4440	"	" feet.
U. D.	2150.42	**	michos.
Cylindrical feet of water			U. S. gallons.
Cubic feet of water.	04.5	13.	s avoirdupois.
menes	10001	· · · · · · · · · · · · · · · · · · ·	
Cymrurical reet.	45.11		
inches. 13.44 U. S. gal.	.0284	4 66	
268.8 U. S. "		66	1 Cwt. 1 Ton.
1.8 Cubic feet.		66	1 Cwt.
35.88 " "		66	1 Ton.
	1.273	" 0	ircular Inches.
STEAM		WATER	
Pounds of water, at 62°	" 0.010	6037 equa	
66 66 66	" 1.2	<i>"</i>	Gallons. Imperial gals.
Tons " "	" 35.90	66	Cubic feet.
Gallons per second ×	474.08	Acres Cr	feet per hour.
Gallons per minute "	7.9	equal ou.	reet per nour.
Cu. feet per second "	2.222	" Cn vô	ls. per minute.
Cu. reet per second	133.333	" " " "	" hour.
Cu. feet per minute "	2.222	66 66 66	46 66
Feet of water at 52.3° I		Rennals i	nches of mer-
cury at 32° F.	. / 0.0026	o equally 1	nones of mer
Atmospheres × 14.70	6 equals	pounds ne	r square inch.
2105.66	4		r square foot.
" " 8.50			er square yard.
" 29.92	2 "		es of mercury.
" " 33.96		feet of wa	ater at 52.3° F.
TO CONVER		VEIGHT (	DF-
Wrought-Iron into Cast		multiplie	
Stee		111111111111111111111111111111111111111	1.014
Zinc		66	" 0.918
Bras		66	" 1.082
Copi		66	" 1.144
Lead		4.4	" 1.468

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AN INCH	
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A FOOT FOR EACH 1-32 OF AN INCH	
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	=	.9167	.9193	.9219	.9245	9271	9297	9323	9349	9375	.9401	.9427	.9453	9479	.9505	.9531	.9557	.9583	6096	9635	1996.	8896	.9714	9740	926	9792	.9818
NOH.	10	.8333	.8359	.8385	.8411	.8438	.8464	.8490	.8516	.8542	8928	£628°	.8620	.8646	.8672	8698	.8724	.8750	9228	8802	.8828	8854	0888	9068	8932	8668	.8984
AN IN	6	.7500	.7526	.7552	8121.	.7604	.7630	.7656	.7682	.7708	.7734	.7760	.7786	.7813	.7839	:7865	1881	7167.	.7943	.7969	.7995	.8021	.8047	8073	6608	8125	1618.
1-32 OF	∞	1 2999.	.6693	6719	.6745	.6771	7629.	.6823	.6849	6875	1069.	.6927	.6953	6269.	.7005	.7031	.7057	.7083	.7169	.7135	.7161	.7188	.7214	.7240	.7266	.7292	.7318
EACH	2	.5833	.5859	.5885	.5911	.5938	.5964	.5990	.6016	.6042	8909	.6094	.6120	.6146	.6172	.6198	.6224	.6250	.6276	.6302	.6328	.6354	.6380	.6406	.6432	.6458	.6484
T FOR	9	.5000	.5026	.5052	.5078	.5104	.5130	.5156	.5182	.5208	.5234	.5260	.5286	.5313	.5339	.5365	.5391	.5417	.5443	.5469	.5495	.5521	.5547	.5573	.5599	.5625	.5651
A FOOI	5	.4167	.4193	.4219	.4245	.4271	.4297	.4323	.4349	.4375	.4401	.4427	.4453	.4479	.4505	.4531	.4557	.4583	.4609	,4635	,4661	.4688	.4714	.4740	.4766	.4792	.4818
STS OF	4	.3333	.3359	.3385	.3411	.3438	.3464	.3490	.3516	.3542	.3568	.3594	.3620	.3646	.3672	.3698	.3724	.3750	.3776	.3802	.3828	.3854	.3880	.3906	.3932	3958	.3984
4L PARTS	တ	.2500	.2526	.2552	.2578	.2604	.2630	.2656	.2682	2708	.2734	.2760	.2786	.2813	.2839	.2865	.2891	.2917	. 2943	.2969	.2995	3021	.3047	.3073	3099	.3125	.3151
DECIM	2	.1667	.1693	.1719	.1745	.1772	1797	.1823	.1849	.1875	1061.	.1927	.1953	.1979	.2005	.2031	7502.	.2083	.2109	.2135	.2161	.2188	.2214	.2240	.2266	.2292	.2318
E OF	-	.0833	.0859	.0885	1160.	.0938	.0964	0660	.1016	.1042	.1068	.1094	.1120	.1146	.1172	.1198	.1224	.1250	.1276	.1302	.1328	.1354	.1380	.1406	.1432	.1458	.1484
TABLE	0	0000	.0026	.0052	.0078	.0104	.0130	.0156	.0182	.0208	.0234	.0500	.0286	.0313	.0339	.0365	10301	.0417	.0443	.0469	.0495	.0521	.0547	.0573	.0599	.0625	190.
	Inch.	0	1-37	1-16	3-37	1/2	5-35	3-16	7-32	14	9-32	5-16	11-32	3,5	13-32	7-16	I5-32	1/2	17-32	9-16	19-32	2%	21-32	11-16	23-37	3,4	25-32

Continued).	-		39		Decimals of an Inch.	75 765625 7765625 7786875 7786875 828125 828125 84875 875 890625 921875 921875 9685 9685 96875 96875
.		• •	.8255 .9089 .8281 .9115 .8307 .9141	an INCH.	Fractions f an Inch.	8452464888888888888888888888888888888888
1-32 OF AN INCH		7344 7370 9867	7422	64ths of	Decimals   of an Inch.	5 5116625 54125 541847 548475 548475 548475 640625 640625 636525 63625 641875 71875 71875 71875
7 22 07	- 0	.6536 6536 6536	.6589 .6615 .6641	and		377
		.55773 .5703 .6273	.5755 .5781 .5807	hs, 32ds,	Fractions of an Inch.	7.83.7 2.93.9 3.94.82 5.94.82 7.94.83
FOD F		4844 4870 4896	4922 4948 4974	s, 16ths,		
TABLE OF DECIMAL FARIS OF A FOOT FOR EACH		-4010 -4086 -4063	4089	S of 8ths,	Decimals of an Inch.	25622 286875 286875 3125 328125 328125 34875 359375 390625 40025 40025 4376 4876 48875 48875
20 S.13		3203 2223 2223	.3281 .3281 .3307	EQUIVALENTS		
4L FA	1	2374 2396 2396	2422 2448 2474	EQUIV	Fractions of an Inch	25-64 27-64 27-64 27-64 28-63 28-63 28-63 28-64 28-64 28-64 28-64 28-64 28-64 28-64 28-64 31-64
DECLINA	1	1536	1589	DECIMAL	Decimals of an inch.	015625 03125 046875 046875 048875 078125 09875 1109875 111625 117875 1875 1875 2203125 2203125 234375
S OF		.0570 .0708 .070	07570 07570 0800	DE	Dec of ar	
TABLE	THOM:	13-16 27-32 7.0	29-32 15-16 31-32		Fractions of an Inch.	46444444444444444444444444444444444444

# DECIMAL PARTS OF A POUND (16 oz) REDUCED TO THEIR VALUE IN OUNCES.

Oun- ces.	100th Parts.	Ounces.	100th  Parts	Ounces	100th Parts	Ounces	100th Parts
16 151/2 15 141/2 14 131/2 13 121/2	1.00 .96 .94 .90 .87 .84 .81	12 111/ <sub>2</sub> 11 101/ <sub>2</sub> 10 91/ <sub>2</sub> 9 81/ <sub>2</sub>	.75 .72 .69 .65 .62 .59 .56	8 71/2 7 61/2 6 51/2 5 41/2	.50 .46 .43 .40 .37 .34 .31	31/2 3 21/2 2 11/2 1	.25 .22 .19 .15 .12 .09

# Equivalents of Carats in Decimal parts, unity being Twenty-Four Carats.

Carats.	Decimals.	Carats.	Decimals.	Carats.	Decimals
1 2 3 4 5 6	0.042 0.033 0.125 0.167 0.208 0.250 0.292	9 10 11 12 13 14 15	0.375 0.417 0.459 0.500 0.542 0.583 0.625	17 18 19 20 21 22 23	0.707 0.750 0.792 0.833 0.875 0.917 0.958
8	0.333	16	0.666	24	1.000

# DECIMAL EQUIVALENTS TO FRACTIONAL PARTS OF LINEAL MEASURES.

Inch.         Dec.         Inch.         Dec.         Inch.         Dec. $78 + 3.32 = .96875$ $58 + 1.32 = .65625$ $14 + 3.32 = .3437$ $78 \cdot 1.16 \cdot .9375$ $58 \cdot .625 \cdot .625$ $14 \cdot .166 \cdot .3125$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$

### ONE FOOT OF 12 INCHES.

Inch. De	ec.   Inch.	Dec.	Inch.	Dec.	Inch.	Dec.
11 = .91 10 " .63 9 " .75 8 " .66 7 " .58	338   5 " 5   4 " 366   3 "	.4166 .3333	7/8 " 3/4 "	.0833 .07291 .0625 .05208 .04166	3/8 = 1/4 " 1/8 "	.03125 .02083 .01041

#### SAW-LOGS REDUCED TO INCH BOARD MEASURE.

		-			•			_			
Length in Feet.			1	DIAM	ETE	R IN	N IN	CHE	s.		
e E	$\frac{12 + 13}{12 + 13}$	3   14	15	16   1	17  18	119	20	21   2	2   23	12412	5   26
10	49  61	-			16 138		_	-	09 235		87 313
11	54 67				27 147				30 259		
12	59  78		107	119 13	39 160		210	228 2	51 283	3 303 3	
13	64 79		116 125	$129   10 \\ 139   10$	$50 178 \ 32 187$	195	227 2 245 2	$247   2 \\ 266   2 \\$	72 306 92 330	$\begin{vmatrix} 328 & 3 \\ 353 & 4 \end{vmatrix}$	73 408 01 439
14 15	69 85 74 91			149 1			262		13 353		30 469
16	79 97	1114	142	159 18	85 213	240	280	304 3	34 377	404 4	59 500
17	84 103			168 19		255			55 400		87 531
18 19	89 109   93 116		160 169	178 20	$08 240 \ 19 253$	$\begin{array}{c} 270 \\ 285 \end{array}$			76 424 97 447		16 562 45 594
20	98 122		178			300	350 3		18 470		73 625
21	103 128	150			43 280	315	368				03 656
22	108 134 113 140		196	218 20 $228 20$	55 293	330 345		118 46 137 48			31 688 59 719
23 24	118 146				$\frac{30}{8}$	360				606 6	
25	123 152									631 7	
			1				200			10021	والمرابط بالخاد
		12.10								100211	
					TER					10021	
	27   28					IN	INC	HES		37	1 38
I Length		29	DI	AME	TER			HES	. 36		
Length 10 11 Feet	27   28   342 363   377 400	29  381  419	DI 30 411 457	31   444   488	TER   32     460    506	IN 33 490 539	INC   34   500   550	HES   35   547   602	36   577   634	37 644 708	38   669   734
Length 11 15 11 15 11 15 11 15 11 15 11 15 11 15 11 15 11 15 15	27   28  342 363  377 400  411 436	29  381  419  457	DI 30 411 457 493	31   444   488   532	32   460  506  552	IN  33  490 539 588	INC   34   500   550   600	HES 35 547 602 657	36   577   634   692	37 644 708 772	38   669   734   801
Length 13 13 13 13 13 13 13 13 13 13 13 13 13	27   28  342 363  377 400  411 436  445 473	29   381   419   457   495	DI 30 411 457 493 534	31   444   488   532   576	TER   32     460     506     552     598	33 490 539 588 637	INC   34   500   550   600   650	HES   35   547   602   657   712	36   577   634   692   750	37 644 708 772 836	38   669   734   801   868
Tength 10 11 13 14 15	27   28 342 363 377 400 411 436 445 473 479 509 514 545	29   381   419   457   495   533   571	DI 30 411 457 493 534 575 616	31   444   488   532   576   622   666	TER   32     460    506   552   598   644   690	33 490 539 588 637 686 735	INC   34   500   550   600   650   700   750	HES   35   547   602   657   712   766   821	36   577   634   692   750   807   865	37 644 708 772 836 901 965	38   669   734   801   868   934   1001
Tength 10 11 12 13 14 15 16	27   28 342   363 377   400 411   436 445   473 479   509 514   545 548   582	29   381   419   457   495   533   571   609	DI 30 411 457 493 534 575 616 657	31   444   488   532   576   622   666   710	TER   32   460  506 552 598 644 690 736	IN  33  490 539 588 637 686 735 784	INC   34   500   550   600   650   700   750   800	HES   35   547   602   657   712   766   821   876	36   577   634   692   750   807   865   923	37 644 708 772 836 901 965 1029	38   669   734   801   868   934   1001   1068
Tength 10 11 12 13 14 15 16 17	27   28   342   363 377   400 411   436 445   473 479   509 514   545 548   582 582   618	29   381   419   457   495   533   571   609   647	30 411 457 493 534 575 616 657 698	31   444   488   532   576   622   666   710   755	TER   32     460     506     552     598     644     690     736     782	IN  33  490 539 588 637 686 735 784 833	INC   34   500   550   600   650   700   750   800   850	HES   35   547   602   657   712   766   821   876   931	36   577   634   692   750   807   865   923   980	37 644 708 772 836 901 965 1029 1094	38   669   734   801   868   934   1001   1068   1134
Tength II 10 11 12 13 14 15 16 17 18 19	27   28 342   363 377   400 411   436 445   473 479   509 514   545 548   582 558   616 650   692	29 381 419 457 495 533 571 609 647 685 723	DI 30 411 457 493 534 575 616 657 698 739 780	31   444   488   532   576   622   666   710   755   799   843	TER   32   460  506 552 598 644 690 736	IN  33  490 539 588 637 686 735 784	INC   34   500   550   600   650   700   750   800	HES   35   547   602   657   712   766   821   876	36   577   634   692   750   807   865   923   980   1038	37 644 708 772 836 901 965 1029	38   669   734   801   868   934   1001   1068
Tengt ui 10 112 133 144 156 177 189 20	27   28 342   363 377   400 411   436 445   473 479   509 514   545 548   582 582   618 660   692 684   728	29 381 419 457 495 533 571 609 647 685 723 761	30 411 457 493 534 575 616 657 698 789 780 821	31   444   488   532   576   622   666   710   755   799   843   888	TER    32     460     506     552     598     644     690     736     782     828     874     920	33 490 539 588 637 686 735 784 833 882 931 980	INC   34   500   550   600   650   700   750   800   850   900   950   1000	HES.    35	36   577   634   692   750   807   865   923   980   1038   1096   1152	37 644 708 772 836 901 965 1029 1094 1158	38   669   734   801   868   934   1001   1068   1134   1201
Tength ii 10 112 13 14 15 16 17 18 19 20 21	27   28 342   363 377   400 411   436 445   473 447   509 514   545 548   582 616   654 650   692 668   728 719   764	29   381   419   457   495   533   571   609   647   685   723   761   800	1 30 411 457 493 534 575 616 657 698 739 780 821 863	31   444   488   532   576   622   666   710   755   799   843   888   932	TER   32     460    506    552    598    644    690    736    782    828    874    920    966	33 490 539 588 637 686 735 784 833 882 931 980 1029	INC 34 500 550 600 650 700 800 850 900 950 1000 1050	HES.    35	36   577   634   692   750   807   865   923   980   1038   1096   1152   1210	37 644 708 772 836 901 965 1029 1094 1158 1222	38   669   734   801   868   934   1001   1068   1134   1201   1268
Teogl ui 10 11 12 13 14 15 16 17 18 19 20 21 22	27   28 342   363 377   400 411   436 445   479 509 514   545 548   582 582   618 616   654 650   692 684   728 719   764 719   764 719   764 753   806	29   381   419   457   495   533   571   609   647   685   723   761   800   838	30 411 457 493 534 575 616 657 698 739 780 821 863 904	31   444   488   532   576   622   666   710   755   795   843   888   932   976	TER   32   460 506 552 598 644 690 736 782 828 828 874 920 966 1012	33 490 539 588 637 686 735 784 833 882 931 980 1029 1078	INC   34   500   550   600   650   700   850   900   950   1000   1050   1100	HES.    35   547     602     657     712     766     821     876     931     985     1040     1095     1150     1204	36   577   634   692   750   807   865   923   980   1038   1096   1152   1210   1268	37 644 708 772 836 901 965 1029 1094 1158 1222	38   669   734   801   868   934   1001   1068   1134   1201   1268
Tength ii 10 112 13 14 15 16 17 18 19 20 21	27   28 342   363 377   400 411   436 445   479   509 514   545 582   618 616   654 664   728 719   764 775   806 787   837	29   381   419   457   495   533   571   669   761   800   838   876   914	101 30 411 457 493 534 575 616 657 698 739 780 821 863 904 945 986	31   444   488   532   576   622   666   710   755   799   843   888   932   976   1021   1065	TER   32     460    506    552    598    644    690    736    782    828    874    920    966    1012    1058    1104	33 490 539 588 637 686 735 784 833 882 931 929 1078 1127 1176	INC   34   500   550   600   650   700   850   900   950   1000   1050   1100	HES.    35   547   602   657   712   766   821   876   931   1095   1150   1204   1259   1314	36   577   634   692   750   807   865   923   980   1038   1096   1152   1210   1268   1322   1380	37 644 708 772 836 901 965 1029 1094 1158 1222	38   669   734   801   868   934   1001   1068   1134   1201   1268

To find the amount of lumber any log will make—First, find the length of the log in the first or left-hand column; then, on the top of the page, to the right, find the diameter and under the same will be found the quantity of lumber your log will make; calculated for any length from 10 to 25 feet, and for any diameter from 12 to 38 inches.

Table to Facilitate the Mensuration of Timber,

arm m 24 3   arm m 24 3   arm m 24 3   arm m	rea f a n.ft.
	A OH
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	.7708 .7917 .8125 .8334 .8542 .8750 .8959 .9167 .9375 .9583 .9792

RULE.--Multiply the length by the number in the table

corresponding to any given number.

EXAMPLE.—Given a board 16½ feet in length and 934 inches in breadth.

The number in the table opposite  $9\frac{3}{4}$  inches = .8125  $\times$  16 $\frac{1}{2}$  = 13.4 square feet.

Contents (Board Measure) of I lineal foot of Timber.

_		- '		ببندين	سننج		فالتباكة					
oth Ins				TH	ICI	KNES	S IN	INCE	IES.			
Br'1	2	3	4	5	6	7	8	9	10	11	12	13
18	3.	4.5	6.	7.5	9.			13. 5	15.	16. 5	118.	19.5
17	2.83			7.08			11.32					
16	2.67			6.67			10.67			14.67		17.33
		3.75		6.25			10.00			13.75		
14			4.67			8.17				12.83		
13				5.42		7.58						14.08
12	2.	3.	4.		6.	7.	8.	9.		11.	12.	
11	1.83		3.67			6.42	7.33	8.25		10.08		
10			3.33	4.17	5.	5.83	6.67	7.5	8.33			
9		2.25		3.75		5.25	6.	6.75				
8	1.33			3.33		4.67	5.33					
7	1.17			3.92		4.08						
6	1	1.5		2.50	3.		- 1					
5	.83		1.67	2.08			- 1	į				
4	.67		1.33				1					
6 5 4 3 2	.50											
_2	.33					1 1						

To ascertain the contents of a piece of timber. Find in the table the contents of one foot and multiply by the

length in feet of piece.

EXAMPLE:—What is the contents of a piece of timber  $10 \times 11$ . 20 feet long?  $9.17 \times 20 = 183.4$  feet. B. M.

TABLE TO FACILITATE THE MENSURATION OF

	THE	SOLIDIT	Y OF TIM	IBER.	
1 qr girth in inches.	Area in Feet.	1 qr girth in Inches.	Area in Feet,	1 qr girth in Inches.	Area in Feet.
inches.  6 614 61/2 63/4 7 714 71/2 73/4 8 81/2 83/4 91/2 93/4 10 101/4 101/2 103/4 11	.250 .272 .294 .317 .340 .364 .390 .417 .444 .472 .501 .531 .562 .594 .626 .626 .639 .766 .803 .803 .840 .878	$\begin{array}{c} 1214 \\ 121/2 \\ 123/4 \\ 13 \\ 13 \\ 131/2 \\ 133/4 \\ 14 \\ 141/2 \\ 143/4 \\ 151/2 \\ 153/4 \\ 151/2 \\ 163/4 \\ 161/2 \\ 163/4 \\ 161/2 \\ 163/4 \\ 171/4 \\ 171/4 \\ 171/4 \\ 171/4 \\ 171/4 \\ 171/4 \\ \end{array}$	1.042 1.085 1.129 1.174 1.219 1.265 1.313 1.361 1.410 1.460 1.511 1.562 1.668 1.722 1.777 1.833 1.890 1.948 2.066 2.066	Inches.  19 191/2 200/2 201/2 211/2 221/2 23 231/2 241/2 251/2 26 261/2 27 271/2 28 281/2 29 291/2	2.640 2.777 2.917 3.062 3.209 3.562 3.516 3.673 3.883 4.340 4.168 4.516 4.694 4.876 5.062 5.262 5.444 5.640 5.841
$111/2 \\ 113/4 \\ 12$	$egin{array}{c} .918 \\ .959 \\ 1.000 \\ \end{array}$	$\begin{array}{ c c c }\hline 173/4 \\ 18 \\ 181/2 \\ \end{array}$	$2.187 \\ 2.250 \\ 2.376$	30	6.250

RULE:-Multiply the area corresponding to the quarter girth in inches by the length in feet.

Example:—Given a piece of timber 20 feet long and 12 inches square.

The number opposite 12 inches =  $1.000 \times 20 = 20$  Cubic feet.

The following table of scantling measure gives the number of feet in a scantling from 1 foot to 13 feet and from  $2\times2$  to  $11\times12$ .

EXAMPLE:—How many feet in a 5×6 scantling 10 feet long? First find 10 feet under the column marked "Length in Feet" and opposite the number under the column marked 5×6 will be found 25 feet, the number of feet, the scantling contains,

If your scantling is longer than that given in the table

take two lengths and add them together.

EXAMPLE:—How many feet in a 3×4 scantling 21 feet long? Opposite 10 feet and under 3×4 is 10 feet. Opposite 11 feet and under  $3\times4$  is 11 feet. Then 10+11=21 feet, the number of feet the scantling contains.

## SCANTLING MEASURE.

Length in Feet.			ING	CHES.		
in Feet.	$2\times2$	$+2\times3$	$+2\times4$	2×5	$+2\times6$	$ 2\times7 $
1 2 3 4 5 6 7 8 9 10 11 12 13	ft. in.       0       4       0       8       1       0       1       4       2       3       4       3       4       6       6       7       8       8       8       8       8       8       8       8       8       8       8       8       8       8 <td>  ft. in.   0</td> <td>0 8 4 4 0 0 8 4 4 6 6 6 8 4 6 7 4 8 8 8 8 8</td> <td><math display="block"> \begin{bmatrix} 0 &amp; 10 \\ 1 &amp; 8 \\ 2 &amp; 6 \\ 3 &amp; 4 \\ 4 &amp; 2 \\ 5 &amp; 0 \\ 5 &amp; 10 \\ 6 &amp; 8 \\ 7 &amp; 6 \\ 8 &amp; 4 \\ 9 &amp; 2 \\ 10 &amp; 0 \\ 10 &amp; 10 \\ \end{bmatrix} </math></td> <td><math display="block"> \begin{bmatrix} 2 &amp; 0 \\ 3 &amp; 0 \\ 4 &amp; 0 \\ 5 &amp; 0 \\ 6 &amp; 0 \\ 7 &amp; 0 \\ 8 &amp; 0 \\ 9 &amp; 0 \\ 10 &amp; 0 \\ 11 &amp; 0 \\ 12 &amp; 0 \\ 13 &amp; 0 \\ \end{bmatrix} </math></td> <td>  ft. in. 1 2 2 4 3 6 4 8 5 10 7 0 8 2 9 4 10 6 11 8 12 10 14 0 15 2</td>	ft. in.   0	0 8 4 4 0 0 8 4 4 6 6 6 8 4 6 7 4 8 8 8 8 8	$ \begin{bmatrix} 0 & 10 \\ 1 & 8 \\ 2 & 6 \\ 3 & 4 \\ 4 & 2 \\ 5 & 0 \\ 5 & 10 \\ 6 & 8 \\ 7 & 6 \\ 8 & 4 \\ 9 & 2 \\ 10 & 0 \\ 10 & 10 \\ \end{bmatrix} $	$ \begin{bmatrix} 2 & 0 \\ 3 & 0 \\ 4 & 0 \\ 5 & 0 \\ 6 & 0 \\ 7 & 0 \\ 8 & 0 \\ 9 & 0 \\ 10 & 0 \\ 11 & 0 \\ 12 & 0 \\ 13 & 0 \\ \end{bmatrix} $	ft. in. 1 2 2 4 3 6 4 8 5 10 7 0 8 2 9 4 10 6 11 8 12 10 14 0 15 2
	2½×3	$ 21/2 \times 4 $	21/2×5	2½×6	21/2×7	21/2×8
1 2 3 4 5 6 7 8 9 10 11 12 13	0 8 1 3 1 11 2 6 3 2 3 9 4 5 5 0 5 8 6 3 6 11 7 6 8 2	$ \begin{array}{c cccc} 0 & 10 & 10 \\ 1 & 8 & 2 & 6 \\ 3 & 4 & 2 & 5 \\ 5 & 0 & 5 & 10 \\ 6 & 8 & 7 & 6 \\ 8 & 4 & 9 & 2 \\ 10 & 0 & 10 & 10 \\ \end{array} $	1 1 1 2 1 1 3 1 1 4 2 3 5 3 7 4 8 4 9 5 11 6 12 6 13 7	1 3 2 6 3 9 5 0 3 7 6 8 9 10 0 11 3 12 6 13 9 15 0 16 3	1 6 2 11 4 5 5 10 7 4 8 9 10 3 11 8 13 2 14 7 16 1 17 6 19 0	1 8 3 4 5 0 6 8 8 4 10 0 11 8 13 4 15 0 16 8 18 4 20 0 21 8
	3×3	3×4	3×5	3×6	3×7	3×8
1 2 3 4 5 6 7 8 9 10 11 12 13	0 9 1 6 3 0 3 9 4 6 5 6 6 6 7 8 9 9	$ \begin{bmatrix} 1 & 0 \\ 2 & 0 \\ 3 & 0 \\ 4 & 0 \\ 5 & 0 \\ 6 & 0 \\ 7 & 0 \\ 8 & 0 \\ 9 & 0 \\ 10 & 0 \\ 11 & 0 \\ 12 & 0 \\ 13 & 0 \\ \end{bmatrix} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 6 3 0 4 6 6 0 7 6 9 0 10 6 12 0 13 6 15 0 16 6 19 6	1 9 3 6 5 3 7 0 8 9 10 6 12 3 14 0 15 9 17 6 19 3 21 0 22 9	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

## SCANTLING MEASURE.

Length in Feet.			I	N C	нЕ	s.		-		
in Feet.	$4\times4$	4×5		$\times 6$	$4 \times$		4>	<8	4>	<del>(</del> 9
1 2 3 4 5 6 7 8 9 10 11 11 12 13	ft. in 1	1 8 8 6 8 8 8 10 11 8 15 15 15 16 18 18 120 21 8	3   2 4   4 0   6 8   8 1   10 0   12 8   14 1   16 0   18 8   20 1   22	in. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ft. 2 4 7 9 11 14 16 18 21 23 25 28 30	in. 4 8 0 4 8 0 4 8 0 4 8 0 4 8 0	ft. 2 5 8 10 13 16 18 21 24 26 29 32 34	in. 8 4 0 8 4 0 8 4 0 8 4 0 8	ft. 3 6 9 12 15 18 21 24 27 30 33 36 39	in. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	5×5	5×6		$\times 7$	$5 \times$		5 >			<10
1 3 4 5 6 7 8 9 10 11 12 13	2 4 6 8 10 8 10 11 11 11 11 11 11 11 11 11 11 11 11	2 5 3 7 4 10 5 12 1 15 7 17 7 17 8 20 9 22 9 22 9 25 27 9 30	6   2 0   5 6   8 0   11 6   14 0   17 6   20 0   23 6   26 0   29 6   32 0   35 6   37		10 13 16 20 23 26 30 33 36 40 43	4 8 0 4 8 0 4 8 0 4 8 0 4	3 7 11 15 18 22 26 30 33 37 41 45 48	9 6 3 0 9 6 3 0 9 6 3 0 9	8 12 16 20 25 29 33 37 41 45 50	2 4 6 8 10 0 2 4 6 8 10 0 2
	$6 \times 6$	6×7		<8 ∣	$6 \times$		$6 \times$		6>	(11
1 2 3 4 5 6 7 8 9 10 11 12 13	3 0 6 0 9 0 12 0 15 0 18 0 21 0 24 0 30 0 33 0 36 0 39 0	3   6   7   10   6   14   6   17   6   17   6   17   6   17   6   17   17	8 12 16 20 24 32 36 36 36 40 44 48	0 0 0 0 0 0 0 0 0 0 0	13 18 22 27 31 36 40 45 49 54 58	6 0 6 0 6 0 6 0 6 0 6	5 10 15 20 25 30 35 40 45 50 60 65	0 0 0 0 0 0 0 0 0 0	5 11 16 22 27 33 38 44 49 55 60 66 71	6 0 6 0 6 0 6 0 6 0 6 0 6 0 6

## HANDY MECHANICAL,

## SCANTLING MEASURE.

Length in Feet.			ING	внЕ	s.				
in Feet.	7×7	7×8	7×9	7×	10	$7 \times$	(11	7×	(12
1 2 3 4 5 6 7 8 9 10 11 12 13	ft. in 4 1 8 2 12 3 16 4 20 5 24 6 28 7 32 8 36 9 40 10 44 11 49 0	ft. in. 4 8 9 4 114 0 118 8 228 0 32 8 37 4 42 0 46 8 51 4 556 0	ft. in 5 3 10 6 15 9 21 0 26 3 31 6 36 9 42 0 47 3 52 6 63 0 68 3	11 17 23 29 35 40 46 52 58 64 70	in. 10 8 6 4 2 0 10 8 6 4 .2	ft. 6 12 19 25 32 38 44 51 57 64 70 77	in. 5 10 3 8 1 6 11 4 9 2 7 0	ft. 7 14 21 28 35 42 49 56 63 70 77 84 91	in. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
10	$\frac{ 53 }{ 8\times8 }$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$8\times10$	$\frac{18}{18\times}$		8×	19	9>	
1 2 3 4 5 6 7 8 9 10 11 12 13	5	6	6	14 22 29 36 44 51 58 66 73 80 88 95	4 8 0 4 8 0 4 8 0 4 8 0 4	8 16 24 32 40 48 56 64 72 80 88 96 104	0 0 0 0 0 0 0 0 0 0 0	6 13 20 27 33 40 47 54 60 67 74 81 87	9630963096309
	$+9\times10$	9×11	$9\times12$	10>		10>		10×	
1 3 4 5 6 7 8 9 10 11 12	7   6   15   0   0   0   0   0   0   0   0   0	16 6 24 9 33 0 41 3 49 6 57 9 66 0 74 3 82 6 90 9	27 36 45 54 63 72 81	0 8 0 16 0 25 0 33 0 41 0 50 0 58 0 66 0 75 0 83 0 91 0 100	4 8 0 4 8 0 4 8 0 4 8 0 4 8 0 4	9 18 27 36 45 55 64 73 82 91 100 110	2 4 6 8 10 0 2 4 6 8 10 0 2 4 6 8	10 20 30 40 50 60 70 80 90 100 110 120 130	

BOARD MEASURE, (I inch thick).

Length in Feet.		W	IDTH I	N INCH	ES.		
in Feet.	4	5	6	1 7	8		9 .
1 2 3 4 5 6 7 8 9 10 11 12 13	ft. in 0 4 0 8 1 0 1 4 1 8 2 0 2 4 4 2 8 8 3 0 4 3 8 4 4 0 4	0 5 0 10 1 3 1 8 2 1 2 6 2 11 3 4 3 9 4 27 5 0 5		ft. in.   0   7   1   2   1   2   1   2   1   2   1   3   4   4   8   5   5   1   5   6   7   7   7   7   7   7   7   7   7	22344566788	n.   ft.   8   4   1   2   8   3   4   3   4   5   6   6   8   4   8   9   9   9	in. 9 6 3 0 9 6 3 0 9
	10	11	12	13	14		.5
1 2 3 4 5 6 7 8 9 10 11 12 13	0 10 1 8 2 6 3 4 4 2 5 0 5 10 6 8 7 6 8 4 9 2 10 0 10 10		1 3 4 5 6 7 8 9 10 11 12 13	1 2 2 3 3 4 4 5 5 6 6 6 7 7 7 8 8 9 9 9 10 10 11 11 11 13 11 11 11 11 11 11 11 11 11	6 7 8 9 10 11 14 15	2   1 4   2 6   3 8   5 10   6 0   7 2   8 4   10 6   11 8   12 10   13 0   15 2   16	3 6 9 0 3 6 9 0 3 6 9 0 3
	16	17	18	19	20	2	
1 2 3 4 5 6 7 8 9 10 11 12 13	1 4 8 8 9 4 4 10 8 112 13 14 16 17 4 4	9 11 11 4 12 9 14 2 15 7 0 17 0	1 6 3 0 4 6 6 0 7 6 9 0 10 6 12 0 13 6 15 0 16 6 18 0 19 6	11 12 14 15 17 19	6 10	8 1 4 3 5 7 4 8 0 10 8 12 4 14 0 15 8 17 4 19 0 21 8 22	9 6 3 0 9 6 3 0 9 6 3 0 9

NOTE:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

## BOARD MEASURE, (2 inch thick).

Length		TI.	IDI		INC	CHE	S.		
n Feet.	6	1 7		8	9		10	1	1
8 9 10 11 12 13 14 15 16 17 18 19 20	8 9 10 11 12 13 14 15 16 17 18 19 20	$ \begin{vmatrix} 9 & 4 \\ 10 & 6 \\ 11 & 8 \\ 12 & 10 \\ 14 & 0 \\ 15 & 2 \\ 16 & 4 \\ 17 & 6 \\ 18 & 8 \\ 19 & 10 \\ 21 & 0 \\ 22 & 2 \\ 23 & 4 \end{vmatrix} $	10 12 13 14 16 17 18 20 21 22 24 25 26	8 0 4 8 0 4 8 0 4 8 0 4 8	ft. 12 13 15 16 18 19 21 22 24 25 27 28 30	in. 0 6 0 6 0 6 0 6 0 6 0 6	13 15 16 18 20 21 23 25 26 28 30 31 33	14 14 0 16 8 18 14 20 0 22 8 23 14 25 0 27 8 29 14 31 0 33 8 34 4 36	in. 8 6 4 2 0 10 8 6 4 2 0 10 8
						-	16		7
8 9 10 11 12 13 14 15 16 17 18 19 20	18 20 22 24 26 28 30 32 34 36 38 40	19 6 21 8 23 10 26 0 28 2 30 4 32 6 34 8 36 10 39 0 41 2 43 4	21 23 25 25 28 30 32 35 35 37 39 42 44	0. 4 8 0 4 8 0 4 8 0 4 8	22 25 27 30 32 35 37 40 42 45 47 50	6 0 6 0 6 0 6 0 6	26 29 32 34 37 40 42 45 48 50 53	25 328 4 31 34 36 4 39 42 8 45 4 48 5 53 4 56	8 6 4 2 0 10 8 6 4 2 0 10 8 8
	18								23
9 10 11 12 13 14 15 16 17 18	30 33 36 39 42 45 48 51 54	28 6 31 8 34 10 38 41 2 44 47 6 50 8 57 60 5	30 33 33 36 40 43 44 46 50 50 60 60 60 60 60 60 60 60 60 60 60 60 60	0 4 8 0 4 8 0 4 8 0 4	31 35 38 42 45 49 52 56 63 66	6 0 6 0 6 0 6 0 6 0 6 0 6	36 40 44 47 51 55 58 62 66 69	0 34 8 38 4 42 0 46 8 49 4 53 0 57 8 61 4 65 0 69 8 72	8 6 4 2 0 10 8 6 4 2 0 10 8 8 6 8
	8 9 10 11 12 13 14 15 16 17 18 19 20 8 9 10 11 12 13 14 15 16 17 18 19 20 20 8 9 10 11 12 13 14 15 16 17 18 19 19 10 11 12 13 14 15 16 17 18 18 19 10 11 12 13 14 15 16 17 18 18 19 10 11 12 13 14 15 16 17 18 18 19 10 11 12 13 14 15 16 17 18 18 19 10 11 12 13 14 15 16 17 18 18 19 10 11 12 13 14 15 16 17 18 18 19 10 10 11 12 13 14 15 16 17 18 18 19 10 10 10 10 10 10 10 10 10 10 10 10 10	S   S   S   S   S   S   S   S   S   S	Treet.   6   7   7   8   8   9   9   10   6   6   10   11   8   11   12   10   12   12   14   15   15   15   17   6   16   16   18   8   17   17   19   19   19   22   22   20   20   23   4   11   22   24   26   6   11   22   24   26   6   11   22   24   26   6   13   24   25   46   17   34   36   39   41   22   24   26   6   21   3   26   28   34   36   36   36   37   37   38   36   39   38   36   39   38   36   39   38   38   38   38   38   38   38	Treet.	Treet.	Teet.	Treet.	Teet.	Treet.

Note:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

CUBIC CONTENTS of SQUARE TIMBER.

Length in Feet.			INC	HES.		
in Feet.	$6\times6$	6×7	6×8	6×9	6×10	6×11
10 11 12 13 14 15 16 17 18 19 20 21 22	ft. in 2 9 9 1 3 6 8 9 9 4 9 0 4 4 9 1 5 5 6	ft. in. 2 11 3 3 6 3 10 4 1 4 5 4 8 5 0 5 7 5 10 6 2 5	ft. in. 3 4 8 4 0 4 4 4 8 5 0 5 4 6 6 8 7 0 7 4	ft. in. 3 9 4 2 4 6 4 11 5 8 8 6 0 6 5 6 9 7 2 2 7 11 8 3	ft. in.   4	5 6 0 6 5 11 7 4 7 10 8 3 8 9 9 2 9 8 10 1
	7×7	7×8.	7×9	7×10	7×11	7×12
10 11 12 13 14 15 16 17 18 19 20 21	3	$ \begin{vmatrix} 6 & 5 \\ \hline 7 \times 8 \\ \hline 3 & 11 \\ 4 & 8 \\ 5 & 1 \\ 55 & 8 \\ 66 & 37 \\ 77 & 0 \\ 77 & 9 \\ 28 & 7 \end{vmatrix} $	4	1 4 10 5 4 5 10 6 4 6 10 7 4 7 9 8 3 8 9 9 9 10 3 10 8	5 4 5 11 6 5 6 11 7 6 8 0 8 7 9 1 9 8 10 2 10 8 11 3 11 9	5 10 6 5 7 0 7 7 8 2 8 9 9 4 9 11 10 6 11 1 11 8 12 3 12 10
	8×8	8×9	8×10	8×11	8×12	8×13
10 11 12 13 14 15 16 17 18 19 20 21 22	4 5 4 11 5 4 5 9 6 3 6 8 7 1 7 7 8 5 8 11 9 4 9 9	5 0 5 6 6 0 6 6 7 0 7 6 8 0 8 6 9 0 10 0 10 6 11 0	5 7 6 1 6 8 7 3 7 9 8 4 8 11 9 5 10 0 10 7 11 1 11 8 12 3	$ \begin{vmatrix} 6 & 1 \\ 6 & 9 \\ 7 & 4 \\ 7 & 11 \\ 8 & 7 \\ 9 & 2 \\ 9 & 9 \\ 10 & 5 \\ 11 & 0 \\ 11 & 7 \\ 12 & 3 \\ 12 & 10 \\ 13 & 5 \\ \end{vmatrix} $	6 8 7 4 8 0 8 8 9 4 10 0 10 8 11 4 12 0 12 8 13 4 14 0 14 8	$ \begin{vmatrix} 7 & 3 \\ 7 & 11 \\ 8 & 8 \\ 9 & 5 \\ 10 & 1 \\ 10 & 10 \\ 11 & 7 \\ 12 & 3 \\ 13 & 0 \\ 13 & 9 \\ 14 & 5 \\ 15 & 2 \\ 15 & 11 \\ \end{vmatrix} $

Note:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

CUBIC CONTENTS of ROUND TIMBER.

Longth			DIAI	MET	ER I	N INC	HES			
Length in Feet.	10	1		12		13	14	1 1	1	5
13 14 15 16 17 18 19 20 21 22 23 24 25	ft. in 7 11 7 8 8 2 9 8 9 10 10 11 11 6 112 12 13 13 8	1 ft. 8 9 9 10 10 11 12 13 13 13 14 7 15 15		ft. 10 11 11 12 13 14 14 15	in. ft 3 12 0 12 9 13 7 14 4 11 2 11 11 11 9 12 6 11 3 12 10 12 8 12	in. 22 0 22 11 3 10 4 9 5 8 6 7 7 6 8	ft.   13   15   16   17   18   19   120   121   122   123   124   125	in. 11	ft. 15 17 18 19 20 22 23 24 25 27 28 29 30	in. 11 2 5 8 10 1 4 7 7 9 0 3 6 8
-	16	1	7	18	Ť	19	1 :	20		21
13 14 15 16 17 18 19 20 21 22 23 24 25	18	7 22 1 23 1 25 2 26 2 28 6 30 1 31 1 33 2 36 5 37 1 39	6 1 8 3 10 5 0 6 1 8 3 10 5 5	23 24 26 28 30 31 33 35 37 38 40 42 44	0 2 9 2 6 2 3 3 3 1 3 3 1 0 3 7 3 3 2 4 4 8 4 4 5 4 4 2 4	5791357913579	30 32 34 37 39 41 45 445 48 45 48 45 48	4 7 9 11 1 3 6 8 10 0 2 5 7	31 33 36 38 40 43 45 48 50 52 55 60	3 8 1 6 11 4 9 2 6 11 4 9
	22		23	2		25		6		27
18 14 15 16 17 18 19 20 21 22 23 24 25	37 39 42 44 1 47 50 52 1 55 58 60 63	4   37 0   40 7   43 8   46 1   49 6   51 6   60 1   63 6   69 7   72	6 5 4 2 1 11 10 9 7 6 5 3 2	40 44 47 50 53 56 59 62 66 69 72 75	5 5 7 6 9 6 10 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7 9 1 4 8 6 1 10 8 1 1 5 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 62 6 66 0 70 2 73 7 77 0 81 5 84 0 88	11 8 4 0 8 5 1 9 6 3	51 55 59 63 67 75 79 83 87 91 95	9888777766665

Note:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

CUBIC CONTENTS OF ROUND TIMBER WHEN SQUARED.

Length in Feet.	1		DIA				INCH	IES	5.		
m Feet.	10	1	1	1	2		13		14	1	.5
13 14 15 16 17 18 19 20 21 22 23 24	ft. in 4 4 4 4 5 5 5 5 5 1 6 6 6 1		in. 11 4 8 1 5 10 2	ft. 5 6 6 7 7 8 8 9 9 9 10	in. 10 4 9 2 8 1 7 0 5 11 4	ft. 6 7 7 8 9 9 10 10 11 11 12 12	in. 10 5 11 5 0 6 0 7 1 7 2 8	ft. 8 9 10 11 11 12 12 13	in. 0 7 2 10 5 0 8 3 10 6	ft. 9 10 11 12 13 14 14 15 16	in. 2 10 7 3 11 8 4 1 9 6 2 11 7
$\frac{24}{25}$	7 1	$\begin{array}{c c} 6 & 9 \\ 0 & 9 \end{array}$	1 5	10 11	10	12 13	8 2	14 15	8	16 17	11 7
	16	[ ]	17	1	.8	1	19		20		21
13 14 15 16 17 18 19 20 21 22 23 24 25	10 11 12 12 13 14 15 16 16 17 18 19 20	5   11 2   12 0   13 9   14 7   15 5   16 2   17 0   18 9   19 7   19 5   20 2   21 0   22	9 8 7 5 4 3 2 1 0 10 9 8 7	13 14 15 16 17 18 19 20 21 22 23 24 25		2 15 2 16 2 18 3 19 3 20 3 21 3 22 3 23 3 24 2 27	8 10 11 1 2 4 5 7 8 10 11 1	16 17 18 20 21 22 23 25 26 27 28 30 31	3 6 9 0 3 6 9 0 3 6 9 0 3 6 9	17 19 20 22 23 24 26 27 28 30 31 53 34	11 4 8 1 5 10 2 7 11 4 8 1 5
	22		23		24	1	25		26		27
13 14 15 16 17 18 19 20 21 22 23 24 25	19	8   21 2   23 8   24 2   26 9   28 3   29 9   31 3   33 9   34 3   36 9   38 4   39 10   41	6 2 10 5 1 9 5 1 9 4 0 8 4	23 25 27 28 30 32 34 36 37 39 41 43 45		2 27 0 29 0 31 7 33 5 35 2 37 0 39 0 41 7 43 6 44 2 46	5 4 4 3 2 2 1 1 0 0 0 11 11 10	27 29 31 33 35 38 40 42 44 46 48 50 52	6 7 8 10 11 0 2 3 4 6 7 8	29 31 34 36 38 41 43 45 47 50 52 54 56	7 11 25 9 0 3 7 10 1 5 8 11

NOTE:—The rule for this table is worked in the same manner as the rule for scantling measure, on page 151.

STANDARD CONTENTS OF LOGS.

Length		DI		R IN INC	HES.	
in Feet.	10	11	12	13	14	15
10	.21	.26	.31	.36	.42	.48
11	.23	.28	.34	.40	.46	.53
$\hat{1}\hat{2}$	.26	.31	.37	.43	.50	.58
13	.28	.34	.40	.47	.54	.62
14	.30	.36	.43	.50	.58	.67
15	.32	.39	.46	.54	.63	.72
16	.34	.41	.49	.58	.67	.77
17	.36	.44	.52	.61	.71	.81
18	.38	.46	.55	.64	.75	.86
19 20	.40	.49	.58	.68	.79 .84	.91
$\frac{20}{21}$	.45	.54	.64	.76	.88	.96 1.01
$\frac{21}{22}$	.47	.57	.67	79	.92	1.05
44	16	17	1 18	19	1 20	21
10	.55	.62	.69	.77	.85	.94
11	.60	.68	.76	.85	.94	1.03
$\mathbf{\tilde{1}}$	.65	74	.83	.92	1.02	1.13
13	.71	.80	.90	1.00	1.11	1.22
14	.76	.86	.97	1.08	1.19	1.32
15	.82	.92	1.04	1.15	1.28	1.41
16	.87	.99	1.10	1.23	1.36	1.50
17	.93	1.05	1.17	1.31	1.45	1.60
18	.98	1.11	1.24	1.38	1.53	1.69
19	1.04	1.17	1.31	1.46	1.62	1.79
20	1.09	1.23	1.38	1.54	1.70	1.88
$\frac{21}{22}$	1.15 1.20	1.29 1.35	$1.45 \\ 1.52$	$1.62 \\ 1.69$	1.79 1.88	1.97
24	1.20	1.55	1.52		1.88	2.07
				25		27
10 11	1.03	1.13	1.23 1.35	1.33	1.44	1.55
11	1.13	1.24 1.35	1.33	1.46 1.60	1.58 1.73	1.71 1.86
$\frac{12}{13}$	1.34	1.47	1.60	1.73	1.86	2.02
14	1.44	1.58	1.72	1.86	2.02	2.17
15	1.55	1.69	1.84	$\frac{1.00}{2.00}$	2.16	2.33
16	1.65	1.80	1.96	$\frac{2.00}{2.13}$	2.30	2.49
17	1.75	1.92	$\frac{100}{209}$	2.26	2.45	2.64
18	1.86	2.03	2.21	2.40	2.59	2.80
19	1.96	2.14	2.33	2.53	2.74	2.95
20	2.06	2.25	2.46	2.66	2.88	3.11
21	2.17	2.37	2.58	2.80	3.02	3.26
22	2.27	2.48	2.70	2.93	3.17	3.42

Note:—A log 13 feet long and 19 inches in diameter is the standard. The table shows the comparison of logs with this standard.

Table showing the Temperature of Steam at different pressures, from 1 lb., to 240 lbs., per square inch, and the quantity of Steam produced from a cubic inch of water, according to pressure.

	- 1	nen or w	ater,	accor	aing to p	ress	ure.	
Pressure per Sq. In.	Corresp'd'g Temp. of S. to pressure.	C. Ins. of S. from a C. Ins. o	Pressure per Sq. In.	Corresp'd'g Temp. of S. to pressure.	C. Ins. of S. from a C.In of water ac- cord'g to P.	Pressure per Sq. In.	Corresp'd'g Temp. of S. to pressure.	C. Ins. of S. 998 from a C.In. of S. of S. cord's to P. cord's to P.
12 2 3 3 4 4 5 6 6 7 7 8 8 9 9 10 11 12 13 13 14 14 15 6 16 17 7 18 20 22 23 24 25 26 27 33 1 32 2 33 34 35 5 36	102.9 1126.1 141.0 152.3 161.4 169.2 175.9 182.0 187.4 197.0 201.3 205.3 209.1 212.8 225.6 228.5 225.6 228.5 231.2 231.2 243.3 245.3 247.6 255.6 255.6 257.3 259.1	2068   20668   10874   7437   5685   4617   3897   3376   2983   2674   2221   2050   1904   1778   1669   1411   1343   1481   1225   1174   11225   1084   10044   1007   973   941   911   883   857   883   810   788   767	39 40 41 42 48 44 45 46 47 50 51 52 53 56 66 66 66 66 67 71 72 73	26-3 269.1 270.6 275.0 275.0 276.4 277.8 279.2 280.5 281.9 283.2 284.4 285.7 286.9 288.2 291.7 292.9 293.2 291.7 292.9 293.3 301.3 302.4 305.4 306.4 306.4 306.4 306.4 306.4 306.4	2475 85 679 666 649 635 622 610 589 586 575 564 554 554 554 555 64 477 470 463 449 443 447 4419 448 408 8388 398	777 7880 81 822 833 844 855 866 877 888 899 91 920 933 944 110 1200 1100 1100 1200 1200 2010	315.8 316.7 317.6 318.4 319.3 320.1 321.0 321.8 322.6 323.5 324.3 325.1 325.9 326.7 327.5 328.2 329.8 330.5 339.2 339.2 345.8 357.9 368.7 378.4	\$62   358   354   354   354   346   342   339   325   325   322   316   310   307   301   298   225   271   231   218   205   218   218   219   218   219   218   219   218   219   218   219   218   219   219
36 37 38	262.6 264.3 265.9	748 729 712	74 75 76	310.3 311.2 312.2	388 383 379	220 230 240	395.5 399.4 403.1	145 140 134

Note:—Add the pressure of the atmosphere 15 lbs to the pressure on the Steam gauge, to correspond with the table.

Table showing the average Pressure of the Steam upon the Piston throughout the Stroke when cut-off in the Cylinder, from 1-3 to 11-12 commencing with 10 lbs., and advancing in 5 lbs., up to

Pressure in Ibs., at the Commencement of the Stroke.    10   15   20   25   30   35   40   45   50   55   60   65   70   75     Average Pressure in Ibs. upon the Piston.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
Average Pressure in fbs. upon the Piston.
1/3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Table showing the average Pressure of the Steam upon the Piston throughout the Stroke when cut-off in the Cylinder, from 1-3 to 11-12 commencing with 10 lbs., and advancing in 5 lbs., up to 135 lbs., Pressure, (Continued).

Cut- the ler.	Pressure in lbs., at the Commencement of the Stroke.												
am ind	80   85   90   95   100   105   110   115   120   125   130   135												
Steam off in Cylin	Average Pressure in fbs. upon the Piston.												
1/3	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
2/3 1/4	1 473 503 533 563 593 623 654 684 714 744 774 804												
1/2 3/4	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
1-5	413 444 47   494 524  543  574  60   624  654  673  704												
2-5 3-5	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
4-5	1 781 83   88   923   973   1023   1071   1121   1171   1221   1271   132												
1-6 5-6	$\begin{array}{c} 37\frac{1}{4}39\frac{1}{2}44\frac{1}{4}44\frac{1}{4}46\frac{1}{3}48\frac{3}{4} & 51\frac{1}{4} & 53\frac{1}{2} & 55\frac{3}{4} & 58 \\ 78\frac{3}{4}88\frac{3}{4}88\frac{3}{4}98\frac{1}{2}98\frac{1}{2}103\frac{1}{2}108\frac{1}{4}113\frac{1}{4}118\frac{1}{4}123\frac{1}{4}128 & 133 \\ \end{array}$												
1-7	331 351 371 40 42 44 46 481 501 521 541 561												
2-7 3-7													
4-7	711 65 3 80 84 3 89 93 3 98 102 3 106 3 111 3 115 3 120 3												
5-7 6-7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$												
1/2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$												
5/0	$ \begin{bmatrix} 59\frac{1}{2} & 63 \\ 70\frac{1}{2} & 74\frac{1}{4} \\ 78^{2} & 81\frac{3}{4} \\ 78\frac{1}{2} & 85\frac{1}{4} \\ 89\frac{1}{4} & 96\frac{1}{2} \\ 101 \\ 105\frac{1}{2} & 110\frac{1}{4} \\ 114\frac{1}{4} & 119\frac{1}{2} \\ 124 \\ \end{bmatrix} $												
5/8 7/8 1-9													
1-9 2-9	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												
4-9	641   681   721   761   801   841   881   921   961   1011   1041   1081												
5-9 7-9													
8-9	$ 79\frac{1}{4} 84\frac{1}{4} 89\frac{1}{4} 94\frac{1}{4} 99\frac{1}{4} 104\frac{1}{4} 114\frac{1}{4} 119\frac{1}{4} 124 129 134$												
1-11 2-11	24½   26½   27½   29½   30½   32½   35½   37   38½   40   41½   90½   41½   44½   46½   40   51½   54   56½   59   61½   68½   66½												
3-11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$												
4-11 5-11	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												
6-11	70												
7-11 8-11	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												
9-11													
10-11 1-12	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
7-12	$  67\frac{1}{2}  72  76\frac{1}{2}  80\frac{1}{2}  84\frac{1}{2}  89  93\frac{1}{2}  97\frac{1}{2}  110\frac{1}{2}  105\frac{1}{2}  110  114\frac{1}{2} $												
11-12	$ 79\frac{1}{2} 84\frac{1}{2} 89\frac{1}{2} 94\frac{1}{2} 99\frac{1}{2} 104\frac{1}{2} 109\frac{1}{2} 114\frac{1}{2} 119\frac{1}{2} 124\frac{1}{2} 129\frac{1}{2} 134\frac{1}{4} 119\frac{1}{2} 11$												

#### CONDENSING ENGINE.

EXAMPLE:— 15 pounds pressure on the piston above atmosphere, cut-off at one-fourth the piston's traverse, will be thus; 15 pounds steam and 15 pounds that atmosphere pressure equals 30; then look for 30 pounds at the head of the table, and down the first column for 1/4; trace that 1/4 under 30 and you will find the average to be 173/4 pounds throughout the stroke.

#### NON-CONDENSING ENGINE.

EXAMPLE:—45 pounds steam above atmosphere upon the piston, cut-off at one quarter the length of stroke. Thus 45 pounds of steam cut-off at one-fourth the stroke

with 15 pounds added make 60 pounds.

Look for 60 on the top line and 14 on the side, trace that 14 to the figures under 60 and the average will be found to be 3534 pounds. Take 16 pounds from 3534 pounds, for friction (1 1b)., and atmosphere pressure, and there remains 1934 pounds, the available pressure on the piston.

#### STEAM.

A cubic inch of water evaporated under an ordinary atmospheric pressure is converted into 1 cubic *foot* of steam (approximately).

The specific gravity of steam (at atmospheric pressure) is .411 that of air at 34° Fahrenheit, and .0006 that of water

at same temperature.

27.222 cubic feet of steam weigh 1 pound; 13.817 cubic

feet of air weigh 1 pound.

Locomotives average a consumption of 3000 gallons of

water per 100 miles run.

The best designed boilers, well set with good draft and skillful firing, will evaporate from 7 to 10 pounds of water per pound of first-class coal. The average result is from 25 to 60 per cent. below this.

In calculating horse-power of Tubular or Flue boilers, consider 15 square feet of heating surface equivalent to

one nominal horse-power.

Steam engines in economy, vary from 20 to 60 pounds of feed water, and from 2 to 7 pounds of coal per hour per

indicated horse-power.

Condensing engines require from 20 to 30 gallons of water to condense the steam represented by every gallon of water evaporated—approximately for most engines, we say, from 1 to 1½ gallons per minute per I. H. P. Jet condensers do not require quite as much water for condensing as surface condensers.

Surface condensers should have about 2 square feet of tube (cooling) surface per horse-power of steam engine.

# RATIO OF VACUUM TO TEMPERATURE (Fahrenheit) OF FEED WATER.

0 1	Inches.	Vacuum	212°	171/2	Inches,	Vacuum,	112°
11	66	66	190°	281/2	6.	66	920
18	6.6	6.6	170°	29 ~	6.6	66	72°
221/	6 "	66	150°	291/2	6.6	6.6	52°
221/ *25	4.6	66	135°	/2			-

\*Usually considered the standard point of efficiency—condenser and air pump being well proportioned.

#### A TABLE OF MULTIPLIERS TO FIND THE LAP AND LEAD, WHEN THE STEAM IS TO BE CUT OFF AT 14 TO 76ths OF STROKE.

		OLL	A 1 %	4 10	70 cris	OI D	TITOI	T.L.	
H	alf-	Five-e	ig'hs	Thi	ee-	Sev	en-		
Str	oke.	0	L .	fourth	18 01	eigni	ns or		
201	OILO.	the st	roke.	the St	roke.	thes	troke		
1	2	1	2	1	2	1 2			
lap.	lead.	lap.	lead.	lap.	lead.	lap.	lead	read- being	
2.41	.000	1.58	.000	1.000	.000	1.540	.000	13.3 t	.00000
2.16	.145	1.41	.124	.893	.105	.477	.089	8223	.00208
2.06	.198	1.35	.170	.851	.146	.450	.123	ee of the Piston from one oke when steam is rective return stroke being the stroke multiplied.	.00416
1.94	.268	1.27	.231	.795	.200	.413	.170	J. 5.2	.00833
1.84	.318	1.21	.276	.754	.240	.385	.204	2223	.01250
1.97	.358	1.16	.312	.723	.271	1.363	.232	2 8 8 25	.01666
1.71	.391	1.12	.342	.691	.299	.344	.257	Piston steam rn str	.02083
1.65	.420	1.08	.368	.668	.322	.327	.277	28.30	.02500
1.60	.444	1.05	' .391	.644	.343	.313	.296	the return	.02916
1.56	.467	1.02	.412	.623	.362	1.298	.313	2828	.03333
1.48	.505	.968	.449	.586	.396	.273	.343	re re	.04166
1.41	.540	.921	.480	.554	.425	.251	.370	distance of its stroke for the to half the	.05000
1.35	.570	.881	.508	.526	.451	.232	.393	stane for the	.05833
1.30	.595	.844	.532	.500	.473	.215	.414	its its fo	.06666
1.25	.617	.810	.554	.476	.495	1.198	.434	2 23	.07500
1.21	.638	.779	.572	.454	.514	.183	.452	The dof itted ual	.08333
1.17	657	.751	.592	.434	.532	1.160	.468	The pd of sitted	.09166
1.13	.674	.724	.607	415	.548	1.156	.483	The cend of mitted equal t	1.00000

The lap must be equal to the width of the Steam port multiplied by col 1. The lead must be equal to the width of the Steam port multiplied by col. 2.

of the Steam port multiplied by col. 2.

EXAMPLE:—Stroke 36 inches; width of port 2 inches; Steam to be cut off at half-stroke; distance of the piston from the end of its stroke when Steam is readmitted for the return stroke. 15 inches

the return stroke, 1.5 inches.  $1.5 \div 18 = .0838$  Find that number or the one nearest to it, in the right hand or last column, and take out the multipliers on the same line under the head half-stroke.

Then  $2 \times 1.21 = 2.42$  inches = the lap. And  $2 \times .638 = 1.276$  " = the lead. Table showing the amount of "LAP" required for slide valves, when the Steam is to be worked expansively.

Traverse of the	Tra	verse	of the	e Pist	on wh	en th	e Ste	am is	cut-off.
Valve in	1/4	1/3	5-12	1/2	7-12	2/3	3/4	10-12	11-12
Inches.				The	requi	red I	ap.		1
2	7/8	3/4	11 78	5/8	9 16	1/2	16	3/8	5 3 8
21/2	116	1	7/8	13	11 16 51 16	16 34	1/2	र्वेड	3/8
3	11/4	$1\frac{3}{16}$	11/8	11/	116	34	5/8	16	1/2
31/ <sub>2</sub> 4	11/2 13/4	$1\frac{5}{16}$ $1\frac{9}{16}$	$1_{16}^{3}$ $1_{16}^{7}$	11/8	116	1.1	78	9/4 13	16
41/2	2	113	116	11/2	13/8	11/4	11/8	913/436 0	3/4
572	21/8	216	113	196	11/2	13/8	114	1,40	13
51/2	$2^{5}_{16}$	23	$\frac{113}{2}$	113	15/8	11/2	13/8	11/8	78
6	21/2	$ 2\frac{7}{16} $	23	2	148	15/8	11/2	136	15
61/2	23/4	$2^{9}_{16}$	276	$\frac{2^{3}}{32}$	2	113	15/8	11/4	1
7'-	3	$\frac{2^{11}_{16}}{3}$	216	23/8	23	2	134	17/8	11/8
7½ 8	$\begin{vmatrix} 3\frac{3}{16} \\ 3\frac{5}{16} \end{vmatrix}$	$\frac{3}{3}$	$\frac{211}{3}$	$\begin{vmatrix} 21/2 \\ 25/8 \end{vmatrix}$	23/8	$\frac{2\frac{3}{32}}{238}$	$egin{bmatrix} 278 \ 2 \end{bmatrix}$	11/2	136
81/2	35/6	$3\frac{5}{16}$	33	$2^{18}_{16}$	$\frac{272}{211}$	21/2	21/8	15/8 13/4	156
972	35/8 313	35/8	$3^{16}_{16}$	316	$\frac{2_{13}^{16}}{2_{16}^{18}}$	211	214	1%	13/8
91/2	4	313	35/8	33	3	$\begin{bmatrix} \overline{2}_{16}^{\dagger 3} \\ \overline{3} \end{bmatrix}$	$2\sqrt[3]{8}$	$\overline{2}^{\prime 0}$	176
10	41/4	4	313	35	3.3	3	21/2	216	11/2
101/2	47	41/4	4	31/2	3,5	31/8	25/8	$2\frac{3}{16}$	196
11	416	476	41/4	35/8	31/2	3,3	23/4	21/4	15/8
$\frac{111}{12}$	413 5	4 9 116	416	37/8	35/8	338	$\frac{27/8}{3}$	23/8	134
24	10	1116	116	1 = 1/8	1 2	35/8	0	44/2	17/8

Note:—The traverse of the valves being ascertained, and also the amount of cut-off desired, the above table shows the amount of "LAP" required.

TABLE OF CONSTANT NUMBERS, by which to ascertain the AVERAGE PRESSURE OF the STEAM against the PISTON for DIFFERENT PRESSURE and POINTS OF CUT-OFF, from 1-4 to 7-8 of the stroke.

Point of	Constant	Point of   Cut-off.	Constant
Cut-off.	Number.		Number.
1/4	.5965	5/8	.9188
1/5	.6995	2/3	.9370
3/8	.7428	3/4	.9657
1/2	.8465	7/8	.9919

Multiply the pressure in pounds, as shown by the gauge, by the constant number opposite the point of cut-off in the left column. The product is the average.

Table showing usual consumption of coarse anthracite coal and soft wood by different sized engines, 12 hours per day.

Horse- Power.	Pounds of Coal.	Cords of Wood.	Horse-power.	Pounds of Coal.	Cords of Wood.
4 6 8 10 12 14 16 18 20 25 30 35 40 45	168 252 336 420 504 588 672 756 840 1066 1260 1458 1680 1896	$\begin{array}{c c} & 1/2 \\ & 34 \\ & 1 \\ & 1 \\ 11/2 \\ & 11/2 \\ & 21/2 \\ & 21/2 \\ & 21/2 \\ & 3 \\ & 31/2 \\ & 41/4 \\ & 43/4 \\ & 51/2 \\ \end{array}$	50 55 60 65 70 75 80 85 90 95 100	2100 2300 2520 2780 2940 3150 3360 3560 3780 3990 4200	6 61/2 71/4 8 81/2 91/4 93/4 101/2 11 113/4 121/2

Table showing the effluent velocity with which Steam at different pressures, will flow into the atmosphere, or into steam at a lower pressure

	0		
Pressure above the atmosphere.	Velocity of escape per Sec.	Pressure above the atmosphere.	Velocity of escape per Sec.
ībs.	feet.	Ibs.	feet.
1	540	. 50	1736
. 2	698	60	1777
$\frac{2}{3}$	814	70	1810
4	905	80	1835
5	981	90	1857
10	$123\bar{2}$	100	1874
10 20 30	1476	110	1889
30	1601	120	1900
40	1681	130	1909

| TABLE OF AREAS OF CYLINDERS from 1 to 36 ins. DIAM. | Diam. | Area | Diam. | Area | Diam. | Area | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In Ins. | In In

111 1116.	111 1110.	lim mo.	111 1112.	Im mo.	111 TH2'	III TIIO.	IIII IIIS
1	.78	51/2	23.7	10	78	19	283
11/2	1.7	6	28.2	11	95	20	314
2	3.1	61/2	33.1	12	113	21	346
21/2	4.9	7	38.4	13	132	22	380
3	7.	71/2	44.1	14	153	23	415
31/2	9.6	8	50.2	15	176	24	452
4	12.5	81/2	56.7	16	201	28 -	615
41/2	15.9	9	63.6	17	226	30	706
9	19.6	91/2	70.8	18	254	36	1017

To find the area—Multiply the square of the diameter in inches by .7854—For other Areas see page 73.

Table showing length of stroke and number of revolutions for different piston speeds in feet per minute.

_								,		-			
	Stroke in Ins.	Speed of Piston in feet per minute.											
		200	210	220	230	240	250	260	270	! 280			
	E. CE				Re	voluti	ons.						
	2	600	630	660	690	720	750	780	810	840			
	3	400	420	440	460	480	500	520	540	560			
	4	300	315	330	345	360	375	390	405	420			
	5 .	240	252	264	276	288	300	312	324	336			
	6	200	210	220	230	240	250	260	270	280			
	7	179	180	188	197	206	214	223	231	240			
	8	150	137	165	172	180	187	195	202	210			
	7 8 9	133	140	147	153	160	166	173	180	187			
	10	120	126	132	138	144	150	156	162	168			
	11	109	114	120	125	131	136	142	147	153			
	12	100	105	110	115	120	125	130	135	140			
	$\overline{13}$	92	97	101	106	111	115	120	125	129			
	14	86	90	94	93	103	107	111	116	120			
	15	80	84	88	92	96	100	104	108	112			
	16	75	79	82	87	90	94	97	101	105			
	17	70	74	78	8i	85	88	92	95	99			
	<b>1</b> 8	67	70	73	76	80	83	86	90	93			

Table of Units of H. P. for Different Piston Speeds. Indicated Horse-Power for each pound average pressure per square inch, with different Diam, and speed of piston.

per equal to the control of the cont													
Diam. of Cy-		Speed of Piston in feet per minute.											
linder	240	300	350	400	450	500	550	600					
lns.													
4	.091	.114	.133	.152	.171	.19	.209	.228					
5	.144	.18	.21	.24	.27	.3	.33	.36					
6	.205	.256	.299	.34	.385	.428	.471	.513					
7	.279	.348	.408	.466	.524	.583	.641	.699					
8 9	.365	.456	.532	.603	.685	.761	.837	.912					
9	.462	.577	.674	.77	.866	.963	1.059	1.154					
10 .	.571	.714	.833	.952	1.071	1.39	1.409	1.428					
11	.691	.864	1.008	1.152	1.296	1.44	1.58	1.728					
12	.820	1.025	1.195	1.366	1.54	1.708	1.884	2.05					
13	.964	1.206	1.407	1.608	1.809	2.01	2.211	2.412					
14	1.119	1.398	1.631	1.864	2.097	2.331	2.564	2.797					
15	1.285	1.606	1.873	2.131	2.409	2.677	2.945	3.212					
16	1.461	1.827	2.131	2.436	2.741	3.045	3,349	3.654					
17	1.643	2.054	2.396	2.739	3.081	3.424	3.766	4.108					
18	1.849	2.312	2.697	3.083	3.468	3.854	4.239	4.264					
19	2.061	2.577	3.006	3.436	3.865	4.295	4.724	5.154					
20	2.292	2.855	3.331	3.807	4.265	4.759	5.234	5.731					
21	2.518	3.148	3.672	4.197	4.722	5.247	5.771	6.296					
22	2.764	3.455	4.031	4.607	5.183	5.759	6.334	6.911					

Applebys Table showing the rumber of gallons discharged per minute by single-acting pumps of grokes per minute.

	15	075.	099.	.945	1.29	1.695	2.64	3.81	5.19	6.78	8.57	10.5	12.75	15.15	20.77	27.13	34.33	42.40	61.02	95.41	137.37	169.6	244.23	ps at 10
	14	.392	919	885	1.204	1.582	2.464	3.55	4.84	6.32	8.0	8.6	11.9	14.14	19.38	25.32	32.04	39.56	56.94	89.04	128.2	158.3	227.9	mnd gu
	12.			_																	_	-	_	gle-actin
되	10												-			_							_	for sing
C	6																					حد	اسد	calculated
	8																							are calc
O K	7	.196	808.	.441	.602	.791	1.232	1.778	2.45	3.16	4.20	4.9	5.95	7.07	69.6	12.66	16.02	19.78	28.47	44.52	64.10	79.15	113.97	and a
=	9													90.9	8.31	10.85	13.73	16.96	24.40	38,16	54.94	67.84	99,66	gallons
0	9	140	3 .220	315	430	2 565	088	$\frac{1.270}{1}$	1.780	2.26	2.86	3.5	4.25	5.05	6.92	9.04	11.44	14.13	20.34	31.80	45.79	56.53	81.41	2 .
G T	4	41. 112	.17(	9 255	347	9 455	8	2 1.016	387	1.82	2.29	2.8	3.40	4.04	5.54	7.23	9.15	11.30	16.27	25.44	36.63	45.23	65.12	the table are in
	es 																98.9	8.48	12.20	19.08	27.47	33.92	48.48	ii.
	2	128	944	63	98	13	76	54	146	52	72 1.14	4	1.7	1 2.02	2.77	33.0	89 4.57	27 5.45	000	61 12.72	58 18.31	07 22 61	82 32.56	s given
pl.	es. 1	-	_	_		-	_	-	_	-		-	-			-	2.2	28	4.6	6.3	9.	11.3	16.2	nantities
Diam.	in inch	-	11/4	11/6	13/4		$\frac{2}{216}$	i ori	31%	4	41/6	1	51/6	. 9	2	-00	6	2	12	15	22	186	121	The gr
	DENGTH OF STROKE IN INCHES.	LENGTH OF STROKE IN INCHES.    3   4   5   6   7   8   9   10   12   14	LENGTH OF STROKE IN INCHES.   1   2   3   4   5   6   7   8   9   10   12   14	LENGTH OF STROKE IN INCHES.	TENGTH OF STROKE IN INCHES.	1   2   3   4   5   6   7   8   9   10   12   14	LENGTH OF STROKE IN INCHES.   14   1   2   3   4   5   6   7   8   9   10   12   14   14   15   15   15   15   15   15	LENGTH OF STROKE IN INCHES.   14   1   2   3   4   5   6   7   8   9   10   12   14   14   15   15   15   14   15   15	1   2   3   4   5   6   7   8   9   10   12   14   14   15   15   14   15   15   14   15   15	LENGTH OF STROKE IN INCHES.   14   1   2   3   4   5   6   7   8   9   10   12   14   14   14   14   14   14   14	1   2   3   4   5   6   7   8   9   10   12   14   14   15   15   14   15   15   14   15   15	LENGTH OF STROKE IN INCHES.   14   1   1   2   3   4   5   6   7   8   9   10   12   14   14   14   14   14   14   14	1   2   3   4   5   6   7   8   9   10   12   14   14   17   12   14   17   18   18   18   18   17   18   18	1   2   3   4   5   6   7   8   9   10   12   14   14   15   15   15   15   15   15	LENGTH OF STROKE IN INCHES.   14   1	1         2         3         4         5         6         7         8         9         10         12         14           0.028         0.066         0.084         1.12         1.30         1.66         1.89         1.90         1.90         1.35           0.044         0.086         1.12         1.20         1.36         1.36         3.52         2.29         2.29         2.29         3.96         3.95         3.96	1         2         3         4         5         6         7         8         9         10         12         14           1028         0.056         0.084         1.12         1.40         1.66         1.96         1.824         2.52         2.20         3.20         3.39         3.39         3.00         3.39         3.00         3.39         3.00         3.39         3.00         3.00         3.39         3.00	TENGTH OF STROKE IN INCHES.   14   1   2   3   4   5   6   7   8   9   10   12   14   14   14   14   14   14   14	1         2         3         4         5         6         7         8         9         10         12         14           0.02         0.06         0.08         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06         0.02         0.06	LENGTH OF STROKE IN INCHES.   14   5   6   7   8   9   10   12   14   14   14   14   14   15   14   15   14   15   14   15   14   15   14   15   14   15   14   15   14   15   14   15   14   15   15	1         2         3         4         5         6         7         8         9         10         12         14           0.028         0.08         1.12         1.30         1.66         1.96         3.52         2.80         3.90         1.92         1.9         1.9         1.1         1.1         1.1         1.2         1.4         1.85         1.86         1.82         2.20         1.80         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         3.92         3.90         <	1         2         3         4         5         6         7         8         9         10         12         14           0.02         0.08         0.08         1.12         1.30         1.24         1.36         2.24         3.52         2.29         2.29         1.20         1.36         1.60         1.80         3.52         3.24         3.36         3.61         3.61         3.62         3.24         3.36         3.61         3.62         3.24         3.36         3.61         3.62         3.24         3.36         3.61         3.62         3.24         3.36         3.62         3.24         3.26         3.89         3.74         3.86         3.61         3.62         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.76         3.88         3.78         3.89         3.89         3.89         3.74         3.78         3.88         3.78         3.89         3.78         3.89         3.78         3.89	TENGTH OF STROKE IN INCHES.   14   1   1   1   1   1   1   1   1	1         2         3         4         5         6         7         8         9         10         12         14           0.02         0.08         0.08         1.12         1.30         1.66         7         8         9         10         12         14           0.03         0.04         0.03         0.04         1.06

strokes per minute; if required for double-acting pumps the number found in the table should be doubled. The quantity for any other number of strokes may be found by multiplying or dividing the number found in the table.

Table showing the power to raise water to different altitudes, varying from I foot to 10.000 feet.

annuaces, ran jung from river to reverse recen												
What a		2 H. H			P. will	4 H. P. will						
will rais	e per	raise	per	raise	per	raise per						
minu	te.	min	ute.	min	ute.	minute.						
gals.	feet	gals.	feet	gals.	feet	gals.	feet					
or	or	or	or	or	or	or	or					
feet.	gals.	feet.	gals.	feet.	gals.	feet.	gals.					
2.500	1	5.000	1	7.500	1	10.000						
1.250	2.	2.500	2	3.750	2	5.000	$\bar{2}$					
833	3	1.666	$\frac{2}{3}$	2.500	3	3,333	3					
625	4	1.250	4	1.875		2,500	4					
500	5	1.000	4 5	1.500	5	2.000	5					
416	6	833	6	1.250	6	1.666	6					
357	1 3 4 5 6 7	714	7	1.070	4 5 6 7	1,428	7 4					
312	8	625	8	937	8	1,250	1 2 3 4 5 6 7 8					
277	8	555	ğ	833	9	1.111	9					
$\bar{2}50$	<b>1</b> 0	500	10	750	10	1,000	10					
125	$\tilde{20}$	250	2ŏ	375	20	500	20					
83	30	166	30	250	30	333	30					
62	40	125	40	187	40	250	40					
50	50	100	50	150	50	200	50					
41	60	83	60	125	60	166	60					
$3\overline{5}$	70	72	70	107	<b>7</b> 0	142	70					
31	80	$6\overline{2}$	80	93	80	125	80					
27	60	55	90	83	90	111	90					
$\tilde{25}$	100	50	100	75	100	100	100					
		, ,,,,										

To find what an 8 Horse-Power will raise, multiply gals, or feet column under 4 Horse-Power by 2 the product will be the number of gals, or feet.

To find what any H. P. will raise, multiply gals, or feet in first column, by the H. P. you have, and the product will be the number of gals, or feet.

CAPACITY OF CISTERNS.—IN U.S. GALLONS, (2.31 Cubic Inches) FOR EACH 10 INCHES IN DEPTH.

Feet in Diam.	Gallons.	Feet in   Diam.	Gallons.	Feet in   Diam.	Gallons.
2	19.5	6 61/2 7 71/2 8	176.25	10	489.20
21/2	30.5		206.85	11	592.40
3	44.06		239.88	12	705.
31/2	59.97		275.40	13	807.4
4	78.33		313.33	14	959.6
41/2	99.44	81/2	353.72	15	1101.6
5	122.40	9	396.56	20	1958.6
51/2	148.10	91/2	461.40	25	3059.9

TABLE SHOWING THE CAPACITY OF CISTERNS AND TANKS, COMPUTED IN BARRELS OF 311/2 GALLONS.

Depth		D I	I A M	ET	ER :	IN F	EET	`.	
in feet.	5	6	7	8 j	9.1	10	11	12	13
5	23.3	33.6	45.7	59.7	75.5	93.2	112.8	134.3	157.6
6	28.0	40.3	54.8	71.7	90.6	111.9	135.4	161.1	189.1
7 8	32.7	47.0	64.0		105.7	130.6	158.0	188 0	220.6
8	37.3	53.7	73.1		120.1	149.2	180.5	214.8	
9	42.0	60.4		107.4		167.9	203.1	241.7	283.7
10	46.7	67.1		119.4		186.5	225.7	268.6	315.2
11	51.3			131.3		205.1	248.2	295.4	346.7
12	56.0			143.2		223.8	270.8	322.3	
13	60.7			155.2		242.4	293.4	349.1	409.7
14	65.3			167.1		261.1	315.9	376.0	
15	70.0			179.0		279.8	338.5	402.8	
16	74.7			191.0		298.4	361.1	429.7	504.3
17	79.3			202.9		317.0	383.6	456.6	535.8
18	84.0				272.0	335.7	406.2	483.4	567.3
19	88.7				287.0	354.3	428.8	510.3	598.0
20	93.3	134.3	182.8	238.7	302.1	373.0	451.3	537.1	630.4

For cisterns larger in diameter multiply the barrels of half the diameter by four and the product will be the number of barrels which it will contain. Thus 10 feet deep by 20 feet in diameter,  $\frac{1}{2}$  of 20 feet is 10 feet, look opposite 10 feet in first column and under 10 feet we find  $186.5 \times 4 = 746$  barrels.

Table showing the power in foot pounds, required to raise a given quantity of water a given height.

Height										
in feet.	1	2	3	4	5	10	20	30	40	50
1	20	40	60	80	100		300		550	675
2	30	60	90	120	150		500			1175
3	40	80	120	160	200	375	700		1350	1675
4 5	50	100	150			475	900		1750	
	60	120	180	240	300	575	1100			2675
10	110	220	330	440	500	1076	2102	3128	4154	5180
20	210	420	630	840	1050	2076	4102	6128	8154	10180
30	310	620	930	1240	1550	3076	6102	9128	12154	15180
40	410	820	1230	1640	2050	4076	8102	12128	16154	20180
50					2550			15128		
100	1010	2020	3030	4040	5050	10076	20102	30128	40154	50180

The numbers given in the table are in foot its, including allowance for friction.

A foot pound = 1 lb. raised 1 foot high in 1 minute.

A man is capable of exerting 6.000 foot pounds for 10 hours a day. 33,000 ft. lbs. = 1 Horse-Power.

Table showing quantity of water per lineal foot in pumps verticle pipes of different diameters

	verticie	pipes of	ainerent	diamete	rs.
		No. of			No. of
Pump in	gal. per	Cu. ft. per	Pump in	gal. per	Cu. ft. per
Inches.	lin. ft.	lineal foot	Inches.	lin. ft.	lineal foot
2	.136	.0218	8	2.176	.3490
21/4	.172	.0276	81/4	2.314	.3712
21/2	.212	.0340	81/2	2.456	.3940
$23\overline{4}$	.257	.0412	83/4	2.603	.4175
3	.306	.0490	9	2.754	.4417
31/4	.359	.0576	91/4	2.909	.4666
31/9	.416	.0688	91/5	3.068	.4923
$33\sqrt{4}$	.478	.0766	93/4	3.232	.5184
4	.544	.0872	10	3.400	.5454
41/4	.614	.0985	101/4	3,572	.5730
41/2	.688	.1104	101/2	3.748	.6013
43/4	.767	.1230	103/4	3.929	.6302
5	.850	.1363	11	4.114	.6599
51/ <u>4</u> 51/ <u>2</u>	.937	.1503	111/4	4.303	.6902
51/2	1.028	.1649	111/2	4.496	.7212
53/4	1.124	.1803	113/4	4.694	.7529
6	1.224	.1963	12	4.896	.7853
61/4	1.328	.2130	121/2	5.312	.8521
61/2	1.436	.2304	13	5.746	.9217
6¾ 7	1.549	.2489	131/2	6.196	.9934
7	1.666	.2672	14	6.664	1:0689
71/4	1.787	.2866	15	<b>7.</b> 650	1.2271
71/2	1.912	.3067	16	8.704	1.3962
73/4	2.042	.3275	18	11.016	1.7670

# AIR IN MOTION.

Velocity of the wind.		Force or	Common amplications		
Miles per Hour.	Feet per Sec.	pressure per sq. ft. in Ibs. avoir.	Common applications of the Force Wind.		
1	1.47	.005	Hardly preceptible.		
$\frac{2}{3}$	$\frac{2.93}{4.40}$	.020 }	Just " -		
2 3 4 5	5.87 7.33	.079 {	Gentle pleasant winds.		
10 15	$\frac{14.67}{22.00}$	.492 { 1.107 \	Pleasant brisk gale.		
20 25	29.34 36.37	1.968 2	Very brisk.		
30 35	44.01 51.34	4.429 { 6.027 {	High winds.		
40	58.68	7.873 (	Very high.		
45 50	66.01 73.35	9.963 5 12.300	A Storm or Tempest.		
60 80	88.02 117.36	17.715 31.400	A great storm. A hurricane.		
- 50	TT4.00	01.400	A maricane.		

TABLE SHOWING NUMBER OF FEET IN SQUARE FRAMES OF DIFFERENT SIZES AND WIDTHS.

1 10212	MES (	) F DI	I I II	101311	1 1312	LES A	ND I	VIDI.	ць,
Leng- th in		Wi	dth o	f Mo	uldin	gs in	Inche	s.	
Ins.	1	11/2	2	21/2	3	31/2	4	41/2	5
8 10 12 14 16 18 20 22 24 26 30 32 34 40 42 44 46 48 50 52 54 56 62 64 64 66	2	21	3 3 3 5 5 5 6 6 6 6 7 7 7 8 8 5 8 9 9 9 9 10 10 10 10 11 11 11 11 11 11 11 11 11	3334 4 1583 1585 6 667 7778 8 1583 9 9 9 10 10 10 11 11	31	32	- 4	41	42
10	$2\frac{1}{3}$	$2\frac{2}{3}$	3	31	32	4	413	42	5
- 12	$2\frac{2}{3}$	3	31	33	4	413	42	5	51
14	3	31	33	4	41/3	42	5	51	$5\frac{5}{3}$
16	31/3	33	4	41/3	42	5	$5_{3}^{1}$	53	6
18	38	4	413	423	5	51/3	$5_{3}^{2}$	6	63
20	4	41/3	43	5	$ 5_{3}^{1} $	$5\frac{2}{3}$	6	$ 6^{1}_{3} $	$6^{2}_{3}$
22	41	43	5	53	53	6	$6_{3}^{1}$	$6^{2}_{3}$	7
24	$4\frac{2}{3}$	5	53	$5\frac{2}{3}$	6	61	$\frac{6^{2}}{3}$	7	$7\frac{1}{3}$
26	5	$5\frac{1}{3}$	53	6	613	$6\frac{2}{3}$	7	$\frac{7_3}{3}$	$7_{3}^{2}$
28	$5\frac{1}{3}$	$5\frac{2}{3}$	6	$6\frac{1}{3}$	62	7	$\frac{7_3}{3}$	$7\frac{2}{3}$	8
30	$5\frac{2}{3}$	6	613	63	7	71	72	8	$8_{3}^{1}$
32	6	$6\frac{1}{3}$	63	7	$\frac{7\frac{1}{3}}{}$	73	8	$ 8_{3}^{1} $	$8_{3}^{2}$
34	$ 6\frac{1}{3} $	63	7	71	73	8	$8_{3}^{1}$	82	9 "
36	$6\frac{2}{3}$	7	71/3	73	8	81	82	9 **	91
38	7	$7\frac{1}{3}$	72/3	8	81	82	9	$9_{3}^{1}$	$9_{3}^{2}$
40	$\frac{7_{\frac{1}{3}}}{3}$	$\frac{72}{3}$	8	81	82	9	91	93	10
42	72	8	81	82	9	93	92	10	$10^{\frac{1}{3}}$
44 -	8	81/3	82	9	91	93	10	101	$10^{2}_{3}$
46	81	83	9	93	$9\frac{2}{3}$	10.	103	102	11
48	82	9	91	93	10	$10\frac{1}{3}$	103	11	113
50	9	91	92	10	$10\frac{1}{3}$	103	11	$11\frac{1}{3}$	$11_{3}^{2}$
52	91	93	10	103	103	11	1113	112	12
54	92	10	101	103	11	1113	$11_{3}^{2}$	12	$12\frac{1}{3}$
56	10	2233354444555566677788889990110111	103	11	113	112	12	121	123
58	101	103	11	111	113	12	121	$12^{2}_{3}$	13 .
60	22233344445556666777888999901101	11	1113	113	12	121	123	13	131
62		1113	113	12	121	123	13	131	133
64	11½ 11½	11½ 11½ 12	1113 1123 12 1213	$11\frac{1}{3}$ $11\frac{2}{3}$ $12$ $12\frac{1}{3}$ $12\frac{1}{3}$	34 4 4 4 4 5 5 5 5 6 6 6 6 7 7 7 7 7 8 8 10 8 9 9 15 8 9 10 10 10 10 10 11 11 11 11 11 11 11 11	4 4 4 5 5 5 6 6 6 6 7 7 7 7 8 8 8 8 9 9 9 9 10 11 11 11 11 12 12 12 13 13 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	$\begin{bmatrix} 4 & 4 & 4 & 5 & 5 & 5 & 5 & 6 & 6 & 6 & 6 & 7 & 77 & 8 & 6 & 8 & 9 & 9 & 9 & 9 & 9 & 9 & 9 & 9 & 9$	445 555 6 6667 7788 8889 9 99 9 10 1001 1112 1223 1334	45 5 5 5 6 6 6 6 7 7 7 7 8 8 8 9 9 9 0 10 2 2 10 2 3 10 2
66	112/3	12	121	123	13	133	$\frac{ 13_3^2 }{ 13_3^2 }$	114	141

RULE.—Take the number of inches in half the size of a frame, (thus; a frame 22×28 added, making 50 inches), find 50 in the first column, select your width, and you have the number of feet desired.

## SURFACE OF BOILER TUBES.

Diam.	Length.	Surface.	Diam.	Length.	Surface.
Ins.	ft. in.	sq. ft.	Ins.	ft. in.	sq. in.
21/2	$5 \cdot 0$	3.27	3	6 0	4.70
66' -	5 3	3.42	66	6 3	4.90
66	5 6	3.60	66	6 6	5.10
66	5 9	3.75	66	7 0	5.50
44	6 0	3.90	66	7 6	5.89
66	6 3	4.05	66	8 0	6.28
66	6 6	4.20	- "	8 6	6.67

VALUE OF IRON PER TON OF 2.240 POUNDS AT FROM 2c. TO 13c. PER LB.

per lb.	Ton	per Ib	₩ Ton.	per Ibi	₩ Ton	per lb	P Ton.
$\overline{2}$	\$44.80	43/4	\$106.401	71/2	168.0011	101/4	\$229.60
21/8	47.60	47/8	109.20	75/8	170.80	$103/\hat{8}$	232.40
21/4	50.40	5	112.00	73/4	173.60	101/2	235.20
23/8	53.20	51/8	114.80	77/8	176.40	105/8	238.00
$21/_{2}$	56.00	51/4	117.60	- 8	179.20	103/4	240.80
234	85.80	53/8	120.40	81/8	182.09	$10\frac{7}{8}$	243.60
25/8	61.60	51/2	123,20	81/4	184.80	11	246.40
27/8 3	64.40	55/8	126.00	83/8	187.60	111/8	249.20
3	67.20	534	128.80	81/2	190.40	111/4	252.00
31/8	70.00	57/8	131.60	85/8	193.20	113/8	254.80
31/4	72.80	6	134.40	83/4	196.00	111/2	257.60
33/8	75.60	61/8	137.20	87/8	198.80	$115\sqrt{8}$	260.40
31/2	78.40	61/4	140.00	9	201.60	113/4	263.20
35/8	81.20	63/8	142.80	91/8	204.40	1178	266.00
33/4	84.00	61/2	145.60	91/4	207.20	12	268.80
37/8	86.80	63/8	148.40	93/8	210.00	121/8	271.60
4 .	89.60	63/4	151.20	91/2	212.80	121/4	274.40
41/8	92.40	67/8	154.00	95/8	215.60	123/8	277.20
41/4	95.20	7	156.80	934	218.40	121/2	280.00
43/8	98.00	71/8	159 60	97/8	221.20	125/8	282.80
41/2	100.80	71/4	162.40	10	224.00	123/4	285.60
45/8	103.60	73/8	165.204	101/8	226.80	13	291.20

## DEPRECIATION OF MACHINERY.

Per Annum on first Cost.	Depreci- ation.	Wear and Tear.	Total.
Engines. Boilers. Machinery tools. Mill work, shafti'g & gear. Bands and Belts.	$\begin{bmatrix} 6 & \text{per } \phi \\ 10 & \text{``} \\ 71/2 & \text{``} \\ 4 & \text{``} \end{bmatrix}$	3 per ¢ 3 " 31/2 " 21/2 " 45 "	9 per ¢ 13 " 11 " 61/2 " 45 "

### REGULAR POLYGONS.

No. sid's	Name.	Numbers on square for mi	tre.
4 5 6	Square, Pentagon. Hexagon. Heptagon. Octagon.	12½ and 7¼, mark along longes Any two equal numbers. 7¼ and 10, mark along shortest 7¼ and 12½, """ 6" 12½,"""" 2 and 5; or 7 and 17"" 6½ and 20.	

Regular polygons are plain figures whose sides are *equal* straight lines. A regular polygon of six sides is often called a six-square, and one of eight sides an eight-square, etc.

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Sec., 4.934 U. S. Rev. Stat. reads:	The :	following
shall be rates for patent fees;		
On application for patent, except in design	cases	. \$15.
In design cases for 3 y'rs and 6 mo.		10.
In design cases for 7 years.		15.
In " " 14 "		30.
Filing caveat.		10.
" disclaimer.		10.
Re-issue application.		30.
On appeal from primary examiners.		10.
On appeal to Commissioner.		20.

#### CEMENTS.

Cast-Iron Slowly Setting.—Two ounces of sal-ammoniac, 1 cunce sulphur, and 16 cunces of borings or filings of cast-iron, to be mixed well in a mortar, and kept dry. When required for use, take one part of this powder to 20 parts of clear iron borings or filings, mix thoroughly in a mortar; make the mixture into a stiff paste with a little water, and then it is ready for use. A little fine grindstone sand improves the cement.

CAST-IRON QUICKLY SETTING.—One ounce sal-ammoniac. 2 ounces of sulphur, and 80 ounces of iron filings or boring. Mix the same as for "slowly setting."

RED LEAD CEMENT FOR FACE JOINTS.—Equal parts of white and red lead, mixed with linseed-oil to the proper consistency.

For Leather.—By dissolving in a mixture of 10 parts; of bisulphide of carbon and 1 part of oil of turpentine enough gutta-percha to thicken the composition. The leather must be free from grease, which may be done by placing a cloth between the leather and a hot iron.

The pieces cemented must be pressed together until the

cement is dry.

For Brass and Glass.—Boil 3 parts of resin with 1 part of caustic soda and 5 parts of water. Add 5 times its weight of plaster of Paris. It sets finely in from ½ to 34 of an hour. Zinc, white lead, or percipitated chalk may be substituted for plaster, but hardens more slowly.

For Stone or Marble.—The best cement for mending marble or any kind of stone, is made by mixing 20 parts of litharge and one part of freshly-burned lime in fine dry powder. This is made into a putty by the addition of linseed-oil. It sets in a few hours, having the appearance of light stone.

FIRE AND WATER-PROOF CEMENT.-To 1/2 pint of milk, put an equal quantity of vinegar, in order to curdle it; then separate the curd from the whey, and mix the whey with 4 or 5 eggs, beating the whole well together. When it is well mixed, add a little quick lime through a sieve, until it has acquired the consistency of thick paste. this cement, broken vessels and cracks of all kinds may be mended. It dries quickly, and resists the action of water as well as considerable degree of fire.

FOR FASTENING LEATHER TO IRON, CHINA, OR GLASS.— To 1 quart of glue dissolved in good cider vinegar; add 1 ounce of good Venice turpentine. It should be allowed to simmer about 1/2 day.

HOW TO MIX A GOOD ADHESIVE CEMENT.-MIX pulverized Gum-Arabic with its weight of finely powdered calcined alum. When mixed with a small quantity of water, it forms a cement which unites wood, paper, porcelain, glass, and crockery very finely. It must be kept dry in powder and moistened only as needed.

FOR CISTERNS AND WATER CASKS.—Melted glue 8 parts: linseed-oil, 4 parts; boiled into varnish with litharge.

This cement hardens in about 48 hours, and renders the joints of wooden cister ns and casks air and water tight.

RUBBER BELTING .-- Take 16 parts of Gutta-Percha or India-Rubber; 2 parts common pitch, and 1 part linseedoil. Melt together, and use hot. This cement will unite leather or rubber that has not been vulcanized.

FOR STEAM JOINTS .- Take 2 parts powdered litharge, very fine sand, 2 parts; slacked quick-lime, 1 part.

very line said, 2 parts, stated quick-line, 1 parts and all together. So use. Mix the proper quantity with boiled linseed-oil, and apply quickly. It gets hard very soon.

Or 10 pounds of ground litharge; 4 pounds of ground Paris-white; ½ pound of yellow othre and ½ ounce of hemp: Cut into lengths of ½ inch: Mix all together with boiled linseed-oil to the consistency of a stiff putty. This cement resists fire and will set in water.

AMMONIA SHELLAC CEMENT. -- As rubber plates and rings are now-a-days used almost exclusively for making connections between steam and other pipes and apparatus, much annoyance is often experienced by the impossibility or imperfection of an air-tight connection. This is obviated entirely by employing a cement which fastens alike well to the rubber and to the metal or wood. Such cement is prepared by a solution of shellac in ammonia. This is best made by soaking pulverized gum-shellac in 10 times its weight of strong ammonia, when a slimy mass is obtained which in three to four weeks, will become liquid without the use of hot water. This softens the rubber and becomes after volatilization of the ammonia, hard and impermeable to gases and fluids.

CEMENTS FOR BELTS.—The cements used for belts may be made by melting together; I part shellac; 2 parts pitch; 2 parts linseed-oil; 4 parts India-rubber; 16 parts guttapercha, until thoroughly incorporated. It is applied warm, in a thin coating, very quickly, and the 2 parts of the belt are properly and firmly clamped together and left until completely set.

CEMENT FOR BELTS.—Of common glue and American isinglass, take equal parts; place in a kettle, add sufficient water to cover the whole. Let them soak 10 hours; then bring the mixture to the boiling point, and add tannin, until the whole becomes soapy or appears like the white of eggs; apply it warm. Buff the grain off the leather where it is to be cemented; rub the joint surfaces solidly together, and let it dry for a few hours.

TRANSPARENT.—A transparent cement may be made by dissolving 75 parts of India-rubber (not vuncanized) in 60 parts of chioroform, and adding to this solution 15 parts of gum mastich. Balsam of fir will also serve the purpose, as it is a strong cement when not exposed to heat. Both the cement and the edges of the article to which it is applied should be previously warmed before joining.

For Leather, Wood, etc.—A cement resisting the action of water both hot and cold, and most of the acids and alkalies. Three parts, by weight, of shellac and 1 part of caoutchouc are to be dissolved in separate vessels, in ether free from alcohol, applying a gentle heat. When fairly dissolved, the 2 solutions are to be mixed. If the glue be thinned by the admixture of ether, and applied as varnish to leather, it renders a joint or seam water-tight.

#### VARNISHES.

LAC VARNISH.—Five parts of lac, 1 of turpentine, dissolve in 5 times its weight of alcohol; keep warm until fluid, then strain.

SPAR VARNISH.-Boiled oil and resin.

GOLD VARNISH.—Turmeric, 1 drachm; gamboge, 1 dr; oil of turpentine, 1 quart; shellac, 5 ounces: sandarach, 5 ounces; dragons-blood, 7 drachms; with occasional shaking, for 14 days in a warm place, set it aside to fine and pour off the clear.

VARNISH FOR IRON.—Dissolve in 2 pounds of tar-oil 15 pound asphaltum, 1/2 pound of powdered resin, mix hot and apply cold.

VARNISH FOR METALS.—Dissolve 1 part of bruised copal in 2 parts of strong alcohol. It dries very quickly.

OIL VARNISH.—Dissolve resin in turpentine to about the consistency of treacle; add 2 pints of linseed-oil to 1 of resin and turpentine.

VARNISH FOR WOOD PATTERNS.—Gum-shellac, 3 ounces; and resin, 1½ ounce; dissolved in a pint of wood naphtha.

Varnish for Plaster Casts.—A quarter of an ounce of soap is dissolved in a pint of water, and an equal quantity of wax afterwards incorporated. The cast is dipped in this liquid, and after drying a week is polished by rubbing with soft linen. The surface produced in this manner approaches the polish of marble. When intended to resemble bronze, a soap is used, made of linseed-oil and soda colored by the sulphates of Copper and Iron.

VARNISH FOR IRON AND STEEL.—Clear grains of mastic, 10 parts; camphor, 5 parts; sandarach. 15 parts; and elemi, 5 parts; dissolved in a sufficient quantity of alcohol, and apply without heat. This varnish will retain its transparency, and the metallic brilliancy of the articles will not be obscured.

BLACK VARNISH.—Heat to boiling, 10 parts of linseed-oil varnish with burnt umber, 2 parts, and powdered asphaltum, 1 part. When cooled, dilute with spirits of turpentine as required.

A VARNISH TO GILD WITH, WITHOUT GOLD—Take half a pint of spirits of wine, in which you dissolve I drachm of saffron, and half a drachm of dragon's-blood, both previously well pulverized together. Add this to a quantity of Shell-lac varnish, and get it on fire with 2 drachms of aloes.

A VARNISH FOR FASTENING THE LEATHER ON TOP ROLLERS IN FACTORIES.—Dissolve 234 ounces of Gum Arabic in water, and so much isinglass dissolved in brandy and it is fit for use.

INITATION GOLD VARNISH.—As a substitute for the expensive "gold varnish" 1/2 gallon of turpentine, 1/2 a gill of aspaltum, 2 ounces of yellow aniline, 4 ounces of umber, 1 gallon of turpentine varnish, and 1/2 pound of gamboge, mixed and boiled for ten hours. This is said to have as good an effect as the gold varnish and is very cheap.

#### ENAMELS.

WHITE ENAMEL.—Potash 25 parts; arsenic, 14 parts; glass, 13 parts; salt-petre, 12 parts; flint 5 parts; and lith-arge, 3 parts.

BLACK ENAMEL.—Clay, 2 parts; protoxide of Iron 1 part.

BLUE ENAMEL.—Fine paste, 10 parts; Nitre, 3 parts; color with cobalt.

Green Enamel.—Frit, 1 pound; oxide of C opper, 1/2 ounce; red oxide of Iron, 12 grains.

YELLOW ENAMEL.—White lead, 2 parts; alum, white oxide of Antimony, and sal-ammoniac, each 1 part.

GELATINE GLUE.—If gelatine which has been swelled in cold water, be immersed in linseed-oil and heated, it dissolves and forms a glue of remarkable tenacity which when once dry perfectly resists dampness, and two pieces of wood joined by it will separate any where else rather than at the joint, ordinary glue may be thus dissolved, and sometimes a small quantity of red-lead in powder is added.

MARINE GLUE.—India-Rubber, 1 part; coal-tar naphtha 8 to 10 parts; shellac, 15 to 20 parts; melted together. Use hot. Glue dissolved in skimmed milk will resist the action of moisture; also glue softened with boiled oil or resin, and its weight of Iron oxide added.

WATER-PROOF GLUE.—Boil 8 parts of common glue with about 30 parts of water, until a strong solution is obtained, add 4½ parts of boiled linseed-oil and let the mixture boil 2 or 3 minutes, stirring it constantly.

ETHER GLUE.—An excellent glue is made by dissolving glue in nitric ether; this fluid will only dissolve a certain amount of glue, consequently the solution cannot be made too thick. The glue solution obtained has about the consistency of molasses, and is doubly as tenacious as that made by hot water. If a few pieces of caoutchoue cut into scraps the size of buck-shot be added and the solution be allowed to stand a few days, being frequently stirred, it will be all the better, and will resist dampness twice as well as glue made with water.

LIQUID GLUE.—Glue, water, and vinegar, each 2 parts. Dissolve in a water bath, then add alcohol, 1 part.

PARCHMENT.—Parchment shavings, 1 pound; water, 6 quarts. Boil until dissolved, then strain and evaporate slowly to the proper consistency.

#### POLISHING COMPOUNDS.

Paste for Cleaning Metals.—Oxalic acid, 1 part; rotten stone, 6 parts. Mix with equal parts of train-oil

and spirits of turpentine.

To CLEAN BRASS.—Brass that has not been gilt or lacquered may be cleaned by washing with alum boiled in strong lye, in proportion of an ounce to a pint; afterwards rub with strong tripoil.

Polish for Silver, Gold, Brass and Glass.—Take 5 pounds of the best Spanish whiting, and with it, mix 3 ounces of alcohol, and then wet to the consistency of dough, make into cakes and dry.

CLEANING SILVER, GLASS, ETC.—Emersons compound for polishing and cleaning glass, silver-plate, tinware and surfaces that permit only slight friction and but little action, consists of water 4 onuces; carbonate of ammonia 1 ounce. When dissolved add 16 ounces of Paris white, with aniline for coloring. This forms a solid, as the Paris white consists of white lead, all who purchase this compound should beware of using it upon the inside of culinary vessels.

TO FRENCH POLISH FURNITURE.—For the polish take 1 pint of spirits of wine, add 1/2 ounce gum shellac, 1/2 ounce seed lac, 14 ounce gum sandarac; submit the whole to a gentle heat, frequently shaking it until the gums are dis-solved, when it is fit for use. Make a roller of list, put a little of the polish upon it, and cover that with soft linen rags which must be lightly touched in cold-drawn linseedoil. Rub the wood in a circular direction (not covering too large a piece at one time) until the pores of the wood are filled up; after this rub in the same manner spirits of wine with a little of the polish added to it.

PATENT LEATHER POLISH. —A splendid polish for patent leather, which is used as a blacking in the ordinary way and requires no brushes for polishing; is made by boiling well together ½ pound brown sugar, I ounce gum-arabic and 2 pounds of ivory black. Allow this mixture to cool and become settled and then bottle it.

For Holes in Castings. -Sal-ammoniac, 2 parts; sulphur in powder, 1 part: powdered iron turnings, 80 parts. Make into a thick paste. The ingredents composing this cement should be kept separate and not mixed until required for use.

TO KILL KNOTS.—Cover them with fresh slacked lime for 24 hours; scrape lime off and lay on a coat of red and white lead mixed with glue-size. Pumice-stone when dry and lay on some paint.

FILES (RECUTTING).—Lay dull files in diluted sulphuric acid until they are bit in deep enough.

WATCH-MAKERS OIL, WHICH NEVER CORRODES OR THICKENS -Place coils of thin sheet lead in a bottle of olive-oil, expose it to the sun for a few weeks, and pour off the clear oil.

FRENCH POLISH.-Five ounces of naphtha, 1 ounce of shellac, 1 drachm of myrrh, 10 grains of isinglass, 6

drachms of olive-oil.

Bronzing, or Bronzing Liquid, -Sulphate of Copper, 1 ounce; sweet spirits of nitre, I ounce; water, I pint. Mix well. In four or five days it will be fit for use.

Brown Tint for Iron and Steel.—Dissolve, in 4 parts; of water, 2 parts of crystallized chloride of iron, 2 parts of chloride of antimony, and 1 part of gallic acid, and apply the solution with a sponge or cloth to the article, and dry it in the air. Repeat this any number of times, according to the depth it is desired to produce. Wash with water and dry, and finally rub the article over with boiled linseedoil. The metal thus receives a brown tint and resists moisture. The chloride of antimony should be as little acid as possible.

Browning for Gun Barrels.—Tincture of muriate of iron, 1 ounce; nitric ether, 1 ounce; sulphate of copper; 4 scruples; rain water, 1 pint. If the process is to be hurried, add 2 or 3 grains of oxymuriate of mercury. When the barrel is finished, let it remain a short time in lime water, to neutralize any acid which may have penetrated; then rub it well with an iron wire scratch-brush.

Bronzing Fluid for Guns.—Nitric acid, sp. gr. 1, 2; pure nutric ether, alcohol, muriate of iron, each 1 part. Mix, then add sulphate of copper 2 parts, dissolved in water 10 parts.

PATINA ANTIQUA BRONZE.—Bronze of a good quality acquires, by oxidation, a fine green tint. Corinthian brass receives, in this way, a beautiful clear, green color. This appearance is imitated by an artificial process, called bronzing. A solution of sal-ammoniac and salt of sorrel in vinegar is used for bronzing metals, any number of layers may be applied, and the shade becomes deeper in proportion to the number applied. For bronzing sculptures of wood, plaster figures, etc. etc., a composition of yellow ochre, Prussian blue, and lamp-black, dissolved in water is employed.

NON-CONDUCTING COTERING FOR STEAM-BOILERS AND PIPES.—Make a thin paste of boiling water and flour, then stir in as much sawdust as it can hold together. After drying it will adhere to iron when slightly warmed, after which several coats may be applied in succession. It may be made water-proof by painting with coal-tar.

FLOUR PASTE.—To make paste that will keep a long time mix with each 100 pounds of flour; 5 pounds of alum, 8 ounces of sulphate of lime, and 2 ounces of oil of sassafras.

Parting Sand.—Burnt sand scraped from the surface of castings.

LOAM. - Mixture of brick, clay, and old foundry sand.

BLACKENING FOR MOULDS.—Charcoal powder; or, in some instances, fine coal-dust.

BLACK-WASH. - Charcoal, plumbago, and size.

To Soften Horn.—Take 1 pound, of wood-ashes, add 2 pounds of quick-lime, put them into a quart of water, let the whole boil until reduced to 1-3, then dip a feather into it. if the plume comes off on drawing it out, then it is boiled enough; when settled filter it off, and in the liquor, add shavings of horn, let them soak for 3 days, then rubbing oil on your hands work the horn into a mass, and print or mould it in what ever shape you want.

Easy way of Cleaning the Hands from Dyes etc.— Take a small quantity of pot-ash or pearl-ash in your hand, pour into it a small quantity of water, rub it well all over your hands with a little sand, then wash it off, take in your hands a small quantily of chemic (chloride of lime), pour a little water into it, and rub it well on the hands in a semi-liquid state; wash the hands well in water, and they will be clean. If not perfectly clean, repeat the operation.

PRESERVATIVE FOR STEEL.—Caoutchouc, 1 part; turpentine, 16 parts; and boiled oil, 8 parts; well mixed and boiled together, caoutchouc should first be dissolved in the turpentine by gentle heat, and the boiled oil added, it should be applied with a brush, and may be removed by turpentine.

To Prevent Iron from Rusting.—Warm it, then rub with white wax; warm again to allow the wax to prevade the entire surface, or immerse the iron in boiled linseed-oil, and allow it to dry upon the metal.

Brazing.—The edges filed or scraped clean and bright, covered with spelter and powdered borax, and exposed in a clear fire to a heat sufficient to melt the solder.

MIXTURE FOR WELDING STEEL.—One part of sal-ammoniae and 10 parts of borax, pounded together and fused until clear, when it is poured out, and when cool reduce to powder.

ETCHING SOLUTION FOR IRON AND STEEL.—Take 4 of nitric acid, 2 of sal-ammoniac, 1 of sulphate of copper, and 72 parts water. This is by weight.

WATER ANNEALING.—Heat the steel to a red heat, and let it lie a few minutes, until nearly black hot, then throw it into soap suds. Steel in this way, may be annealed softer than by putting in the ashes on the forge.

EVERLASTING PASTE.—Dissolve half a teaspoonful of alum in a pint of water; when it is cold, for it should be heated when the alum is mixed with it, stir in flour enough to make it about as thick as rich cream; do not leave a lump in it; stir in as much powdered rosin as will lie on a cent piece. Put a saucepan on the stove, put a teacupful of boiling water in it, then stir in the mixture; stir it constantly to keep it from burning. Add a few drops of winter-green. When it is about as thick as mush take it from the fire, put it in a jar or glass can and set it where it will be cool. It will become hard, and when needed for use take out a little and soften it with warm water; it will only take a minute or two to do this. This paste will keep a year at least.

## STAINING WOODS.

Rosewood.—Boil 8 ounces of logwood in 3 pints of water until reduced to 1/2; apply it boiling hot 2 or 3 times, let-

ting it dry each time. Put in the streaks with a camel's hair brush dipped in a solution of copperas and verdigris in a decoction of logwood.

LIGHT MAHOGANY.—Brush over the surface with diluted nitrous acid, and when dry apply with a soft brush the following: Four ounces of dragon's blood, 1 ounce of carbonate of soda, 3 pints of alcohol. Let it stand in a warm place, shake it frequently and then strain.

To STAIN MUSICAL INSTRUMENTS.—Boil 1 pound of ground Brazil wood in 3 quarts of water for 1 hour; strain it, then add ½ an ounce of cochineal; boil ½ hour longer. This makes a crimson stain.

EBONY.—Wash the wood several times with a solution of sulphate of iron; let it dry, then apply a hot decoction of logwood and nutgalls. When dry wipe it with a wet sponge; and when dry again polish it with linseed-oil.

PURPLE.—Boil a pound of chip logwood in 3 quarts of water for an hour; then add 4 ounces of alum.

BLUE.—Boil 4 parts of alum with 85 parts of water.

TO IMITATE EBONY.—Infuse gall-nuts in vinegar wherein you have soaked rusty nails; then rub your wood with this; let it dry, polish and burnish.

TO PREVENT LOGS AND PLANKS FROM SPLITTING.—LOGS and planks split at ends because the exposed surface dries faster than the inside. Saturate muriatic acid with lime, and apply like whitewash to the ends. The chloride of calcium formed attracts moisture from the air, and prevents the spliting.

TURNING OR CUTTING METAL WITH PETROLEUM.—A machinist has discovered that by keeping his turning tools constantly wetted with petroleum, he was able to cut metals and alloys with them, although when the tools were used without the oil, their edges were turned and dulled. The hardest steel can be turned easily if the tools be thus wet with a mixture of 2 parts of petroleum with 1 part of turpentine.

WATER-PROOF BOOTS.—The following is said to have been used by the New England fishermen for over a century: Tallow 4 ounces; rosin and bees-wax, of each 1 ounce: melt together in a gentle heat, and add an equal bulk of neats-foot oil. This is first melted and applied to the boots, rubbing it in before the fire; it will make them soft, and at the same time water-proof.

TRACING PAPER.—Nut-oil, 4 parts; turpentine, 5 parts; mix and apply to the paper, then rub dry with flour and brush it over with ox gall.

TRACING PAPER.—A very good tracing-paper may be made by saturating with a camel-hair pencil the finest tis-

sue paper with the following mixture:-Half an ounce of the balsam of Canada, to one ounce of the spirits of turpentine, shaken well together in a two ounce bottle, it requires no heat, When covered with the mixture, hang the paper on a line to dry; then wash in like manner the other side.

Paper for Draughtsmen etc.—Powdered tragacanth, 1 part; water 10 parts. Dissolve and strain through clean gauze, then lay it smothly upon the paper, previously stretched upon a board. This paper will take either oil or water color.

TRANSFERRING PAPER.-Take half a sheet of very fine bank post paper, lay it on a clean place and rub it well with the scrapings of red chalk; a small bit of sponge is good for this purpose. Apply the chalk, until the paper is all one color, then with a piece of clean old muslin, rub the greater part of the color from the surface. The color may be renewed occasionally as the marking becomes faint.

BLUE PRINTS FOR COPYING MECHANICAL DRAWINGS ETC.

Take 1% ounces pure Ammonia Citrate of Iron, 8 ounces distilled water or pure rain water. Pure Ferricyanide (Red Prussiate of Potash), 114 ounces, 8 ounces distilled water. Mix separately and unite. Keep in yellow bottle or in the dark.

To sensitize paper, moisten it uniformly with the liquid by means of a soft clean camel hair brush and suspend in a dark room to dry. Keep from light.

To print the design or drawing put the sensitized paper on a flat surface and then lay the drawing over it and cover with a pane of glass. Expose to the Sun for 15 to 30 minutes (according to the brightness of the Sun) and then rinse thoroughly with pure rain or distilled water.

# FACTS FOR FARMERS.

Table Showing the Quantity of Garden Seeds Required to Plant a Given space.

DESIGNATION. Asparagus.

Beets.

SPACE AND QUANTITY OF SEEDS. 1 oz. produces 1000 plants and requires a bed 12 feet square.

Beans, pole, large. 1 " " small. 1 "

1000 plant a bed 4 ft. wide, 225 feet long. Eng.dwarf beans. 1 qt. plants from 100 to 150 feet of row. French "250 or 350 of row.

66 100 hills.

300 " or 250 feet of row. 10 lbs. to the acre: 1 oz. plants 150 feet of row.

Broccoli and Kale I oz. gives 2500 plants, and requires 40 square feet of ground.

Early sorts same as broccoli, and requires Cabbage. 60 square feet of ground. Canliffower. The same as cabbage. 1 oz. to 150 of row. 1 oz. gives 7000 plants, and requires 8 Carrot. Celery. square feet of ground. 1 oz. for 150 hills. Cucumber. 1 oz. sows a bed 16 feet square. Cress. 1 oz. gives 2000 plants. Egg Plant " req'i'es 80 ft. of ground Endive. 1 oz. 3000 Leek. - . . 1 oz. 2000 60 1 oz. 7000 " seed bed of 120 ft. Lettuce. Melon. 1 oz. for 120 hills. Nasturtium 1 oz. sows 25 feet of row. 200 Onion. 1 02. 200 Okra. 1 oz. Parsley. 1 oz. 200 Parsnip. 1 oz. 250 Peppers. 1 oz. gives 2500 plants. 1 quart sows 120 feet of row. Peas. 1 oz. to 50 hills. Pumpkin. Radish. 1 oz. to 100 feet. 1 oz. to 150 " of row. Salsify. 1 oz. to 200 Spinage. Squash. 1 oz. to 75 hills 1 oz. gives 2500 plants, requiring seed bed of 80 feet. Tomato. Turnip. 1 oz. to 2000 feet.

#### Table Showing the Number of Plants, Hills, or Trees Contained in an Acre at Epual Distances Apart. From 3 Inches up to 66 Feet.

Water melon, 1 oz. to 50 hills.

Distan				No. of		stance	Э			lo. of
apar	τ.			plants.	i	ipart.			$\mathbf{p}$	lants.
3 inches.	by.	3 iı	iches.	696,960	4	feet.	by	1	foot	10.890
4 "		4	6.6	392.040	4	+4		2	feet	5.445
6 "	+ 6	6	66	174.240	4	6.	• •	3	**	3,630
9	• •	9	4.6	77.440	4	6.6	* *	4	+ 4	2.722
1 foot	**	1	foot	43.560	41	/2 "	6.4	41/2	**	2.151
11/2 feet	• •	11/9	feet	19.360	5		4.4	1	foot	8.712
2	**	1	foot	21,780	5	6.	6.6	2	feet	4.356
2	• •	2	feet	10.890	5	+ 6	4.6	3	**	2.904
21/2 "	• •	215	6.	6.960	5	**	6 .	4	**	2.178
3	**	1 -	foot	14.520	-5	**	••	5	4.1	1.742
3		2	feet	7.260	51	/2	••	51/9	**	1.417
3 "	• •	3	**	4.840	6		6.4	6	••	1.210
31/2 "	• •	312	**	3.555	61,	§ ··		61/2		1.031

		tan			No. of plants.		Dist			No. of plants.
7	feet	by	7	feet	881	17	feet	by	17	150
8	**		-8	**	680	18	••		18	134
9	• •	**	9	**	537	19	•••	••	19	120
10	• •	**	10	+ 6	435	20			20	108
-11	**	+6	11	4.6	361	25	••	+6	$\tilde{25}$	69
12	••	**	12		302	30	••	••	30	48
13	• • •		13	•••	257	33	• •	44	33	40
14	• • •		14		222	40			40	27
15	6 .	+4	15	+ 6	193	50			50	17
16	**	+4	16	76	170	66			60	12
161	1/2"	**	161	5	160	66		**	66	10

Table Showing the Numtber of Seeds in one Pound, and Weight per Bushel.

NAME.	No. of seeds per pound.	No. of lbs., per bushel,
Wheat,	10,500	58 to 64
Barley.	15,400	48 to 56
Oats.	20,000	38 to 42
Rye.	23,000	56 to 60
Vetches.	8,500	60 to 63
Lentils.	8,200	58 to 60
Beans.	600 to 1,300	60 to 65
Peas,	1.800 to 2,000	60 to 65
Flax seed.	108.000	
Turnip seed.	155,000	50 to 60
Rape seed.	118,000	50 to 56
Mustard (white).	75,000	50 to 56
Cabbage seed.	128,000	57
Mangel-wurzel.		52 20 to 14
	24,600	20 to 24
Parsnip seed.	97,000	14
Carrot-seed.	257,000	9
Lucern-seed.	205.000	58 to 60
Clover (red).	249,600	60 to 63
" (white).	686,400	59 to 62
Rve-grass (perennial)	334,000	20 to 28
" (İtalian).	272,000	13 to 18
Sweet vernal grass.	923,000	8
Buck-wheat.	25.000	42 to 52

Table Showing Quantity per Acre when Planted in Rows or Drills.

Broom Corn.	1	to 11/2	bushel.	Onions.	4 to 5	pounds
Beans.	11/9	to 2	44	Carrots.	2 to 219	4.6
Peas.	11/9	to 2	4.6	Parsnips.	4 to 5	**
Pon-unte	1 -	to 2	66	Roote	1 to 6	**

# Table showing the quantity of seed required to the acre.

Designation.	Quantity of Seed.	Designation,		anti See	
Wheat.	11/4 to 2 bu.	Broom Corn.	1 to	11/2	bus.
Barley.	11/2 " 21/2 "	Potatoes.	5 ''	10	66
Oats.	2 " 4 " "	Timothy.	12 "	24	qts.
Rye.	1 " 2 "	Mustard.	8 "	20	7.6
Buckwheat.	34 " 11/3 "	Herd Grass.	12 "	16	6.6
Millet.	1 " 11/3 "	Flat Turnip.	2 "	3	lbs.
Corn.	14 " 1 "	Red Clover.	10 "	16	66
Beans.	1 " 2 "	White Clover.	3 "	4	6.6
Peas.	21/2 " 31/2 "	Blue Grass.	10 "	15	66
Hemp.	1 " 11/2 "	Orchard "	20 "	30	6.6
Flax.	1/2 " 2" "	Carrots.	4 "	5	6.6
Rice.	2 " 21/2 "	Parsnips.	6 "	8	64

# NUMBER OF YEARS SEEDS RETAIN THEIR VITALTY.

Vegetables.	У	ears	5.	Vegetables.		years	
Cucumber.	8	to	10	Asparagus.	2	to	3
Melon.	8	4.6	10	Beans.	2		3
Pumkin.	8	6.6	10	Carrots.	$\bar{2}$	**	3
Squash.		6.6	10	Celery.	$\bar{2}$	**	3
Brocoli.	855555438833333	6.6	6	Corn (on cob).	$\bar{2}$		3
Cauliflower.	5	64	ě.	Leek.	$-\tilde{2}$	**	3
Artichoke.	5	64	ĕ	Onion.	$\bar{2}$		3
Endive.	5	44	ĕ	Parsley.	$\bar{2}$		
Pea.	5	6.6	ĕ	Parsnip.	$\tilde{2}$	44	333
Radish.	Ä	6.6	5	Pepper.	5	44	3
Beets.	2	66	4	Tomato.	$\frac{2}{2}$		3
Cress	9	66	4	Egg Plant,	1		3
Lettuce.	9	6.	. 4	Egg Flam.	1		- ii
	ð	66	4	HERB	S.		
Mustard.	ð	4.	4				
Okra.	3	44	4	Anise.	3	to	+
Rhubarb.	3		4	Caraway.	2		
Spinach	3	**	4	Summer Savory.	1	6.0	2
Turnips.	3	**	5	Sage.	2	•••	3

# Amount of Seeds, Bulbs, etc., Required to Plant One Agre.

Barley,	21/2 bus.
Beans, bunch, in drills 21/2 feet	11/2 "
Beans, poles, $\lim_{n \to \infty} 4 \times 4$ feet	20 gts.
Beets, drills 21/2 feet	9 lbs.
Broom-corn in drills	
Cabbage in beds	12 oz.
Clover, large, red	16 lbs.
Clover, large, with timothy.	
Corn, sugar	10 ots.

Corn, field	8. qts.
Cucumbers in hills	8 7.
Grass, timothy with clover	6 "
Grass, timothy without clover	10 "
Grass, orchard 25 to	30
Grass, red-top 20 to	
Grass, blue	28 "
Grass, rye	20
Lawn orass	25 lbs.
Lawn grass	3 "
	0. 1
Onions in beds for sets	50 lbs.
Onions in rows for large bulbs	7 105.
Onions in rows for large bulbs	0 040
Pumpkins in hills 8×8 feet	2 qts.
Peas in drills, low varieties	2 bus.
Peas in drills, tall varieties 1 to	11/2
Peas, broadcast	9
Potatoes	8 "
Rye, broadcast	13/4 ''
Rye, drilled	11/2 "
Turnips in drills 2 feet	3 lbs.
Turnips, broadcast	3 "
Wheat in drills	114 bus.
Wheat, broadcast	13 11

Table showing the number of hills or plants on an acre of land, for any distance apart, from 10 inches to 6 feet—the lateral and longitudinal

distances being unequal,

	10 in.	12 in.	15 in	18 in	20 in.	2 ft.	$2\frac{1}{2}$ ft.	3 ft.	3½ ft	4 ft.
	62626									
12 "	52272	43560								
15 "	41817	34848	27878							
18 "	34848	29040	23232	19360						
	31363									
	26136									
21/2"	20908	16424	13939	11616	10454	8712	6969			
3_''	17424	14520	11616	9680	8711	7260				
31/2"	14935 13068	12446	9953	8197	7467	6223	4976			
4 ''	13068	10890	8712	7260	6534	5445				
41/2"	11616 10454	9680	7744	6453	5808		3872			
5 "	10454	8712					3484			
51/2"	9504	7920			4752		3168			
6 "	8712	7260	5808	4840	4356	3630	2904	2420	2074	1865

# TO PROTECT NEWLY PLANTED CORN.

To prevent the corn from being destroyed and eaten by chickens, birds, or insects before it grows through the surface of the soil, prepare the seed before planting by sprinkling a sufficient portion of coal tar, (procured at the gas manufactory), through it, stirring so that a portion

will adhere to each grain; then mix among the corn some ground plaster-of-Paris, which will prevent the tar from sticking to the fingers of those who drop the corn, and vegetation will be promoted thereby. The tar and plaster will not injure the corn so as to prevent its growing, by being kept some days after it is so mixed together.

#### TO PROTECT CORN STALKS FROM MICE.

Sprinkle from four to six bushels of dry white sand upon the root of the stalk before the thatch is put on. The sand is no detriment of the corn, and stacks thus dressed have remained without injury. So very effective is the remedy, that nests of dead young mice have been been found where the sand have been used, but not a live mouse could be seen.

## MEASURE OF AN ACRE PLOT.

Either of the following measure include about an acre plot.

3	by	531/8	Rods.	1 8	by	20	Rods.
4	66	40	66	9	66	177/8	6.6
5	66	32	4.6	10		16	+ 6
6	6+	$262_{3}$	6.6	11	**	14 6-11	4.6
7	6.6	22 6-7	"	12	+ 6	131/3	66
	12 R	ods 10 ft.	and 81/2 in	square	make	an Acre	

# Square Feet and Feet Square in Fractions of an Acre.

Fractions of an Acre.	Sq. Ft.	Ft. Sq.	Fractions of an Acre.	Sq. Ft.	Ft. Sq.
1-16	27221/2	521/2	1/2	21780	1471/2
1/8	5445	7334	1	43560	2081/4
<u>14</u>	10890	$1041/_{2}$	2	87120	2951/4
1/3	14520	$1201/_{2}$	3	130680	

# HILLS IN AN ACRE OF LAND.

			*****		
			Hills.		Hills.
40	feet	apart.	27 1	8 feet apart.	680
35 30 25	6.6	~66	35	6 " "	1210
30	6.6	66	48	5 "	1742
25	6.6	6.6	69	31/5" "	3556
20	66	6.6	108	3	4840
15	6.6	64	193	21/2** **	6969
12	66	_ 66	302	2	10890
10	6.6	66	435	1 " "	43560

# TO ESTIMATE GRAIN CROPS PER ACRE.

Frame together four light sticks, measuring exactly a foot square inside, and with this in one hand, walk into the field and select a spot of fair average yield, and lower the frame square over as many heads as it will inclose, and

shell out the heads thus enclosed carefully, and weigh the grain. It is fair to presume that the proportion will be the 43560th part of an acre's produce. To prove it go through the field and make ten or twenty similar calculations, and estimate by the mean of the whole number of results. It will certainly enable a farmer to make a closer calculation of what a field will produce than he can by guessing.

## Comparative Yield of Various Grains, Vegetables and Fruits.

	Lbs		Lbs.,
	per Acre.		per Acre.
Hops.	.442	Grass.	7,000
Wheat.	1,260	Carrots.	6.800
Barley.	1,600	Potatoes.	7,500
Oats.	1,840	Apples.	8,000
Peas.	1,920	Turnips.	8,420
Beans.	2,000	Cinque foil grass.	9,600
Plums.	2,000	Vetches, green.	9,800
Cherries.	2,000	Cabbage.	10,900
Onions.	2,800	Parsnips.	11,200
Hay.	4,000	Mangel Wurzel.	22,000
Pears.	5,000		

# CONTENTS OF FIELDS AND LOTS.

# To assist farmers in making an estimate of the amount of land in different fields.

220	feet	by	198	feet of	land.	е	quals.	. 1	acre.
440		"	99	••	66	• • • •	66	1	
110 60		6.	369 726	44	66	• • • • •	44	1	
120	4.4	4.	363	46	66		••	î	4.
240	6.6	••	1811/2	46	6.6		••	Ī	
200	44	6.	108 9	66	6.6		6.	1/2	••
100	66	66	$145_{10}^{2}$	**	66 .			1/3	
100	.,		$108_{12}^{9}$	••	••			1/4	

# A PRACTICAL RULE FOR LAYING PIPE

FOR	DRAIN	IING	LAND.	Dist	ance.
Soils.	De	epth o	of Pipe.		art.
Coarse, Gravel Sand.			6 inches,	 .60	
Light Sand with Grav	7el. 4	66	"	 . 50	44
Light Loam.	3	66	6 "	 . 33	6.6
Loam with Clay.	3	66	2 "		**
" Gravel.	3	66	3	 .27	• 6
Sandy Loam.	3	** !	9	 . 40	4+
Soft Clay.	2	44	) "	 . 21	4.
Stiff Clay.	2	**	3 "	 . 15	••

Greatest Fall of Rain is 2 inches per hour—54308.6 gallons per acre.

Showing Number of Acres drained by different sizes of tile, the rainfall being considered as equal to one-half inch in depth each 24 hours.

			616016	010 CI	CPOIL	cucre.	24 160	w/ ·s.		
R	ate of	Inclin	ation	1	1	ACRES	S DR.	AINE	D.	
F	eet to	one of	f rise.	2-in.  Tile.	3-in.  Tile.	4-in. Tile.	6-in. Tile.	8-in. Tile.	10-in. Tile.	12-in. Tile.
111111111111111111111111	foot	in 10 20 25 30 40 60 70 80 96 100 150 200 200 400 600 800 1.000	feet	6.6	18.9 13.0 11.4 10.9 9.4 8.4 7.6 6.9 6.5 6.1 5.7 4.5 3.9 3.5	26.8 24.0 21.9 19.0 17.0 15.6 14.5 13.4 12.6 11.9 9.5 8.2 7.5 6.9 5.9	66.2 61.5 53.3 47.7 43.4 39.9 37.2 35.0 33.1 26.6 222.8 20.4 16.5 14.8 13.3	126.4 109.6 98.0 90.0 83.0 77.0 72.5 69.2 56.0 48.0 43.4 38.2 34.6 30.1 28.0 21.2	190.5 170.4 156.0 144.4 135.0 127.0 120.6 97.3 83.9 74.4 65.5 60.3 54.0 48.6 41.9 37.2	269.0 246.0 228.1 213.0 200.5 154.4 132.5 117.0 90.7 81.6 74.0 65.0 56.0 47.0
1	66	2.000	44						30.8	40.8

Showing carrying capacity of different sizes of tile in Gals.

Carrying Capacity—Gallons per Minute.											
Size of pipes.		11/2 in. fall per 100 ft.	3 inch fall per 100 ft.	6 inch fall per 100 ft.	9 inch fall per 100 ft.	1 foot fall per 100 ft.	11/2 ft. fall per 100 ft.	2 foot fall per 100 ft.	3 foot fall per 100 ft.		
21/2	in.	14	20	28	34	40	49	55	68		
3		21	30	42	52	60	74	85	104		
3 4 5	4.4	36	52	76	92	108	132	148	184		
	+ 6	54	78	111	134	159	192	219	269		
6	6.6	84	120	169	206	240	294	338	414		
8	4.6	144	208	304	368	432	528	592	736		
9	4.4	232	330	470	570	660	810	930	1140		
10	4.4	267	378	563	655	803	926	1340	1613		
$\tilde{1}\tilde{2}$	4.6	470	680	960	1160	1360	1670	1920	2350		
15	6.6	830	1180	1680	2040	2370	2920	3340	4100		
18	66 .	1300	1850	2630					6470		
	1.44				3200	3740	4600	5270			
20	44	1760	2450	3450	4180	4860	5980	6850	8410		
24		3000	4152	5871	7202	18303	10021	11743	14466		

# THE NUMBER OF RAILS, RIDERS AND STAKES REQUIRED FOR EVERY TEN RODS OF ZIGZAG FENCE.

of of	don	of el.	Number	r of Ra n 10 Ro	of	of gle).	
Length Rail.	Deflect from ri	Length	Rails nigh.	Rails nigh.	n Rails igh.	imber Stakes.	mber ers (sing
Ft.	Ft.	Ft.	Five	Six	Seve	Ŋ	Ride
12	6 7	8	103 83	123	144 116	42 34	21 17
161/2	8	12	83 69	84	95	28	14

For longer distances than 10 rods the proper number of rails, etc., may be computed by multiplying. For instance: If 50 rods of fence, multiply the above number by 5; if for 100, multiply by 10, etc. The like rule will apply to the next.

# THE NUMBER OF RAILS AND POSTS REQUIRED TO EACH TEN RODS OF POST AND RAIL STRAIGHT FENCE.

to .	of 1.	of	f	Number of Rails for each 10 Rods.						
Length Rail	Length	umber o Panels.	Number of Posts.	e Rails Iigh.	Rails Iigh.	n Rails Iigh.	it Rails Tigh.			
Ft.	Ft.	Z	Z	Fiv	Six	Seve	Eigh			
10 12	8	205/8	21	103	123	144 116	165 133			
14 161/2	12 141/ <sub>2</sub>	133/4 111/3	14 12	83 69 57	99 84 69	116 95 81	165 133 109 93			

# Contents of Bins and Granaries.

Contents of Bins and Granaries. (Continued).

					_	(00,000	meacu !	•
Width	5 Ft	. high.	6 Ft	. high.	7 Ft.	high.	8 Ft.	high
Length in feet.	Sti' k'n.	Heap.	Sti'- k'n.	Heap.	Sti'- k'n.	Неар.	Sti'- k'n.	He'p.
5 × 5 5 * 6 5 * 7 5 * 8 5 * 9 5 * 11 6 * 6 6 * 7 6 * 8 6 * 10 6 * 11 7 * 12 8 * 8 8 * 9 9 * 10 9 * 11 9 * 11 9 * 11 10 * 11 11 * 11	100 120 130 130 130 130 130 130 130 130 130 13	157½ 180 202½ 202½ 225 247½ 270 205¾ 257¾ 269¼ 308½ 318¼ 347¼ 321½ 353½ 385¾ 385¾ 385¾ 342¼ 344¼	173 ½ 202½ 201½ 200½ 231½ 260¼ 236¼ 236¼ 236¼ 236¼ 405 347½ 371½ 462₹ 385¼ 462₹ 580½ 580½ 666¼ 669¼ 669¼ 669¼ 669¼ 669¼ 669¼ 669	1383 162 1851 1851 1852 2081 2185 2277 189 270 297 324 246 247 308 270 317 317 416 416 416 416 416 416 416 416 416 416	275 <sup>2</sup> 315 <sup>4</sup> 335 <sup>4</sup> 339 <sup>2</sup> 433 <sup>1</sup> 472 <sup>2</sup> 393 <sup>2</sup> 450 45 506 <sup>1</sup> 560 <sup>1</sup> 560 <sup>2</sup> 618 <sup>2</sup> 660 <sup>2</sup> 680 <sup>2</sup> 742 <sup>1</sup> 810	220½ 252 283½ 346½ 378 328 324 364 364 396 432 405¼ 4450 495 540 540 540 540 540 540 540 540 540 54	411 ½ 4623 565½ 667½ 578½ 6366 634½ 6423 707½ 777½ 777½ 9253	3294 4114 4525 4982 4623 4623 5144 5653 6624 66783 7403

This table of "Stricken and Heap" bushels is given to the nearest quarter and can be used for deeper bins, than that employed in the table:—Take the contents of half the depth and multiply by 2.

# CAPACITY OF BOXES.

A box 16 inches square and 8.4 inches deep, will contain 1 bushel.

A box 16 inches by 8.4 inches wide, and 8 inches deep will contains 1/2 bushel.

A box 8 inches by 8.4 inches wide, and 8 inches deep will contain 1 peek.

A box 8 inches by 8 inches square, and 4.2 inches deep. will contain 1 gallon.

A box 7 inches by 4 inches wide, and 4.8 inches deep, will

contain 1/2 gallon.

A box 4 inches by 4 inches square and 4.2 inches deep, will contain 1 quart.

A box 24 by 16 inches square, and 28 inches deep will contain a barrel (5 bushels shelled corn).

A box 24 by 16 inches square, and 14 inches deep will

contain 1/2 a barrel.

A box 26 by 161/2 inches square, and 8 inches deep, will

contain 1 bushel.

A box 4 feet by 7 inches long, 2 feet 4 inches wide, 2 feet 4 inches deep, holds 20 bushels.

#### CAPACITY OF A FREIGHT CAR.

A load is nominally 10 tons of 20,000 pounds. The following can be carried: whiskey, 70 bbls., salt, 70 bbls., llme, 70 bbls.; flour, 90 bbls.; eggs, 130 to160 bbls.; flour, 200 sacks; wood 6 cords; cattle, 18 to 20 head; hogs, 50 to 60; sheep, 80 to 100; lumber, 6,000 feet; barley, 400 bushels; wheat, 340 bushels; flax seed, 360 bushels; apples, 370 bushels; corn, 400 bushels; Irish potatoes, 430 bushels; cats, 680 bushels; bran, 1.000 bushels; butter, 20.000 pounds; 400 bushels of barley; 300 bushels of sweet potatoes; 200 kegs of nails.

#### TO MEASURE GRAIN IN BINS.

Multiply the length of the bin in inches by the width in inches, and that by the height in inches and divide by 2150 for struck bushels, and by 2748 for heaped bushels. The quotient will be the number of bushels contained in the bins, or-

# TO MEASURE GRAIN IN THE GRANARY.

Divide the cubic feet by 56, multiply by 45, and the result will be struck measure in bushels.

# TO MEASURE CORN IN CRIB.

Multiply the length, breadth and height together, in feet, to obtain the cubic feet; multiply this product by 4, and strike off the right figure; and the result will be shelled bushels, nearly,

# TO MEASURE CORN.

IN COB.—Two heaping bushels of corn on the cob will make 1 struck bushel of shelled corn. Some claim that 1 and ½ bushels of ear will make 1 bushel of shelled corn. Much will depend upon the kind of corn, shape of the ear, size of the cob, etc.

IN CRIB. - To measure corn in a crib, multiply the length of the crib in inches by the width in inches, and that by the height of the corn in the crib in inches and divide the product by 2,748 and the quotient will be the number of heaped bushels of ears. If the crib flares at the sides, measure the width at the top and also at the bottom, add the two sums together, and divide by 2, which will give the mean width.

#### MEASUREMENT OF HAY.

The only method exact of measuring hay is to weigh it, but the rules given below will be found sufficient for ordinary practical purposes:

To Find the Number of Tons of Meadow Hay in Windrows.—Multiply together the length, breadth and height, in yards, and divide the product by 25. The quotient will be the number of tons in the windrow.

To Find the Number of Tons of Hay in a Mow.--Multiply together the length, height and width, in yards, and divide by 15 if the hay be well packed. If the mow be shallow, and the hay recently placed therein, divide by 18, and by any number from 15 to 18, according as the hay is well packed.

To Find the Number of Tons of Hay in Square or Long Stacks.—Multiply the length of the base in yards by the width in yards, and that by half the height in yards, and divide by 15.

To Find the Number of Tons of Hay in a Load.—Multiply together the length, width and height, in yards, and divide the product by 20.

To ascertain the value of a given number of pounds of hay, straw, or other commodity sold by the ton, at a given price per ton, multiply the number of pounds by 1/2 the price per ton, and point off three figures from the right. The result will be the price of the article.

A ton is 100 cubic feet in the mow; that is, when it has settled down and becomes solid. A truss of Hay is, new, 60 pounds, old, 50 pounds, straw, 40 pounds. A load of hay is 36 trusses. A bale of hay is 300 pounds.

# TO MEASURE CISTERNS AND CASKS.

Circular Cisterns.—To ascertain the contents of circular cisterns, multiply the square of the diameter in feet by the depth in feet and that product by  $\frac{373}{4000}$  for the contents in hogsheads, or by  $\frac{373}{2000}$  for barrels, or 478 for the contents in gallons.

Square Cisterns.—To ascertain the contents of square cisterns multiply the width in feet by the length in feet, and that by the depth in feet, and that again by  $\frac{19}{160}$  for hogsheads, or  $\frac{1}{160}$  for barrels, or  $7\frac{4}{100}$  for gallons. Another and simple method is to multiply together the length,

width, and depth, in inches, and divide by 231, which will give the contents in gallons.

Cask Gauging.—To measure the contents of cylindrical vessels, multiply the square of the diameter in inches by 34, and that by the height in inches, and point off four figures. The result will be the contents in, or capacity, in wine gallons and decimals of a gallon. For beer gallons multiply by 28 instead of 34. If the cask be only partially filled, multiply by the height of the liquid instead of the height of the eask, to ascertain the actual contents. In ascertaining the diameter, measure the diameter at the bung and at the head, add together, and divide by 2 for the mean diameter.

#### TO COMPUTE THE WEIGHT OF CATTLE.

Multiply the girth in inches, immediately back of the shoulders, by the length in inches from the square of the buttock to the point of the shoulder blade, and divide the product by 144, which will give the number of superficial feet. If the animal has a girth of from 3 to 5 feet, multiply the number of superficial feet by 16, which will give the weight of the animal. If the girth is from 5 to 7 feet, multiply by 23, and if from 7 to 9 feet, multiply by 31. If less than 3 feet girth, as in the case of small calves, hogs, sheep, etc., multiply by 11. Of course many circumstances, such as the build of the animal, mode of fattening, condition, breed, etc., will influence the weight, but the above will be found approximately correct.

# TO TELL THE AGE OF CATTLE.

A cows horn is generally supposed to furnish a correct indication of the age of the animal. This is not always true. However, for ordinary purposes, the following will

be found approximately correct.

At two years of age a circle of thick matter begins to form on the animal's horns, which becomes clearly defined at three years of age, when another circle or ring begins to form, and so on year after year. Its age, then, can be determined by counting the number of rings and adding two to their number. The rings on the bulls horns do not show themselves until he is five years old, so to the number of rings we must add five to arrive at his age. Unless the rings are clear and distinct this rule will not apply, Besides, dealers sometimes file off some of the rings of old cattle to make them appear younger.

# AGE OF SHEEP AND GOATS.

At 1 year old they have eight front teeth of uniform size. At 2 years of age the two middle ones are supplanted by two large ones. At three a small tooth appears on each side. At four there are six large teeth. At five all the front teeth are large and at six the whole begins to get large.

#### WEIGHT OF A CUBIC FOOT

of various substances, from which the bulk of a load of one ton may be easily calculated:

lbs.	ibs.
Cast Iron450	Common Soil, compact, about 124
Water 62	Clay, about
White Oak 52	Brick, about125
Loose Earth, about 95	Stone, about

Legal Weights of Grain, Seed, etc., in Different States.

ARTICLES.	N. Y.	Ohio.	Penn.	Ind.	Wis.	Iowa.	1111.	Mich.	Conn.	Mass.	R. I.	Ky.	N. J.	Vt.	Mo.	Canada
Wheat, lb.,							60						60			
Rye.							54					56	56	56	56	56
Corn.							56						56	56	52	56
Oats.	32	32	32	32			32		28	30		33	30	32	M	34
Barley.		48		48	48	48	44		45			48		46		48
Buckwheat.	48		48	50			40	42		46		52		46		48
Clover seed.		64		60	60	60		60					64		M	60
Timothy seed.		62		45		45		M		M		45				48
Flax seed.		56		56		56		M		M		56	55		M	56
Hemp seed.	44			44		44										1
Blue grass seed.				14		14										
Apples, dried.	22	25			28	24		28								22
Peaches, "		33			28	33		28								22
Coarse salt.		50		50		50				70		50				56
Fine salt.			83			50				70		50			50	56
Potatoes.	60		1	60		66			60		60			60		1
Peas.	60		1				i			60						60
Beans.		56		60		60				60		60				60
Castor beans.	46			46		46										
Onions.	57	1	1	57		57				50	50		52			1
Corn meal.	1	1		50	1		1				50					

The letter "M" shows the sale in that State is by measure instead of weight.

To reduce cubic feet to bushels, struck measure, divide the cubic feet by 56 and multiply by 45.

# VALUE OF FOOD FOR DOMESTIC ANIMALS.

The figures below give the comparative number of pounds of each substance to equal in effect that of any standard food—as, for instance, that of hay.

Good hay, to					fbs.
Good clover h	ay will give s	ame effe	ct by the	use of. 95	66
Rye Straw	"	6.6	66	355	6.6
Oat Straw	66	66	66	220	6.6
Potatoos	66	66	66	195	6.6

Carrots will	give same	effect by	the use of	280	The
Beets	givo nume	","	"	346	66
Ruta Bagas	41	44	+ 6	262	66
Wheat	66	44	66	43	+6
Peas	44 .	4.6	66	44	66
Beans	44	, 44	66	46	66
Rye	66	66	66	49	+ 6
Barley	66	4.6	44	51	66
Indian Corn	"	66	46	56	6.6
Oats	44	6.6	44	59	6.6
Buckwheat	46	66	44	64	6.6
Oil Cake	66	6.6	6.6	64	6.

#### NUTRITIVE QUALITIES OF FODDER.

The proportion of nutritive matter in 100 pounds of the following substances is as follows:

2020 1120 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Flesh Formers.	Fat Formers.
Clover Hayin pounds,	131/2	30
Timothy	$93\overline{4}$	4834
Corn	10	68
Oats	12	61
Wheat Bran	14	50
Shorts	10	56
Buckwheat Bran	$51/_{2}$	48
Potatoes		21
Apples	1/2	14
Mangels	1	9_

The whole of these amounts may not be digestible, but they serve to give a good idea of their relative value.

# CONSUMPTION OF HAY.

The hay consumed by different animals does not vary greatly from three pounds daily for each hundred pounds weight of the animals. The following table is the result of various experiments by different persons, and will be useful for farmers who wish to determine by calculation beforehand, how their hay will hold out for the winter; 500 cubic feet of timothy hay, in a full bay being about one ton.

Working Horses,	3.08 fbs	Steers.	2.84 Tbs
Working Oxen,	2.40 ''	Dry Cows,	2.42 "
Milk Cows (Boussingault's)	2.25 "	Pigs (Estima	ì-
Milk cows (Lincoln's),	2.40 "	ted),	3.00 "
Young growing cattle,	3.08 ''	Sheep,	3.00 ''

All the articles enumerated in these food tables are estimated as of good quality. If the fodder be of poor quality, more must be allowed.

#### RELATIVE VALUE OF DIFFERENT FOODS IN STOCK RAISING.

To produce the same effect as 100 pounds of hay will require of the following articles the number of pounds opposite ageb.

reduire or and resident	CHESTOSCO CITO ILLUMINOCE CE	Lo cerron
opposite each:		
Beets, white	669	pounds.
Turnips	469	- "
Rye straw	429	6.6
Clover, red, uncured	373	6.6
Clover, red, dry	88	66
Carrots	371	66
Carrot leaves	135	46
	368.5	6.6
Mangolds		64
Potatoes	350	
Oat straw	317	4.6
Lucerne	89	+ 6
Buckwheat	78.5	, 4
Corn	62.5	* **
Oats	59	66
Barley	58	66
Rye	53.5	6.6
Wheat	44.5	
Oilcake, linseed	43	· =
Peas, dry	37.5	6;
Beans	28	• 1

# FOOD FOR POULTRY.

The table shows the percentage of nutriment in different kinds of food for poultry.

There is in Every 100 Parts by Weight of—	Flesh-form Material, vi Gluten, et	Warm giving Fatten Materi viz Fat or Oil.	and ing al	Bone-making Material, or Mineral sub- stance.	Husk, or Fibre.	Water.
Beans and Peas	25	2	48	2	8	15
Oatmeal	18	$\begin{array}{c} 2 \\ 6 \\ 6 \end{array}$	63	$\frac{2}{2}$	2	9
Middlings Thirds, or Fine Sharps	18	6	53		4	14
Oats	15	6	47	$\frac{2}{2}$	20	10
Wheat	12	3	70	2	1	12
Buckwheat	12	6	58	11/2	11	111/2
Barley	11	6 3 6 2 8	60	11/ <sub>2</sub> 2 1	14	111/ <sub>2</sub> 11
Indian Corn	11		65	1	5	10
Hempseed	10	21	45	2	14	8
Rice	7	A trace		A trace		13
Potatoes	61/2		41	2		501/2
Milk	41/2	3	5	3/4		863/4

# FOOD FOR SHEEP.

The table shows the number of pounds, live weight, and the number of pounds of wool and of tallow, produced by 1,000 pounds of each of the articles named, when used as food for sheep.

		•	
KIND OF FOOD.	Increase in weight, Ibs.	Wool pro-	Tallow pro-
Barley Buckwheat Corn Meal, wet Mangel-wurzel, raw Oats Peas Potatoes, raw, with salt Potatoes, raw, without salt Rye, with sait Rye, without salt Wheat	136 120 129 381/2 146 134 461/2 44 133 90 155	111/2 10 131/2 51/4 10 141/2 61/2 14 12	60 33 171/2 61/2 421/2 41 121/2 111/2 35 43 591/2

# CORN AND HOGS.

A bushel of corn will make 10½ pounds of pork gross.

W	hen co	rn co	sts	P	ork c	osts		
			bushel.				pound.	
$\dot{2}\dot{5}$		4.6		$\frac{2}{3}$			16	
35 42		• •	16	4 5	••	4.	.6	
50	**	••	**	š	+ 5		+ 6	
60 65	66	- 4.		7	**		• • •	
00				0				

# AGES OF ANIMALS.

AUE	BUFAL	VIMALS.		
Whales, estimated,	1.000 Yrs.	Cow,	20	Yrs.
Elephant,	400 "	Deer,	20	6.6
Swan,	300 ''	Rhinoceros,	/ 20	6.5
Tortoise.	100 "	Swine,	20	66
Eagle,	100 "	Wolf,	20	6.6
Raven,	100 "	Cat	15	6.6
Camel,	100 "	Fox.	. 15	6.6
Lion,	70 "	Dog,	10	6.6
Porpoise,	30 "	Sheep,	10	66
Horse,	20 "	Rabbit.	7	6.6
Bear.	20 ''	Squirrel.	7	4.6

Careful observations have shown the following to be about the average growth in twelve years, of several varieties of hard wood, when planted in groves and cultivated:

	Inches diameter.	Feet high.
White Maple.	12	30
Ash, Leaf Maple or Box Elder,	12	20
White Willow,	18	35
Lombardy Poplar,	10	.40
Blue and White Ash,	10	25
Black Walnut, and Butternut.	10	20

# NUTRITION IN FOOD.

The following is "Boussingault's Scale of Nutritive Equivalents," and shows how many parts of the various articles of food in common use it takes to be equal in nutrition to 100 parts of wheat flour:

Wheat Flour,	100	Rye,	111
Wheat.	107	Rice,	177
Barley Meal,	119	Buckwheat,	108
Barley,	130	Maize,	130
White Haricots.	56	Horse Beans,	44
Lentils,	57	Peas,	67
White, Cabbage,	810	Potatoes,	313
Dried do at 212°.	83	Carrots,	777
Oats,	117.	Turnips,	1335

# WEIGHTS (MISCELLANEOUS).

Bbl. flour weighs	196	pounds.
Salt	280	**
Beef	200	+6
Pork	200	"
Fish	200	• 6
Keg Powder equals	25	4.6
Stone of lead or Iron equals	14	• 6
Pig of " equals	21	1/2 stone.
1 bush, of Oats		pounds.
1 " Barley .	48	**
1 " Corn, Rye, or flax seed	48 56	4.6
1 " Blue grass	14	. 5
1 " Castor Beans	46	+6
1 " Hemp seed	44	**
1 " (Wheat, beans, clover-	co	4.6
seed, peas, or potatoes	60	* 6
1 " Timothy seed	45	4.5
1 " Onions	57	**
1 " Apples, or dried peaches,	28	4.6
1 " Salt	50	64
A sack of wool	- 308	6.6
A pack " " (for a horse)	240	66

A bale of cotton is 400 pounds, but it is put up in different states varying from 280 to 720 pounds. Sea Island cotton is put up in sacks of 300 pounds.

#### AGES ATTAINED BY BIRDS.

AULS AI.	1 21	T 71 -	D DI DINDS	•	
Blackbird lives	13	yrs.	Parrot lives	65	yrs.
Blackcap lives	15		Partridge lives	15	66
Canary lives	24	6.6	Peacock lives	24	66
Crane lives	27	6.6	Pelican lives	58	6.6
Crow lives	100	16	Pheasant lives	15	66
Eagle lives	100	6.6	Pigeon lives	20	66
Fowl (common) lives	12	6.6	Raven lives	100	6.6
Goldfinch lives	15	66	Robin lives	12	66
Goose lives	50	66	Skylark lives	30	6.6
Heron lives	60	6.6	Sparrow Hawk lives	40	66
Lark lives ·	18	6.6	Swan lives	100	6.6
Linnet lives.	$\tilde{23}$	6.6	Thrush lives	10	6.6
Nightingale lives	<b>1</b> 8	6.6	Wren lives	-š	6.6

# FRESH WATER.

The component parts, by weight and measure, is—Oxygen 88.9 weight, and 1 by measure; hydrogen 11.1 weight, and 2 by measure. One cubic inch of distilled water at its maximum density, 39.83, the barometer 30 inches, weighs 252.7 grains. A cubic foot weighs 62.5 pounds.

# AMOUNT OF OIL IN SEEDS.

Kinds of Seed. Rapeseed Sweet Almond Turnip seed White mustard Bitter Almond	55 47 45 37 37	Oats Clover hay Wheat bran Oat-straw Meadow hay	61/2 5 4 4 31/2
White mustard	37	Oat-straw	4 31/2
Hempseed Linseed		Wheat-straw Wheat flour	3 3
Indian corn		Barley	21/2

The English Quarter, at which wheat is quoted in the English reports, is 560 pounds, or 14 of the ton gross weight of 2,240 lbs. The English legal bushel is 70 pounds, and consequently 8 of those bushels is a quarter—equal to 91/2 of our statue bushels of 60 pounds.

#### HOUSEHOLD WEIGHTS AND MEASURES.

1 Teaspoonful equals 1 dram.

1 dessertspoonful equal 2 teaspoonfuls, or 2 drams.

1 tablespoonful equals 2 dessertspoonfuls, or 4 teaspoonfuls.

2 tablespoonfuls equal 8 teaspoonfuls, or 1 ounce.

1 common size wineglassful equal 2 ounces, or 1/2 gill. A tea cup is estimated to hold 4 fluid ounces, or 1 gill.

- 1 pound of wheat is equal to about 1 quart.
- 1 pound and 2 ounces of Indian meal is equal to 1 quart.

1 pound of soft butter is equal to about 1 pint.
1 pound of sugar is equal to about 1 pint.

# TOWNSHIP PLAT.

7	ownshipRange									
	County,									
			NO	RTH		<del></del>	7			
	- 6	- 5	4	3	2	-ii				
	7	8	- 9	10	- 11	12				
					: : :		1			
Z	-18	17	16	15	14	13	LS			
WEST	19	20	21	22	23	24	EAST			
	10	20		- 22		4=				
	30	29	- 28	27	26	- 25				
×	31	32	33	34	35	36				
			003	TOTAL			1			

SOUTH

\*School section.

A township is 6 miles square = 36 sections. A section "1" = 640 acres.  $1_4$ " = 160 "  $1_4$ " = 40 "

Hence a township contains 23,040 acres. The smallest tract of land sold by the government is a "quarter-quarter section," which contains 40 acres. The sections are numbered from 1 to 36 commencing at the north-east corner.

Any citizen (or foreigner who has declared his intention to become one), who has actually settled upon an unappropriated quarter section (160 acres), and has erected a dwelling-house thereon, acquires the right of "pre-emption," that is, the right to purchase that 160 acre plot at the minimum price, though he had not located the tract before his settlement. He is permitted to take up, without payment of any price, except certain fees, 160 acres of \$1.25 land, or 80 acres of \$2.50 land, as a homestead. But the patent or deed will not be issued until he has resided on it for five years. The "patent" or deed is issued by the U.S. Land Commissioner.

#### THE CENTER OF POPULATION.

The centre of population of the United States is stedily moving westward, at the rate of fifty miles every ten years. The following is the centre point at each census:

1790 miles east of Baltimore. "west of Baltimore.

1800 18 1810 40 north-west of Wasnington.

" north of Woodstock, Va 1820 16

1830 " west by south-west Moorefield, W. Va.
" west of Clarksburg W. Va. 19

1840 16 1850 23 66 south-east Parkersburg, W. Va.

" south of Chillicothe, O. 1860  $\bar{20}$ 

" east by north of Cincinnati. 1870 48 " west by south of Cincinnati. 1880 8

# POWER OF AN ORDINARY MAN.

1 man can raise 10 pounds, 10 feet, in a second, 10 hours a day.

1 man can raise 100 pounds 1 foot.

1 man can draw on a level 640 pounds.

A man can press with hands equal to 110 pounds. A man's force, drawing horizontally, 110 pounds. A man can lift with both hands 236 pounds.

A man can support on his shoulders 330 pounds. 5 men working 10 hours a day are equal to 1 horse working 8 hours.

3 men carrying 100 pounds each will ascend a hill quicker than 1 horse carrying 300 pounds.

A man's strength is greater in rassing a weight when his own weight is to that of his load as four is to three.

# POWER OF A HORSE.

1 horse can raise 150 pounds 220 feet high in a minute: 8 hours a day. 1 horse-power is reckoned at from 30,000 to 36,000 pounds,

raised 1 foot high per minute.

horse's force drawing horizontally is estimated at 770 pounds. 1 horse can draw on a level 4480 pounds, -2 tons—equal to

7 men.

#### FORCE REQUISITE TO MOVE A BODY.

A stone along a rough chiseled floor require's 2/3 of its weight. The same on rollers, 1-32.

A stone along a wooden floor, 3-5 of its weight. The same on rollers 1-40.

# DISTANCE IN FEET GONE BY IN A SECOND.

A man walking, 4; a horse, harnessed, 12; a ship, 14; a steamship, 18; a reindeer on ice, 26; a race horse, 43; a hare, 88; a locomotive engine, 117; a 24 pound cannon ball, 1,300; the moon, 3,300; the earth, 99,733; an eagle, 117; a hawk, 50; a crow, 36.

The electric telegraph, 1.520.640.000, or more than eleven

times around the world.

A swift bird would be 3 weeks in flying round the world. Light travels about 192,000 miles in a second.

Light could pass round the earth in the 18th of a second.

#### SOUND.

Sound	passes	through air	in	a	${\bf second}$			1.130 4.900	
66	6.6	along water Cast-Iron						11.090	
6.6	44	Steel						17.000	
66	66	Glass						18.000	
6.6	6.6	Wood				4636	to	17.000	6.5

Cold air conducts sound better than warm.

# MEASURES OF ROCK AND EARTH.

25	cubic	feet	of sand equal	1 ton.
18	66	6.6	Earth	1 "
17	66	66	Clay	1 "
13	66	66	Quartz, unbroken in lode	1 "
18	64	6.6	Gravel or earth before digging	equals 27
017	hia fo	at wil	on due	

20 cubic feet of quartz, broken (of ordinary fineness from the lode), equals one ton, contract measurement.

# RAILWAY SIGNAL CODE.

One whistle signifies "down brakes," Two whistles signify "off brakes," Three whistles signify "back up," Continued whistles signify "danger." Rapid short whistles "a cattle alarm." A sweeping parting of the hands on the level with the eyes, signifies "go ahead." Downward motion of the hands with extended arms, signifies "stop." Beckoning motion of one hand, signifies "back." Red flag waved up the track, signifies "danger." Red flag stuck up by the roadside, signifies "danger." Red flag stack up by the roadside, signifies "danger ahead." Red flag carried on a locomotive, signifies "an engine following." Red flag hoisted at a station, is a signal to "stop." Lanterns at night raised and lowered vertically, is a signal to "start." Lanterns swung at right angles across the track, means "stop." Lanterns swung in a circle, signifies "back the train."

#### REMARKS ON USING FILES.

A new file should always be used with a light pressure on the work till the needle-like points of the teeth are worn away; after this, a much heavier pressure may be used with much less danger of breaking off the teeth at their base. Many new files are violently diminished half their efficiency by a few careless strokes when first applied to the work.

Do not use a new file on the chilled and gritty skin of castings, or on a weld where borax or any vitreous fluxes have been employed—no file can endure such usage.

Every filer should keep a worn file with which first to attack the rough, gritty or oxy dized surface of iron work, and thereby pave the way for a more efficient work with his sharp files. A piece of gritty or chilled casting that would rapidly destroy the cutting qualities of a new file, would produce scarcely any damaging effect to a worn one. In filing steel, better results can generally be obtained

In fining steel, better results can generally be obtained by using files of a grade not coarser than "2d cut;" finer grades being employed according to the finish and delicacy

of the work under manipulation.

Parties using files should always seek to discover the fitness or adaptibility of cut and form of files especially suited to their work. No one should expect the best results from a file on brass or spelter which was intended for use on iron or steel.

#### SHRINKAGE OF CASTINGS.

Iron, Small cylinders.	=	1-16 in.	per foot.
ripes	= '	1/8	
" Girders, Beams, etc.	=	18 "	in 15 Ins.
" Large cylinder the contracti	on		
" of diameter at top	=	1-16 "	per foot.
" Ditto at bottom	=	1/2 "	-46 46
" in length	=	1/2 " 1/8 "	in 16 Ins.
Brass, thin	=	1/8 "	in 9 "
" thick	=	1/2 "	in 10 "
Zine	=	5-16 "	in a foot.
Lead	=	5-16 "	in " "
Copper	=	3-16 ''	in " "
Bismuth	=	5-32 "	in " "

# SPEED OF SAWS.

To ascertain the proper number of revolutions per minute of any size saw, divide 36.000 by the diameter of the saw in inches, thus -36.000+60=600, the number of revolutions a 60 inch saw should make.

WEIGHT OF GRINDSTONES.—RULE:—Square the diameter (in inches) multiply by thickness (in inches); then by the decimal .06363; the product will be the weight of the stone in pounds.

#### TO ASCERTAIN THE DEGREE OF HEAT OF STEEL.

Steel becomes a ve	ry faint yellow at	(Fahr), 430°
	Straw color	450
	Full yellow	470
	Brown	490
	Brown with purple	
	Purple	530
	Blue	550
	Full blue	560
	Dark blue verging o	

# AVERAGE OF THE LINEAL EXPANSION OF A FEW METALS FROM 32° to 212°.

	ncrease th at			ased leng at 212°	gth
Zinc sheet 1	part in	340	Iron 1	part in	812
" cast	- 66	322	Antimony	- 44	923
Lead	66	351	Palladium	4.6	1000
Tin pure	66	403	Platinum	66	1167
" impure	66	516	Glass	66	1160
Silver		524	Marble	6.6	2833
Copper	4.6	581	Iron soft	66	818
Brass	66	584	Iron cast	66	900
Gold	+ 6	682	Steel tempere	d. "	806
Bismuth	4.6	719	Steel	"	926

# Quantity of water that will flow through a pipe 500 feet long in 24 hours, with a fall of 10 feet.

3/8 1/2	inches	bore	576 1,150	gallons.
5/8 3/4 1	66	66	2,040	66
3/4	4.6	. 6	3,200	6.6
1 <sup>T</sup>		6.6	6,624	66
11/4	6.6	4.6	10,000	46

# METAL IN THEIR PROBABLE ORDER OF THEIR HARDNESS.

Mercury, Sodium, Potassium, Lead, Zinc, Tin, Antimony, Gold. Silver, Cadmium, Bismuth, Tellurium, Copper, Copper and Zinc, (Brass) Platinum, Copper and Tin, (gun metal) Palladium, Iron, Cobalt. Nickel, Crude Iron, (grey) Steel, (soft) Steel, (hardened) Manganese, Titanium, Crude Iron, (white) Chromium, Rhodium, Iridium, Osminum, Hardest steel varying from white iron to top of list.

# The following Table Represents the pressure in pounds on the square inch at a given depth of water.

20	Feet		Ths.		Feet	_				521/4 lbs.
30	- 66	1234	"	80	**	3434	44	130	"	561/2 "
40	4.6	171/4	J6 6	90	66	39	66	140	66	603/4 ''
50	**	213/4	6.6	100	66	431/2	**	150	- 6.6	651/4 ''
-60	4.6	2614	66	110	66	4734	+6			

#### SOLDERS.

For lead, one of tin and one and one-half of lead.

For tin, one of tin and two of lead.

For pewter, two of tin and one of lead.

For brazing (hardest), three of copper and one of zinc. For brazing (hard), one of copper and one of zinc.

For brazing (soft), one of tin, four of copper, and three of

zinc; or, two of tin and one of antimony.

For silver (hardest), four of fine silver, and one of copper. For silver (hard), three of silver one part brass wire. For silver (softest), two of silver and one of brass wire.

For gold (hardest), four of copper seven of silver and eighty-nine of gold.

For gold (hard), sixty-six of copper and thirty-four of

ZIIIC

For gold (soft), sixty-six of tin and thirty-four of lead. For iron, sixty-six of copper, 33 of zinc and one of antimony.

For copper, fifty-three of copper and forty-seven of tin. For steel, thirteen of copper, five of zinc and eighty-two of silver.

For brass, forty-seven of copper forty-seven of zinc.

#### FLUXES FOR SOLDERING OR WELDING.

For iron or steel, borax or sal-ammoniac,

For tinned iron, resin or chloride of zinc. For copper and brass, sal-ammoniac or chloride of zinc.

For zinc, chloride of zinc.

For lead, tallow or resin.

For lead and tin pipes, resin and sweet oil.

# ACTUAL HORSE-POWER OF ENGINES.

RULE:—Multiply the area of the piston by the pressure per square inch; the product by the speed of the piston per minute, equals the force in pounds; this last divided by 33.000 equals the actual horse-power, including the friction.

SIMPLE RULE TO ASCERTAIN HORSE-POWER OF STEAM ENGINE.—Area of cylinder in inches multiply by pounds of steam in boiler, less 20 per cent off, the remainder by speed of piston in feet per minute; divide the product by 33.000

Thus: engine 20-inch cylinder (area 314 inches), boiler pressure 80 pounds, less 20 per cent off=64 pounds, speed of piston 250 feet per minute.

Then:  $314 \times 64 \times 250 \div 33.000 = 152 \text{ H. P.}$ 

# EASY RULE FOR FINDING THE AREA OF A CIRCLE.

A short and easy method of finding the area of a circle, is to multiply the square of the diameter by 7 and divide by 9, and you will have the area (nearly). This rule does

not give it exact; it falls a little short, but is near enough for all ordinary purposes.

To find the circumference when the diameter is given.— Multiply the diameter by 22 and divide by 7, and you will have the circumference (nearly).

#### EFFECTS OF HEAT.

		Degrees Fahr.
Fine-Gold	Melts	2590
" Silver	**	1860
Copper	6.	2548
Wrought Iron	44	3980
Cast "	**	3479
Glass	64	2377
Brass	••	1900
Antimony .	66	951
Bismuth.	44	476
Cadmium	44	600
Steel	44	250
Lead	44	600
Tin	66	424
Mercury boils	• 6	600
" volatilizes		806
Platinum	٠٠	4561
Zinc	6.	766
Mercury	**	39
Bronze (100 copper 10 tin)	6)	1652
Sodium	**	190
Potassium		136
Nicke!	66	3950
Tellerium	**	850
Indium	66	940

#### BLASTING.

In small blasts 1 pound of powder will loosen about  $4\frac{1}{2}$  tons.

In large blasts 1 pound of powder will loosen about 234 tons.

Inclosing 50 or 60 pounds of powder, in a resisting bag hung or propped up against a gate or barrier, will demolish any ordinary construction.

One man can bore, with a bit 1 inch in diameter, from 50 to 100 inches, per day of 10 hours in granite, or 300 to 400 inches, per day in lime stone,

Two strikers and a holder can bore with a bit 2 inches in diameter 10 feet in a day in rock of medium hardness.

# COLORS FOR DRAWING.

MATERIAL.	COLOR.
Brass.	Gamboge.
Brick.	Carmine.
Cast-Iron.	Neutral tint.
Clay.	Burnt umber.
Concrete.	Sepia with dark spots.
Earth.	Burnt umber light.
Copper.	Lake and burnt sienna.
Granite,	Indian Ink light.
Lead,	" Ink & Prussian blue
Steel.	Light blue and lake.
Water.	Cobalt or Verdigris.
Woods.	(Burnt Sienna, deep and light for dark
	and light wood.
Wrought-Iron.	Prussian blue, light.

#### STRENGTH OF ICE.

Ice two inches thick will bear men on foot; four inches, men on horse back; six inches thick will bear cattle and teams with light loads; eight inches thick, teams with heavy loads. Ten inches will sustain a pressure of 1.000 pounds per square foot. The above is on the supposition that the ice is sound, and not "snow-ice."

#### COMPARATIVE VALUE OF WOOD FOR FUEL.

Taking shell-bark hickory as the highest standard, and calling that 100, other trees will compare with it for burning purposes, as follows: shell-bark hickory, 100; pignut hickory, 95; white oak, 84; white ash, 77; dogwood, 75; scrub oak, 73; white hazel, 72; apple tree, 70; white beach 69; black birch, 65; hard maple, 65; black walnut, 62; yellow oak, 60; white elm, 58; red oak, 56; red cedar, 56; wild cherry, 55; yellow pine, 54; chestnut, 52; yellow poplar, 51; butternut, 43; white birch, 43; white pine, 30.

# THE SIZES OF SKATES.

#### COMPARE WITH SIZES OF SHOES AS FOLLOWS.

Skates, Ins.	171	71/2	8	81/2	9	91/2	10	101/2	11	111/2
Shoes, No.	91/2	11	121/2	1	21/2	4	51/2	71/2	9	101/2

# FLY WHEELS.

A fly-wheel should always have high velocity.

The diameter should be from 3 to 4 times that of the stroke of the driving engine.

The weight of the rim should be about 85 to 95 pounds per actual horse-power, the momentum of the wheel being 4½ times that of the piston.

When the engine to which a fly-wheel is to be attached is single-acting, it is customery to make the weight of the wheel 5 times greater than when it is to be attached to a double-acting engine. The weight of a fly-wheel in engines that are subjected to irregular motions, as in a cotton-press, rolling-mill, etc., must be greater than in the others where so sudden a check is not experienced.

### PILING.

Piles may be loaded to 1000 pounds per square inch of head, if driven to firm bottom.

In sandy soil, the greatest force of a pile-driver will not drive a pile over 15 feet.

### MASONRY.

Concrete or Beton should be thrown, or let fall from a height of at least 10 feet, or well beaten down. The average weight of brick-work in mortar is about 102 pounds per cubic foot.

### A FOOT SOLDIER TRAVELS IN ONE MINUTE.

Common time, 70 steps equals vards. In quick time. 110 86 In double quick time140 66 110

He occupies in the ranks a front of 20 inches, and a depth of 13, without a knapsack; the interval between the ranks is 13 inches. Average weight of men, 150 pounds each. Five men can stand in a space of 1 square yard.

Table of Proportions of the Circle and its Equal,

The diameter of any circle  $\times$  3.1416=the circumference. The circumference of a circle  $\times (\frac{1}{3.1416} = 0.31831) =$ the diameter.

The square of the diameter  $\times (\frac{3 \cdot 14 \cdot 16}{4} = 0.7854)$  = the area.

The square of the circumference  $\times \left(\frac{0.7854}{3.1416^2} = 0.07958\right) =$ the area. The diameter of a circle  $\times$  ( $\sqrt{0.7854} = 0.8862$ ) = side of

equal sonare. The circumference of a circle  $\times (\sqrt{0.07958} = 0.2821) = \text{side}$ 

of equal square. The side of any square  $\times$  ( $\pi_{2877}=3.545$ )=circumference

of equal circle. The side of any square  $\times$  ( $\frac{1}{0.8862}$ =1.1284) = diameter of

equal circle. Square of side  $\times (_{\mathfrak{g}_*, 7_{853}} = 1.27324366) =$ square of diameter

of equal circle equal so called round inches.

Round inches  $\times$  ( ${}^{97854}_{44}$ =0.0546) = square feet. Square of diameter of equal circle  $\times$  0.7854 = square side.

### MENSURATION OF SURFACES.

Area of any parallelogram = base  $\times$  perpendicular height.

Area of any triangle = base  $\times 1/2$  perpendicular height. Area of section of circle = arc  $\times 1/2$  radius.

Area of segment of circle=area of sector of equal radius, less area of triangle.

Area of parabola = base  $\times \frac{2}{3}$  height.

Area of ellipse=longest diameter  $\times$  shortest diameter  $\times$  .7854.

Area of any regular polygon=sum of its sides× perpendicular from its centre to one of its sides, divided by 2.

Surface of cylinder = area of both ends + height  $\times$  circumference.

Surface of segment = height of segment  $\times$  whole circumference of sphere of which it is a part.

Cubic contents of a cylinder=area of one end × length.

### MENSURATION OF SOLIDS.

Cylinder = area of one end  $\times$  length,

Sphere = cube of diameter  $\times$  .5236.

Segment of sphere = square root of the height added to three times the square of radius of base  $\times$  by height and by .5236.

Cone of pyramid = area of base  $\times 1/3$  perpendicular height.

Frustrum of a cone=product of diameter of both ends+sum of their squares,  $\times$  perpendicular height  $\times$  .2618.

Frustrum of a pyramid=sum of the areas of the two ends + square root of their product,  $\times$  by  $\frac{1}{3}$  of the perpendicular height.

Solidity of a wedge = area of base  $\times 1/2$  perpendicular height.

Frustrum of a wedge= $\frac{1}{2}$  perpendicular height×sum of the areas of the two ends.

Solidity of a ring=thickness + inner diameter, $\times$  square of thickness,  $\times$  2.4674.

## TO FIND THE DIAMETER AND THE BREAKING STRAIN OF A BOLT.

Multiply the area of 1  $\Box$  inch by 20, of 2  $\Box$  inch by 19, of 3  $\Box$  inch by 18, of 4  $\Box$  inch by 17, of 5  $\Box$  inch by 16, of 6  $\Box$  inch by 15, etc., for Upset Bolts; but with 12.6 for 1  $\Box$  inch, 12.54 for 2  $\Box$  inch, 12.50 for 3  $\Box$  inch, 12.31 for 4  $\Box$  inch, 11.90 for 5  $\Box$  inch, and 11.34 for 6  $\Box$  inch, for common, not Upset Bolts. The result will be the net breaking weight, which is to be divided by the required factor of safety.

EXAMPLE:—What weight can a 2 inch bolt carry before breaking with a factor of 3? Area of 2=3.1416  $\times \frac{19}{3}$  = 19.9 tons if upset, or  $\frac{3*14.16}{3}$   $\times$ 

12.54 = 13.13 if not upset.

What size of Bolt is required to carry 19.9 tons?  $19.9 \times \frac{3}{19} = 3.142 = 2$  inch round bolt upset.  $19.9 \times \frac{3}{12.54}$ =4.76=2.45 inch round, not upset.

### RULES FOR WEIGHTS OF CASTINGS.

		Cast-Iron,	
Multiply the weight	13 "		and the product
of the pattern by	19 "		is the weight of
or size personal	12.2"		the casting.
	11.4"	Zinc.	

### SHRINKAGE IN CASTINGS.

	Cast-Iron,	3-16 of an inch lon-
PATTERN MAKERS	Brass,	
RULE.	Tin,	1/8 } ger per lineal 1-12   foot.
	Zinc,	3-16)

### REDUCTION FOR ROUND CORES AND CORE PRINTS.

RULE:—Multiply the square of the diameter by the length of the core in inches, and the product by 0.017 is the weight of the Pine Core to be deducted from the weight of the pattern.

### SHIPPING ADMEASUREMENT.

REGISTER TON .- For Register tonnage or for measurement of the entire internal capacity of a vessel: 100 cubic feet = 1 Registered Ton.

This number is arbitrarily assumed to facilitate com-

putation.

### Shipping Ton for the Measurement of Cargo:

(1 U. S. shipping ton. 40 cubic feet = 31.16 Imperial bushels. 1 32.143 U. S. (1 British shipping ton. 32.719 Imperial bushels. 42 cubic feet = / 33.75 U. S.

HOW WINES AND LIQUORS ARE PUT UP AND THE NUMBER OF GALLONS THEY CONTAIN

Butt of Sherry		108	gallons.
Pipe of Port		115	
Pipe of Teneriffe		100	6
Butt of Malaga		105	6.6
	10 to	130	4.6
" Brandy 1	10 to	120	66
46 Rum 1	00 to	110	66

Hogshead of Brandy Pipe of Madelra Hogshead of Claret

55 to 60 gallons. 92 46

A hogshead is one-half, a quarter cask is one-fourth, an octave is one-eighth of apipe, butt, or puncheon.

### Proportion of Alcohol in 100 parts of the following Liquors, (Brande),

	6 =440	(2. aa.).	
Small Beer	1.08	Bordeaux	15.1
Cider	9.8	Shiraz	15.5
Porter	5.3	Malmsey	16.4
Brown Stout	6.8	Sherry	17.2
Ale	10.	" old	23.9
Perry	7.3	Alba Flora	17.3
Rhenish	7.6	Constantia, red	18.9
Moselle	8.7	Port	23.
Johannisberger	8.71	Colares	19.7
Elder Wine	8.8	Lisbon	18.9
Clarat	8.9	Malaga	17.2
Tokay	9.4	Cape Muscat	18.3
Rudesheimer	10.7	Tenneriffe	19.8
Marcobrunner	11.6	Lachryma	19.7
Gooseberry Wine	11.8	Currant Wine	20.6
Frontignac	12.9	Maderia	22.3
Hockheimer	12.1	" Sercial	27.4
Vin de Grave	12.8	Marsala	25.1
Champagne	12.7	Raisin Wine	25.2
" Burgundy	14.6	Cape Madeira	29.5
Hermitage red	12.3	Gin	51.6
Hermitage, red " white	17.4	Brandy	53.4
Amontillado	12.6	Rum	53.7
Barsac	13.9	Irish Whiskey	53.9
Santerne	14.2	Scotch "	54.4
White Port	15.	Scotch	01.1
**************************************	200		

### COMMON NAMES OF CHEMICAL SUBSTANCES.

### COMMON NAMES.

Aqua Fortis Aqua Regia Blue Vitriol Cream of Tartar Calomel Chalk Caustic Potassa Chloroform Common Salt Copperas, or Green Vitriol Corrosive Sublimate Diamond

### CHEMICAL NAMES.

Nitric Acid. Nitro-Muriatic Acid. Sulphate of Copper. Bitartrate of Potassium. Chloride of Mercury. Carbonate Calcium Hydrate Potassium. Chloride of Gormyle.
" of Sodium. Sulphate of Iron.

Bi-Chloride of Mercury. Pure Carbon.

COMMON NAMES,

Dry Alum

Epsom Salts
Ettnops Mineral
Fire Damp
Galena
Glauber's Salt
Glucose
Goulard Waters
Iron Pyrites
Jewelers Putty
Kings Yellow
Laughing Gas
Lime

kings fellow
Laughing Gas
Lime
Lunar Caustic
Mosaic Gold
Muriate of Lime
Nitre or Saltpetre
Oil of Vitriol
Potash
Realgar
Red Lead.
Rust of Iron
Sal-Ammoniac
Salt of Tartar
Slacked Lime
Soda

Spirits of Hartshorn Spirits of Salt Stucco or Plaster of Paris Sugar of Lead

Sugar of Lead Verdigris Vermilion Vinegar Volatile Alkali

Water White Precipitate

White Vitriol

CHEMICAL NAMES.

Sulphate Aluminum and Potassium.

Sulphate of Magnesia. Black Sulphide of Mercury. Light Carbureted Hydrogen. Sulphide of Lead. Sulphate of Sodium.

Grape Sugar.
Basic Acetate of Lead.
Bi-Sulphide Iron.

Oxide of Tin.
Sulphide of Arsenic.
Protoxide of Nitrogen.
Oxide of Calcium.

Nitrate of Silver.
Bi-Sulphide of Tin.
Chloride of Calcium.
Nitrate of Potash.
Sulphuric Acid.
Oxide of Potassium.
Sulphide of Arsenic.
Oxide of Lead.

Oxide of Iron.

Muriate of Ammonia.

Carbonate of Potassa.

Hydrate Calcium.

Oxide of Sodium.

Ammonia. Hydro-Chloric or Mur'ic Acid.

Sulphate of Lime. Acetate of Lead. Acetate of Copper. Sulphide of Mercury. Acetic Acid. (Diluted).

Ammonia.
Oxide of Hydrogen.
Ammoniated Mercury.
Sulphate of Zinc.

### WATER AT DIFFERENT TEMPERATURES.

There are four notable temperatures for pure water, viz:—

- 1. Freezing point at sea level, 32° F. weight per cubic foot 62,418 pounds; per cubic inch, .03612 pounds.
- 2. Point of maximum density, 39. 1° F. weight per cubic foot 62.425 pounds; per cubic inch. .036125 pounds.
- British standard for specific gravity 62° F. weight per cubic foot 62.355 pounds; per cubic inch .03608 pounds.

4. Boiling point at sea level, 212° F. weight per cubic foot 59.760 pounds; per cubic inch. .03458 pounds.

Sea water, (average), has a specific gravity of 1.028, boils at 213.2° F., and weighs 64 pounds, per cubic foot at 62° F.

A British Thermal Unit (or heat unit), is that quantity of heat which will raise one pound of water at or about the freezing point, 1° Fahrenheit. A French "Caloric" is the heat required to raise one kilogramme of water 1° Centigrade, and is equal to 3.96832 British thermal units.

### HERSCHEL'S TABLE FOR FORETELLING THE WEATHER.

This table and the accompanying remarks, originally formed by Dr. Herschel, and approved with some alterations, by the experienced Dr. Adam Clarke, are the result of many years' close observation, the whole being on a due consideration of the sun and moon in their several positions respecting the earth. They show what kind of weather will most probably follow the entrance of the moon into any of its quarters; so probably, indeed, that it has been seldom found to fall. If the new moon, first quarter, full moon or last quarter happens—

BETWEEN	IN SUMMER.
12 and 2, morning,	Fair
2 and 4 "	Cold, with frequent showers.
4 and 6 "	Rain.
6 and 8 "	Wind and rain.
8 and 10 ''	Changeable.
10 and 12 "	Frequent showers.
12 and 2, afternoon,	Very rainy.
2 and 4 "	Changeable.
4 and 6 "	Fair.
6 and 8 "	(Fair if wind N. W.; rainy
8 and 10 "	if winds S. or S. W.
10 and midnight,	Fair.
BETWEEN	IN WINTER.
	Hard frost, unless wind be S. or W.
12 and 2, morning, 2 and 4 "	
12 and 2, morning, 2 and 4 " 4 and 6 "	Hard frost, unless wind be S. or W.
12 and 2, morning, 2 and 4 "4 4 and 6 6 6 and 8 "	Hard frost, unless wind be S. or W. Snow and stormy.
12 and 2, morning, 2 and 4 " 4 and 6 ' 6 and 8 " 8 and 10 "	Hard frost, unless wind be S. or W. Snow and stormy.
12 and 2, morning, 2 and 4 "4 4 and 6 6 6 and 8 "	Hard frost, unless wind be S. or W. Snow and stormy. Rain Stormy.
12 and 2, morning, 2 and 4 " 4 and 6 ' 6 and 8 " 8 and 10 "	Hard frost, unless wind be S. or W. Snow and stormy. Rain Stormy. Cold rain if wind be W.; snow if E.
12 and 2, morning, 2 and 4 " 4 and 6 " 6 and 8 " 8 and 10 " 10 and 12 " 12 and 2, afternoon. 2 and 4 "	Hard frost, unless wind be S. or W. Snow and stormy. Rain Stormy. Cold rain if wind be W.; snow if E. Cold and high wind.
12 and 2, morning, 2 and 4 "4 4 and 6 '6 6 and 8 "1 10 and 12 "12 and 2, afternoon. 2 and 4 "4 4 and 6 "	Hard frost, unless wind be S. or W. Snow and stormy. Rain Stormy. Cold rain if wind be W.; snow if E. Cold and high wind. Snow or rain.
12 and 2, morning, 2 and 4 " 4 and 6 ' 6 and 8 " 8 and 10 " 10 and 12 " 12 and 2, afternoon. 2 and 4 "	Hard frost, unless wind be S. or W. Snow and stormy. Rain Stormy. Cold rain if wind be W.; snow if E. Cold and high wind. Snow or rain. Fair and mild.
12 and 2, morning, 2 and 4 "4 4 and 6 '6 6 and 8 "1 10 and 12 "12 and 2, afternoon. 2 and 4 "4 4 and 6 "	Hard frost, unless wind be S. or W. Snow and stormy. Rain Stormy. Cold rain if wind be W.; snow if E. Cold and high wind. Snow or rain. Fair and mild. Fair.

OBSERVATIONS.—1. The nearer the time of the moon's change, first quarter, full or last quarter is to midnight, the fairer will the weather be during the seven days following.

2. The space for this calculation occupies from 10 at night till 2 next morning.

3. The nearer to midday, or noon, the phases of the moon happen, the more foul or wet weather may be expected during the next seven days.

4. The space of this calculation occupies from 10 o'clock

in the morning to 2 in the afternoon.

### ALPHABETS OF DIFFERENT LANGUAGES.

The English alphabet contains 26 letters; the French-25; Hebrew, Chaldee, and Syriac, 22; Greek, 24; Latin. 25; Spanish, 27; Italian, 20; Arabic, 28; Persian, 31; Turkish, 33; Georgian. 36; Coptic, 32; Muscovite, 43; Sclavonic. 27; Dutch, 26; Ethiopic, 222; Tartarian, 222; Bengal India, 21; Brachman, 19; Sanscrit, 28.

### FACTS IN LAW.

Ignorance of the law excuses no one.

It is a fraud to conceal a fraud.

The law compels no one to do impossibilities.

An agreement without consideration is void. Signatures made with a lead pencil are good in law.

A receipt for money paid is not legally conclusive.

The acts of one partner bind all the others. Contracts made on Sunday cannot be enforced.

A contract made with a lunatic is void.

Contracts for advertisements in Sunday newspapers are invalid.

Principals are responsible for the acts of their agents.

Agents are responsible to their principals for errors.

Each individual in a partnership is responsible for the whole amount of the debts of the firm.

Notes bear interest only when so stated.

It is not legally necessary to say on a note "for value received."

Part payment of a debt which has passed the time of

statutory limitation revives the whole debt.

An oral agreement must be proved by evidence. A written agreement proves itself. The law prefers written to oral evidence because of its precision.

### RELATING TONOTES.

Demand Notes are payable on presentation without grace, and bear legal interest, after a demand has been made, if not so written. An endorser on a demand note is holden for a limited time, variable in different States.

A Negotiable Note must be made payable either to bearer, or be properly endorsed by the person to whose

order it is made. If the endorser wishes to avoid responsibility, he can endorse "without recourse."

A Joint Note is one signed by two or more persons, who each become liable for the whole amount.

Three Days Grace are allowed on all time notes, after the time for payment expires; if not then paid, the endorser, if any, should be legally notified, to be holden.

Notes Falling Due Sunday, or on a legal holiday, must be paid the day previous.

Notes Dated Sunday are void.

Altering a Note in any manner by the holder, makes it void.

Notes Given by Minors or Lunatics are void.

The Maker of a Note that is lost or stolen is not released from payment if the amount and consideration can be proven.

Notes Obtained by Fraud, or given by an intoxicated person, cannot be collected

An Endorser has a right of action against all whose names were previously on a note endorsed by him.

Deposits of Money in a Bank placed to the credit of depositors, are always subject to their check for full amount due.

If The Letter Containing a Protest of non-payment be put into the post-office, any miscarriage does not affect the party giving notice.

### READY RECKONING AND DISCOUNTS.

# TO FIND NET COST OF A SINGLE ARTICLE AT VARIOUS DISCOUNTS.

15 per cent. 20 ""	off,	multiply divide	price	per	dozen	рх	.07 1-12
20 and 5	6.6	multiply	66	66	6.6	6+	.061/3
20 " 10	6.6	44	6.6	6.6	4.6	66	.06
25 per cent.	4.6	6.6	66	6.6	6.6	6.6	.061/4
331/3 "	6.6	6.6	+ 6	6.6	44	6.6	1-18
331/3 "	6.6	4.6	6.6	66	6.6	6.6	.05 5-12
40 "	66	44_	**	6.6	4.6	66	.05

<b>4</b> 0 :	and 5 pe	r cen	t. off, multip	oly by .43/4
			multiply by	.04 7-12
50	66	6.6	64	.04 1-6
60	4.6	6.6	4.6	.031/3

TABLE FOR MARKING EACH ARTICLE AT A GIVEN PER CENT.
ADVANCE, WHEN BOUGHT BY THE DOZEN.

To gain	20 p	er cent.,	remo	ve poi	nt one	place to	o left	
"	25	66		after	movin	g point,	add	1-24
4.6	26	66		4.6	- 64		66	1-20
6.6	28	66		66	66	66	66	1-15
6.6	30	66		66	6.6	46	66	1-12
44	32	66		6.6	66	66	4.6	1-10
6.6	331/3	4.6		66	66	6.6	66	1-9
4.6	35	6.6		4.6	66	6.6	66	1/8
4.6	40	66		66	46	44	6.6	1-6
66	44	66		66	66	- 66	6.6	1-5
4.6	50	66		66	66	66	66	1/4
66	60	44		66	66	16	66	1/5
+ 6	80	46		"	**	46	"	$\frac{1}{2}$

EXAMPLE 1.—If goods cost \$20.00 per dozen, what is the price each, at 20 per cent. profit?

S2.00 Answer.

EXAMPLE 2.—At 35 per cent. 8)2.00

.25

\$2.25 Answer.

### TO FIND OUT THE DIFFERENCE BETWEEN PER-CENTAGE ON AND DISCOUNT OFF A PRICE.

60 per cent. on a price, i. e. \$1.00, is \$1.60. This is \$7½ per cent. from a price, \$1.60=\$1.00.

50 per cent. on a price, i. e. \$1.00, is \$1.50. This is 331/3 per cent. or 1/3 from a price, \$1.50=\$1.00.

40 per cent. on a price, i. e. \$1.00, is \$1.40. This is about

281/2 per cent. from a Price, \$1.40=\$1.01. 33 per cent. on a price, i. e. \$1.00, is \$1.331/3. This is 25 per cent. from a price, \$1.331/3=\$1.00.

25 per cent. on a price, i. e. \$1.00 is \$1.25 This is 20 per cent. or 1-5 from a price, \$1.25=\$1.00.

20 per cent. on a price, i. e. \$1.00. This is 16\% per cent. or 1-6 from a price, \$1.29=\$1.00.

 $16\frac{2}{3}$  per cent. on a price, i. e. \$1.00 is \$1.16\frac{2}{3}. This is about  $12\frac{1}{2}$  per cent. or  $\frac{1}{8}$  from a price, \$1.16\frac{2}{3} = \$1.02.

 $121_2$  per cent. on a price. i. e. \$1.00, is \$1.121\_2. This is about 1034 per cent. from a price,  $$1.121_2 = $1.01$ .

10 per cent on a price, i. e. \$1.00, is \$1.10. This is about  $9\frac{1}{8}$  per cent. from a price, \$1.10=\$1.00.

To Find out the Price for Single Pieces when Gross Price is Known (this is very convenient in buying or selling articles by the piece when list price is by the gross).

Multiply gross price by 7, and point off 3 figures from the right; those remaining are cents if gross price is dollars

and will give the price very near, i. e.  $\$10.00 \times 7 = 7.000$  or nearly  $7\phi$  each, or  $84\phi$  per dozen=\$10.08 per gross.

### To Make a List Price from which a Percentage can be Taken and Find Net Cost or Leave a Profit.

For cost 60 per cent. off, multiply by 10 and divide by 4.

EXAMPLE.  $-\$1.00 \times 10 = \$10.00 \div 4 = \$2.50$ ; this less 60 per cent. i. e. \$1.50=\$1.00.

For profit 60 per cent. off add the profit you intend to make and proceed as above.

For 50 per cent, profit on:

EXAMPLE.  $-\$1.00+50=\$1.50\times10=15.00\div4=\$3.75$ ; less 60 per cent., i. e. \$2.25=\$1.50.

If you want to make cost price 60 per cent. and wish to sell at 40 per cent, for retail for 50 per cent, profit on or 331/3 per cent. off of sales:

**E**XAMPLE. -\$2.50 list less 40 per cent. =\$2.50 - \$1.00 = \$1.50the amount of sale.

If you wish to sell at wholesale at 50 per cent, and for 25 per cent, profit on or 20 per cent. off:

EXAMPLE. -\$2.50 list less 50 per cent. =\$1.25, amount of sale.

For cost	50	per cent.	off,	multiply	by	10,	divide	by 5
66	40	- "	66	**		10	66	6
66	30	6.6	66	66		10	66	7
46	25	66	66	44		10	4.6	71/2
66	20	66	66	66		10	66	8′~

### The Following Suggestions are Given for Readily Obtaining the Cost of Goods Sold at a Discount From List Prices.

To deduct 21/2 per cent., subtract 1-40 from amount.

To deduct 5 per cent., subtract 1-20 from amount.

To deduct 5 and 21/2 per cent., subtract 1-20 from the amount; then 1-40 from remainder.

To deduct 71/2 per cent., subtract 11/2 times 5 per cent.
To deduct 10 per cent., subtract 1-10 from amount.
To deduct 10 and 5 per cent., subtract 1-10 from amount; then 1-20 from remainder.

To deduct 121/2 per cent., subtract 1/8 from the amount. To deduct 15 per cent., subtract 1½ times 10 per cent.
To deduct 15 and 5 per cent., subtract 1½ times 10 per cent. from amount, and 1-20 from remainder.

To deduct 20 per cent., subtract 1-5 from the amount. To deduct 20 and 5 per cent., subtract 1-5 from the amount; then 1-20 from remainder.

To deduct 25 per cent., subtract 1/4 from amount.

To deduct 25 and 5 per cent., subtract 1/4 from the amount; then 1-20 from remainder.

To deduct 331/3 per cent., subtract 1/3 from amount.

To deduct 35 per cent., add 30 per cent. to 1/2 the amount.

To deduct 40 per cent., subtract 1/4 from the amount; then subtract 1-5 from remainder.

To deduct 40 and 5 per cent., subtract 14; then subtract 1-5 from remainder; then 1-20. Or, subtract 4-10, and 1-20 from remainder.

To deduct 45 per cent., divide by 2 and add 10 per cent.

To deduct 45 and 5 per cent., divide by 2, add 1-10 and subtract 1-20.

Cost of Articles by the Piece, from I to I Dozen.

					<u> </u>		-				
Price				C	ost I	er (	<mark>Qua</mark> n	tity			
per Dozen.	11	10	9	8	7	6	5	4	3	2	1
\$1.00	18.92	1\$.83	\$.75	\$.67	\$.58	\$.50	\$.42	\$.33	\$.25	\$.17	\$.081/3
1.25		1.04	.94			.63	.52	.42	.31	.21	.101/2
1.50		1.25	1.13		.88	.75	.63	.50	.38	.25	.121/2
1.75				1.17		.88	.73	.56	.44	.29	.145/8
2.00	1.83	1.67	1.50	1.33	1.17	1.00	.83	.67	.50	.33	.162/3
2.25	2.06			1.50			.94	.75	.56	.38	.183/4
2.50	2.29	2.08	1.88	1.67	1.46	1.25	1.04	.83	.63	.42	.211/8
2.75	2.52	2.29	2.06	1.83	1.60	1.38	1.15	.92	.69	.46 .50	.23
3.00	2.75	2.50	2.25	$\frac{2.00}{2.33}$	1.75	1,50	1.25	1.00	.75	.50	.25
3.50	3.21	2.92	2.63	2.33	2.04	1.75	1.46	1.17	.88	.58	.291/4
3.75	3.44	3.13	2.81	2.50	2.19	1.88	1.56	1.25	.94	.63	.311/4
4.00	3.67	3.33	3.00	2.67	2.33	2.00	1.67	1.33	1.00	.67	.331/3
4.25	13.89	3.54	3.19	2.83	2.48	2.13	1.77	1.42	1.06	.71 .75	.351/2
4.50	4.13	3.75	3.38	3.00	2.63	2.25	1.88	1.50	1.13	.75	.371/2
4.75	4.23	3.96	3.56	3.17	2.77	2.34	1.98	1.58	1.19	.79	.395/8
5.00	4.58	4.17	3.75	3.33	2.92	2.50	2.08	1.67	1.25	.83	.412/3
5.25	4.81	4.38	3.94	3.50	3.06	2.63	2.19	1.75	1.31	.88	.433/4
5.50	5.04	4.58	4.13	3.67	3.21	2.75	2.29	1.83	1.38	.92	.46
5.75	5.27	4.79	4.31	3.83	3.35	2.87	2.40	1.92	1.44	.96	.48
6.00	5.50			4.00							
6.25				4.17					1.56		
<b>6.5</b> 0	5.96	5.42	4.88	4.33	3.79	3.25	2.71	2.17	1.63	1.08	.541/4
6.75	6.19	5.63	5.06	4.50	3.94	3.38	2.81	2:25	1.69	1.13	.561/4
7.00	6.42	5.83	5.25	4.67	4.08	3.50	2.92	2.33	1.75	1.17	.581/3
7.25	6.65	6.04	5.44	4.93	4.23	3.63	3.02	2.42	1.81	1.21	.601/2
7.50	6.88	6.25	5.63	5.00	1.38	3.75	3.13	2.50	1.88	1.25	,621/2
7.75	7.11	6.46	5.81	5.17	1.52	3.88	3.23	2.58	1.94	1.29	.645/8
8.00	17.33	6.67	16.00	5.33	1.67	4.00	3.33	2.67	2.00	1.33	.662/3

### HOW TO MARK GOODS.

Suppose an article is bought by the dozen, and the merchant wants to make 20 per cent. All he has to do is remove the decimal point one place to the left. Suppose brooms are \$2.50 a dozen; then 25 cents each is the cost with 20 per cent. added. To make 25 per cent. remove the point one place to the left and add 1-24.

То	make	30	per	cent.	add	1-12	itself.
66	66	331/2	- 66	66	6.6	1-9	+4
66	+ 6	331/ <sub>3</sub> 35	6.6	66	66	1/8	6.6
66	44	40	66	66	66	1-6	
••	4+	44	66	6.6	6.6	1-5	••
6.6	66	50	66	66	66	14	**
6.6	66	60	66	66	66	1/2	**
4.6	66	80	66	4.6	66	1/2	44

Always remove the decimal point one place to the left before making the additions and the sum will be the selling price of the single article,

In calculating the per cent. on a single article if you wish to make

```
10 per cent. divide by 10, multiply by 11
20
                           10
                                               12
   66
          " multiply "
                                               8
25
                           10
                                 divide
                      " 10 multiply
   66
          66
30
             divide
331/3"
          " add 1/3 of itself.
" divide by 3 multiply by
331/3...
          +6
            add 1/2 of itself.
```

### ANTIDOTE FOR POISONS.

In cases where the other articles to be used as antidotes are not in the house, give two tablespoonfuls made nustard in a pint of warm water. Also give large draughts of warm milk or water mixed with oil, butter, or lard. If possible, give as follows:

Poisons.

Antidotes.

BED-BUG POISON,
BLUE VITRIOL,
CORROSIVE SUBLIMATE,
LEAD WATER,
SALTPETRE.
SUGAR OF LEAD,
SULPHATE OF ZINC.
RED PRECIPITATE.
VERMILION,
BISMUTH,
VERDIGRIS,

Give Milk or White of Eggs, in large quantities.

Poisons.

Antidote.

FOWLER'S SOLUTION, WHITE PRECIPITATE, ARSENIC, Give prompt Emetic of Mustard and Salt, tablespoonful of each; follow with Sweet Oil, Butter, or Milk.

ANTIMONIAL WINE, TARTAR EMETIC, Drink warm water to encourage vomiting. If vomiting does not stop, give a grain of Opium in water.

OIL VITRIOL, AQUA FORTIS, BI-CARBONATE POTASS, MURIATIC ACID, OXALIC ACID,

Magnesia or Soap, dissolved in water, every two minutes.

CAUSTIC SODA, CAUSTIC POTASH, VOLATILE ALKALI, Drink freely of water with Vinegar or Lemon Juice in it.

CARBOLIC ACID, IODINE, IODIDE OF POTASS, Give Flour and Water or Glutinous drinks.

CHLORAL HYDRATE, CHLOROFORM, Pour cold water over the head and face, with artificial respiration, Galvanic Battery.

CARBONATE OF SODA, COPPERAS, COBALT,

Prompt Emetics; Soap or Mucilaginous drinks.

LAUDANUM, Strong Coffee followed by Ground Mustard Morphine, Opium, Strong Coffee followed by Ground Mustard worthine, Ke ep in motion.

STRYCHNINE, TINCT. NUX VOMICA,

NITRATE OF SILVER, Give common Salt in water.

Emetic of Mustard or Sulphate of Zinc, aided by warm water.

PHOSPHORUS,

Magnesia with water and copious draughts mucilaginous drinks.

In all cases of poisoning, the first step is to evacuate the stomach. This should be effected by an emetic which is quickly obtained. Mustard or salt (tablespoonful) mixed in a tumblerful of water, or ½ teaspoonful powdered Ipecac every 10 to 15 minutes. When vomiting has already taken place, copious dranghts of warm water should be given to keep up the effect till the poisonous substance has been thoroughly evacuated. If vomiting can not be produced the stomach-pump must be used.

### TABLE OF UNITED STATES AND FOREIGN MONEY

TABLE OF UNITED STA	A TES AND FUREIGN	IVIC	NET.
Argentine Republic.	Peso.	G	\$.965
Austria.	Florin.	G	.336
Belgium	Franc.	G	.193
Bolivia.	Boliviano.	S	.68
Brazil.	Milreis.	G	.546
British Possessions, N. A.	Dollar.		1.00
Chili.	Peso.		.912
Cuba.	Peso.	G	.926
Denmark.	Crown.	G	.268
Ecudor.	Sucre.	G	.68
Egypt.	Pound (100 piastres).	G	4.943
France.	Franc.	G	.193
German Empire.	Mark.	G	.238
Great Britain.	Pound sterling.	G	4.8665
Greece.	Drachma.	G	.193
Guatemala.	Peso.	S	.68
Hayti.	Gourde.	S	.965
Honduras.	Peso.	GSSS	.68
India.	Rupee.	G	.323
Italy.	Lira.	G	.193
Tonon	Yen. {	G	.997
Japan.	1 (	S	.734
Liberia.	Dollar.		1.00
Mexico.	Dollar.	G	.739
Netherlands.	Florin.	G	.402
Nicaragua.	Peso.	SG	.68
Norway.	Crown.	G	.268
Peru.	Sol.	S	.68
Portugal.	Milreis.	G	1.08
Russia.	Rouble.	G	.544
Spain.	Peseta.	G	.193
Sweden.	Crown.	G	.268
Switzerland.	Franc.	G	.193
Tripoli	Mahbub.		.614
Turkey	Piastre.	G	.044
United States Colombia.	Peso.	G	.68
Venezuela.	Bolivar.	G	.136

### UNITED STATES.

10 mills (m)	make	1	cent $\phi$ .
10 cents	**	1	dime $d$ .
10 dimes	66	1	dollar \$.
10 dollars	"	- 1	eagle $E$ .

### FRANCE.

U. S. Value. \$. 4. m.

10 Centimes equal 1 Decime.	.01.8 .18.7 3.72.0 7.44.0 .93.0
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### GREAT BRITAIN AND IRELAND.

GREAT BRITAIN A	IND IRELAND.	
	U. S. Value, \$.	¢. m,
4 Farthings equal 1 Penny	ο. ο. γ αιωο. <b>φ</b> .	γ. πο,
12 Pence "1 Shilling.		.22,2
20 Shillings " 1 Pound Ster	rling.	4.44.4
2 " " 1 Florin.		.44.4
10 Florins " 1 pound.		4.44,4
1 Crown " 5 Shillings.		1.08,0
1 Sovereign " 20 "		4.86,
1 Guinea " 21 "		5.07,5
SPAI	IN.	
34 Maravedis equal 1 H	Real.	.11,0
Q Doole 11 1 T	Pollar or Plate.	.88,0
275 Maravedis " 1 I	Oucat of Exchange.	2.21,0
275 Maravedis " 1 I 4 Dollars of Plate " 1 I	Pistole of "	3.88,4
AMSTER	DAM.	
16 Pfennings equal	1 Stiver.	.02,0
20 Stivers "	1 Florinour Guilder.	
12 Grotes, or Pence Flemish,	or (1 Shilling.	.12,0
12 Grotes, or Pence Flemish, 6 Stivers.	7 Flemish.	.12,0
20 Shillings, or "	{ 1 Pound.	2.40.0
6 Florins,	7 I ound.	2.10,0
21/2 Florins, or	1 Rix Dollar.	.96,0
50 Stivers,	THIX DONAL.	.00,0
HAMB	T D C	
12 Pfennings equal 1 Schillings " 1 Mark	ig or soi.	90.5
16 Schillings " 1 Mark. 3 Marks " 1 Rix Dol	Do-	.28,5
5 Marks 1 Rix Do	lar.	.85,5
PRUS	27.1	
		00.0
12 Pfennings equal 1 Silver (30 Groschen "1 Dollar.	roscnen.	.02,3
30 Groschen " 1 Dollar.		.69.0
DENMA	D V	
12 Pfennings equal 1 Ski 16 Skillings " 1 Mar 6 Marks Danish " 1 Rix	lling.	
16 Skillings " 1 Mar		.08.7
6 Marks Danish " I Rix	dollar	<b>.</b> 52,5 .
R U S S	T 4	
10 Kopecks equal 1	Grieve	.07,5
10 Grieves " 1	Ruble	.75,0
AHAMA	7.4	
AUSTR		
4 Pfenning equal 1	Kreutzer	
	Florin	.48,5
11/2 Florins " 1	Rix dollar	.72,7

### PORTUGAL.

	8 11 1	U. S. Value.	\$. ¢. m.					
1000 Rees equa	ii 1	Milree.	1.24.0					
400 Rees ''	1	Crusado of Exchange.	.49.6					
480 Rees ''	1	1 New Crusado,						
	R C	M E .						
2 Mezzi Quattrini	equ	al 1 Quattrino.						
5 Quattrini	7.	1 Baioccho.	.01.0					
10 Baiocchi	4.6	1 Paolo.	.10,0					
10 Paoli	* 6	1 Scudo.	1.00,6					
B E N G	A L an	d CALCUTTA.						
12 Pice	equa	l 1 Anna.	.03,3					
16 Anna		1 Rupee.	.50,0					
	GRI	EECE.						
100 Lepta	equa	d 1 Drachma.	.16,6					
	T U 1	RKEY.						
3 Aspers	equa	l 1 Para.	.01.0					
40 Paras	11	1 Piastre.	.40.0					

### PORTRAITS ON AMERICAN CURRENCY.

\$1, Washington; \$2, Jefferson; \$5, Jackson; \$10, Webster, \$20, Hamilton; \$50, Franklin; \$100, Lincoln; \$500, General Mansfield; \$1000, De Witt Clinton; \$5000, Madison; \$10-000, Jackson. On silver certificates—\$1, Martha Washington; \$2, Gen. Hancock; \$10, Robert Morris, Thos. A. Hen; dricks; \$20, Commodore Decatur; \$50, Edward Everett. \$100, James Monroe; \$500, Charles Sumner, and \$1000, W. L. Marcy. On gold notes—\$20, Garfield; \$50, Silas Wright; \$100, Thomas H. Benton; \$500, A. Lincoln; \$1000, Alexander Hamilton; \$5000, James Madison; \$10,000, Andrew Jackson.

### HOW BIRDS AND ANIMALS ARE GROUPED.

A table showing in a concise manner how various birds and animals are classed:—A covy of Partridges. A wide of Pheasants. A wisp of Snipe. A bevy of Quail. A flight of Doves or Swallows. A muster of Peacocks. A siege of Herons. A building of Rooks. A brood of Grouse. A plump of Wild Fowl. A stand of Plovers. A watch of Nightingales. A flock of Geese. A cast of Hawks. A trip of Dottrell. A swarm of Bees. A school of Whales. A shoal of Herrings. A herd of Swine. A skulk of Foxes. A pack of Wolves. A drove of Oxen. A sounder of Hogs. A troop of Monkeys. A pride of Lions. A sleuth of Bears.

Interest on \$1 from 2% to 9% to thousandths of a cent, for any number of days, or months, and for 1 year.

Time.   2%   3%   4%   5%   6%   7%		
	8%	9%
1 da.  .00005 .00008 ,00011 .00014 .00017 .00019 .0		.00025
		.0005
3  .00016 .00025 .00033 .00042 .0005  .00058 .0		.00075
4  .00022 .00034 .00044 .00056 .00067 .00078 .0		.001
5 [,00028].00042[.00056].00069[.00083].00097].0		.00125
6 [.00033].0005 [.00067].00083[.001 [.00117].0		.0015
7   .00039 .00058 .00078 .00097 .00117 .00136 .0 8   .00045 .00066 .00089 .00111 .00133 .00156 .0		.00175
8  .00045 .00066 .00089 .00111 .00133 .00156 .0		
9  .0005  .00075 .001  .00125 .0015  .00175 .0		.00225
10 [.00056].00083[.00111].00139[.00167].00194].0		.0025
11 [.00061].00091].00122].00153].00183].00214]-0	0244	,00275
12 [.00067].001 [.00133] 00167].002 [.00233].0		.003
13  ,00072 .60108 .00144 .00181 .00217 .00253 .0		.00325
14 [.00078[.00116].00156[.00194].00233[.00272].0		.0035
15 [.00084].00125].00167[.00208].0025 [.00292].0		.00375
	0356	.004
	00378	.00425
	004	.0045
19  .00106 .00158 .00211 .00264 .00317 .00369 .0	00422	.00475
	00444	.005
21 [.00117].00175].00233].00292].0035 [.00408].0		.00525
22 [.00122].00183[.00244].00306[.00367].00428[.0		.0055
23  .00128 .00191 .00256 .00319 .00383 .00447 .0	00511	.00575
24  .00134 .002  .00267 .00333 .004  .00467 .0	00533	.006
25  .00139 .00208 .00278 .00347 .00417 .00486 .0		.00625
26  .00145 .00216 .00289 .00361 .00423 .00506 .0	00578	.0065
27   .0015   .00225   .003   .00375   .0045   .00525   .0	006	.00675
28  .00156 .00233 .00311 .00389 .00467 .00544 .0	00622	.007
29  .00161 .00241 .00322 .00403 .00483 .00564 .0	00644	.00725
1 mo.   .00167   .0025   .00333   .00417   .005   .00583   .0	00667	.0075
2  .00334 .005  .00667 .00833 .01  .01167 .0	01333	.015
2   .00334   .005   .00667   .00833   .01   .01167   .0 3   .005   .0075   .01   .0125   .015   .0175   .0	)2	.0225
4  .00667 .01  .01333 .01667 .02  .02333 .0	2667	.03
4   .00667 .01   .01333 .01667 .02   .02333 .0 5   .00834 .0125   .01667 .02083 .025   .02917 .0	03333	.0375
6   01   015   02   025   03   035   0	)4	.045
7  .01167 .0175  .02333 .02917 .035  .04083 .0	04667	.0525
8  .01334 .02  .02667 .03333 .04  .04667 .0	)5333	.06
	)6	.0675
	06667	.075
		.0825
1 Yr.   .02   .03   .04   .05   .06   .07   .0	)8	.09

EXAMPLE:—What is the Interest on \$50.00 for 1 year; 3 months and 16 days at 8 per cent?

Interest on \$1.00 for 1 year is . . .08000

" " 1.00 " 3 mo. " . . .02000

" " 1.00 " 16 days " . .00356

Interest on \$1.00, for 1 yr., 3 mo., 16 da., .10356 Then  $$50.00 \times .10356 = $5.178$  interest at 8%.

Showing the Amount of \$1 Improved at Compound Interest for any number of years not exceeding 50.

	est J	or an	y nu	moer	of ye	ars n	oi exc	eeain	g 50.	
Yrs.	1%	11%	2%	21%	3%	31%	4%	41%	5%	6%
1 2 3 4 5 6 7 8 9 10 11 12	\$1.01			\$1.03	\$1.03	\$1.04	\$1.04	\$1.05	\$1.05	
2	1.02	1.03	1.04	1.05	1.06	1.07 1.11 1.15 1.19 1.23 1.27	1.08	1.09	1.10	1.12
3	1.03	1.05	1.06	1.08	1.09	1.11	1.12	1.14	1.16	1.19 1.26 1.34 1.42 1.50
4	1.04	1.06	1.08	1.10	1.13	1.15	1.17	1.19	1.22	1.26
5	1.05	1.08	1.10	1.13	1.16	1.19	1.22	1.25	1.28	1.34
6	1.06	1.09	1.13	1.16	1.19	1.23	1.27	1.30	1.22 1.28 1.34	1.42
7	1.07	1.11	1.15	1.10 1.13 1.16 1.19 1.22 1.25 1.28 1.31 1.34 1.38	1.13 1.16 1.19 1.23 1.27 1.30 1.34 1.38 1.43	1.27	1.17 1.22 1.27 1.32 1.37 1.42 1.48 1.54 1.60 1.67	1.36	1.41	1.50
8	1.08	1.13	1.17	1.22	1.27	1 32 1.36	1.37	1.42	1.48 1.55	1.59
-9	1.09	1.14	1.20	1.25	1.30	1.36	1.42	1.49	1.55	1.69
10	1.10	1.16	1.22	1.28	1.34	1.41 1.46 1.51	1.48	1.55	1.63	1.79
11	1.12	1.18	1.24	1.31	1.38	1.46	1.54	1.62	1.71	1.90
12	1.13	1.20	1.27	1.34	1.43	1.51	1.60	1.70	1.80	2.01
13	1.14	1.21	1.29	1.38	1.47	1.56	1.07	1.77	1.09	2.13
14	1.10	1.45	1.32	1.41	1.51	1.62	1.75	1.00	1.90	2.20
10	1.10	1.20	1.30	1.40	1.00	1.62 1.68 1.73	1.00	1.94	2.00	2.40
10	1.17	1.41	1.57	1.40	1.00	1.75	1.07	2.04	2.10	9.60
10	1.10	1.47	1.08 1.10 1.13 1.15 1.17 1.20 1.22 1.24 1.27 1.29 1.32 1.35 1.37 1.40	1.94	1.00	1,13	2.09	2.11	9.41	9.85
13 14 15 16 17 18 19	1.12 1.13 1.14 1.15 1.16 1.17 1.18 1.20 1.21	1 32	1.46	1.60	1.75	1.00	9 11	2.21	2,53	1.59 1.69 1.79 1.90 2.01 2.13 2.26 2.40 2.54 2.69 2.85 3.03
20	1 99	1 35	1.40	1.60	1 81	1 90	5.10	2.01	2.65	3 21
20 21	1 22	1 37	1.59	1.68	1.86	2.06	2.10	2.52	2.79	3 40
22	1 24	1 39	1.49 1.52 1.55 1.58	1.72	1 92	2.00	2.27	2 63	2 93	3.21 3.40 3.60 3.82 4.05
22 23 24	1 26	1 41	1.58	1 76	1 97	2 21	2.46	2.75	3.07	3.82
24	1 27	1 43	1 61	1 81	2.03	2.28	2.56	2.88	3 23	4 05
$\tilde{2}\tilde{5}$	1.22 1.23 1.24 1.26 1.27 1.28 1.30 1.31 1.32 1.35 1.36 1.37 1.40 1.42	1.066 1.088 1.111 1.134 1.146 1.18 1.20 1.21 1.23 1.25 1.31 1.35 1.37 1.39 1.31 1.41 1.43 1.45 1.47 1.49 1.52 1.55 1.55 1.55 1.55	1.61 1.64	1.41 1.45 1.48 1.52 1.56 1.60 1.64 1.72 1.76 1.81 1,85 1.90 1.95	2.09	1,79 1.86 1.92 1.99 2.06 2.13 2.21 2.28 2.36 2.45 2.53 2.62 2.71 2.81 3.01 3.11 3.22 3.33 3.45	1.80 1.87 1.95 2.11 2.19 2.28 2.37 2.46 2.567 2.77 2.88 3.00 3.12 3.24 3.37 3.51 3.79 3.79 4.10	1.14 1.19 1.25 1.36 1.42 1.49 1.55 1.62 2.17 7.77 1.85 2.02 2.11 2.21 2.31 2.41 2.52 2.63 2.75 2.88 3.01 3.28 3.58 3.58 3.58	1.63 1.71 1.80 1.98 1.98 2.08 2.18 2.29 2,41 2.53 2.65 2.79 3.39 3.56 3.73 3.92 4.12	4.29
26	1.30	1.47	1.67	1.90	2.16	2.45	2.77	3.14	3.56	4.29 4.55
26 27	1.31	1.49	1.71	1.95	2.22	2.53	2.88	3.28	3.73	4.82 5.11 5.42 5.74
28 29 30	1.32	1.52	1.71 1.74 1.78 1.81 1.85 1.92 1.96 2.00 2.04 2.08 2.12	2.00	2.29	2.62	3.00	3.43	3.92	5.11
29	1.33	1.54	1.78	2.05	2.36	2.71	3.12	3.58	4.12	5.42
30	1.35	1.56	1.81	2.10	2.43	2.81	3.24	3.75	4.32	5 74
31	1.36	1.59	1.85	2.15	2.50	2.91	3.37	3.91	4.54 4.76	6.09
32	1.37	1.61	1.88	2.20	2.58	3.01	3.51	4.09	4.76	6.09 6.45 6.84 7.25 7.69 8.15
33	1.39	1.63	1.92	2.26	2.65	3.11	3.65	4.27	5.00	6.84
34	1.40	1.66	1.96	2.32	2.73	3.22	3.79	4.47	5 25 5.52	7.25
35	1.42	1.68	2.00	2,37	2.81	3.33	3.95	4.67	5.52	7.69
36	1.43	1.66 1.68 1.71 1.73 1.76 1.79 1.81 1.84 1.87	2.04	2.43	2.90	3.45	4.10	3.91 4.09 4.27 4.47 4.67 4.88	5.79	8.15
37	1.45	1.73	2.08	2.49	2.99	3.57 3.70	4.27 4.44 4.62 4.80 4.99 5.19	5.10 5.33 5.57 5.82 6.08	6.08	8.64 9.15 9.70
38 39	1.40	1.76	2.12	2.56	3.07	3.70	4.44	0.25	6.39	9.19
39	1.47	1.79	2.16	2.62	3.17	3.83	4.02	0.07	6.70	10.70
40 41	1.49	1.01	2.21	2.09	3.20	3.83 3.96 4.10	4.00	0.04	7.04	10.29
42	1.00	1.09	2.20	2,70	9.00	4.10	5 10	6.35	7.00	11.56
43	1.49 1.50 1.52 1.53	1 1 00	2.30	2.02	9.40	4.24	5.19		8 15	10.29 10.90 11.56 12.25
45	1.00	1.90	2.04	2.09	3.67	4.59	5.62	6.94	8 56	12 99
45	1.55	1.93 1.95	2.39	3.04	1.471 1.516 1.600 1.655 1.700 1.705 1.811 1.922 2.199 2.166 2.222 2.43 2.500 2.565 2.73 2.250 2.366 2.360 2.360 2.360 3.366 3.	4.54 4.70	5.81	7 25	8 99	13.76
46	1.55 1.56 1.58 1.60	1 98	2.16 2.21 2.25 2.30 2.34 2.39 2.44 2.49 2.54 2.54	2.05 2.10 2.15 2.20 2.32 2.37 2.43 2.49 2.56 2.62 2.69 2.75 2.82 2.96 3.04 3.11 3.19 3.27	3 90	4 87	5.40 5.62 5.84 6.08	6.94 7.25 7.57 7.92 8.27	9.43	12.25 12.99 13.76 14.50
47	1.60	$\begin{vmatrix} 1.98 \\ 2.01 \end{vmatrix}$	2.54	3.19	3.90 4.01 4.13	4.87 5.04	6.32	7.92	9.91	15.47
48	1.61	2.04	2.59	3.27	4.13	5.21	6.57	8.27	10.40	16.39
49	1.63	2.07	2.64	3.35	4.26	5.40		1 8.64	110.92	17.38
50	1.64	2.07 2.11	2.69	3.44	4.20 4.38	5.58	7.11	9.03	11.47	18.42

Table showing the net amount of earnings of One Cent to Fifty Dollars per day for Five Years of 313 working days, without interest and with interest at 5, 6, 7, and 8, per cent., improved each six months.

Savings pe <b>r</b> day.	Without interest.	With interest at 5%	With interest at 6%	With interest at 7%	With interest at 8%
1 2 3 4 4 5 6 6 7 8 9 9 10 15 50 6 6 70 8 90 9 10 15 00 6 6 00 25 00 25 00 25 00 25 00 45 00 45 00 50	\$15 65 31 30 46 95 62 60 78 25 93 90 109 55 125 20 140 85 116 50 234 75 313 00 391 25 469 50 626 00 782 50 939 00 1,095 50 1,202 00 1,403 50 1,565 00 3,139 00 4,695 00 1,935 00 12,523 00 12,523 00 12,523 00 12,523 00 12,523 00 12,523 00 12,523 00 12,635 00	\$17 53 35 07 52 60 70 13 87 67 105 20 122 73 140 27 157 80 175 83 263 00 350 00 438 33 526 00 350 00 438 33 526 00 1,227 33 1,402 66 1,578 30 1,778 30 1,778 30 1,778 30 14,027 63 15,779 99 10,519 99 11,773 30 14,027 63 15,779 30 17,533 29 26,299 94 35,066 58 43,833 23 52,599 88 61,366 52 70,133 17 78,899 82 70,133 17 78,899 82 87,666 46	\$17 94 35 88 53 82 71 76 89 70 107 65 125 59 143 53 161 43 179 41 267 11 358 82 448 52 538 23 1,076 43 1,255 87 1,435 28 1,614 69 1,794 10 3,588 19 5,382 29 5,382 29 5,382 29 5,382 29 5,382 29 5,382 29 6,448 52 1,794 96 26 711 46 26 711 46 35,881 94 44,852 43 53,882 91 71,7940 96 26 711 46 87 17,940 96 26 711 46 87 17,940 96 26 711 763 88 88 18 23 91 71,763 88 80,734 37 89,704 86	\$18 36 36 72 55 08 73 44 91 80 110 128 52 146 88 165 24 168 29 367 19 458 99 550 79 917 98 1,101 58 7,101 58 8,671 93 5,507 99 12,851 74 14,682 77 16,523 76 11,682 77 16,523 77 16,523 63 27,539 45 65,078 89 85,078 89 85,078 89 85,078 89 17,8438 52 82,618 84 91,798 15	\$18 79 37 58 56 37 75 16 98 95 112 74 131 53 150 32 169 11 187 90 281 84 375 79 469 74 563 69 751 58 939 48 1,127 37 1,315 27 1,503 16 1,691 06 3,757 91 5,636 89 11,273 73 13,132 69 15,031 65 16,910 60 1,878 96 3,757 91 5,636 86 11,273 73 13,132 69 16,910 60 18,789 56 28,184 34 26,973 89 56,763 45 75,158 23 84,533 01 75,158 23 84,533 01 75,158 23 84,533 01 75,158 23 84,533 01 98,947 79

TIME AT WHICH MONEY DOUBLES AT COMPOUND INTEREST.

At 10 per cent interest, in 7 years 31/2 months; at 9 per cent., in 8 years 1/2 month; at 8 per cent., in 9 years; at 7 per cent., in 10 years 3 months; at 6 per cent., in 11 years 11 months; at 5 per cent., in 14 years 21/2 months; at 4 per cent., in 17 years 8 months; at 3 per cent., in 23 years 51/2 months; at 2 per cent., in 35 years.

### HANDY INTEREST RULES.

For finding the interest on any principal for any number of days, multiply in each case the dollars by the number of days, and for ascertaining at the rate of—

3	per cent.,	Divide b	y 120 90		er cent.,	Divide by	40 36
5	"	"	72	$1\dot{2}$	66	"	30
7		"	$\frac{60}{52}$	15 18	"	"	24 20
8	•6	66	45	20	4.6	66	18

Then by cutting off the two right hand figures, you have the interest in dollars and cents.

Example:-Interest on \$50 for 30 days at 4 per cent.,  $50 \times 30$  equals 15.00, which divided by 90 equals 16\%, the required result.

### CALCULATING INTEREST.

To find the interest on any given amount for a given

For 1 per cent., multiply the amount by the number of

days and divide by 36,000.

For 2 per cent., multiply the amount by the number of days and divide by 18,000. For 3 per cent., multiply the amount by the number of

days and divide by 12,000.

For 4 per cent., multiply the amount by the number of days and divide by 9,000.

For 5 per cent., multiply the amount by the number of days and divide by 7,200.

For 6 per cent., multiply the amount by the number of days and divde by 6,000. For 7 per cent., multiply the amount by the number of

days and divide by 6,000 and add 1. For 8 per cent., multiply the amount by the number of

days and divide by 4.500.

For 9 per cent., multiply the amount by the number of days and divide by 4,000.

For 10 per cent., multiply the amount by the number of days and divide by 3,600.

For 11 per cent. multiply the amount by the number of days and divide by 3,600 and add  $\frac{1}{10}$ .

For 12 per cent., multiply the amount by the number of days and divide by 3,000.

For 13 per cent., multiply the amount by the number of

days and divide by 3,000 and add 12.

For 14 per cent., multiply the amount by the number of days and divide by 3,000 and add \( \frac{1}{6} \).

For 15 per cent., multiply the amount by the number of days and divide by 2,400.

The formula is as follows:

Principal × number of days 
$$\div \frac{36,000}{\text{Rate } \%} = \text{interest.}$$

Table showing the number of days from any given day in one month to any given day in another month.

Mo.	Ja.	Fe.	M.	Ap.	Ma.		J'y.	Au.	Se.	Oc.	No.	De.
Jan.	365	31	59	90	120				243		304	334
Feb.	334	365	28	59	89	120	150	181	212	242	273	303
Mar.	306	337	365	31	61	92	122	153	184	214	245	275
Apr.	275	306	334	365	30	61	91	122	153	183	214	244
May.	245	276	304	335	365	31	61	92	123	153	184	214
Jun.	214	245	273	304	334	365	30	61	92	122	153	183
Jul.	184	215	243	274	304	335	365	31	62	92	123	153
Aug.	153	184	212	243	273	304	334	365	31	61	92	122
Sep.	122	153	181	212	242	273	303	334	365	30	61	91
Oct.	92	123	151	182	212	243	273	304	335	365	31	61
Nov.	61	92	120	151	181	212	242	273	304	334	365	30
Dec.	31	62	90	121	151	182	212	243	274	304	335	365

RULE:—Find the first given month in the left hand column, and the second given month in the line at the top of the table, and to the number of days found at the intersection of the two lines, add the difference between the days mentioned in the two given months.

When the number of days given in the first mentioned month is greater than the given number of days in the second month, then the difference of the days must be subtracted.

EXAMPLE: How many days from March 21st to the 23rd of next September.

184, the number of days at intersection of the lines, and 23 - 21 = 2. the difference of the days in the two given months. Hence 184 + 2 = 186 days.

When February has 29 days, proper allowance must be made.

# INTEREST LAWS OF DIFFERENT STATES.

In the subjoined table the figures under the head "Legal" show the legal rate per cent.; those under "Special" show the highest rate allowed under special contract;

Penalty of Usury.	Loss of interest.  None.  None.  None.  None.  None.  Forfeiture of all interest.  Forfeiture of contract.  Forfeiture of contract.  Forfeiture of all interest.  None.  Sign. or impisonment 6 months, or both.  Forfeiture of all the interest.  Forfeiture of all the interest.  Forfeiture of all the interest.  Forfeiture of access over 12 per cent.  Forfeiture of access over 12 per cent.  Forfeiture of all the interest.  Forfeiture of all the interest.  Forfeiture of all the interest.  Forfeiture of sexess.
Legal. Special.	***************************************
Legal.	000000000000000000000000000000000000000
STATE.	Alabama. Arizona. California California Colorado Connecticut Connecticut Colorado Delaware District of Columbia Fronda Georgia Illinois Illinois Indiano Illinois Indiana Illinois Indiana Illinois Indiana Illinois Indiana Illinois Indiana Illinois Indiana Illinois

# INTEREST LAWS OF DIFFERENT STATES (CONTINUED).

gments).		7 per cent.				and costs.		the interest received.						neipal and costs.	May 28, 1858.	er rate is contracted.		Forfeiture of excess over 6 per cent. and \$100 fine.							est.		bonds only. ‡ No limit.
None (6 per cent. on judgments).	Forfeiture of excess.	Forfeiture of excess over 7 per cent.	None.	Forfeiture of all interest.	None.	Forfeiture of all interest and costs.	None.	Forfeiture of three times the interest received.	Forfeiture of all interest.	None.	Forfeiture of contract.	Forfeiture of interest.	Forfeiture of excess.	Forfeiture of interest, principal and costs.	Forfeiture of excess, Ac	Forfeiture, unless a greater rate is contracted.	None.	Forfeiture of excess over	None.	None.	Forfeiture of excess.	Forfeiture of contract.	None.	Forfeiture of excess.	Forfeiture of all the interest.	None.	*Rate on judgments unless otherwise expressed. † On railroad bonds only. ‡ No limit.
++	2	12	++	10	:	12	++	9	2	12	9	<b>x</b>	œ	12	9	++	++	2	++	++	+	12	++	9	10	++	otherwis
9	9	_	9	9	2	2	10	9	_	9	9	9	9	2	9	.9 *	_	9	ж —	2	9	9	2	9	2	10	unless
Massachusetts	Michigan	Minnesota	Mississippi	Missouri	Montana	Nebraska	Nevada	New Hampshire	New Jersey	New Mexico	New York	North Carolina	Ohio	Oregon	Pennsylvania	Rhode Island	South Carolina	Tennessee	Texas	Utah	Vermont	Virginia	Washington Territory.	West Virginia	Wisconsin	Wyoming	*Rate on judgments

Statutes of Limitations—State Laws with reference to Limitation of Action, the limit of years to bring Action.

itation of Action, t	he limit	of year	s to br	ing  Act	ion.
STATES	Assault.	0		T	Sealed &
and	Replev-	Open	Notes.	Judg-	witnes'd
TERRITORIES.	in etc.	acints.		ments.	Instr'ts
Alabama.	1 1	3	6	20	1 10
Arkansas	l ī	3	6 5	10	10
California	3	$\tilde{2}$	4	5	Š
Colorado	ĺ	$\bar{2}$	$\tilde{2}$	3	3
Connecticut	1	6	6	6	17
Dakota	$\frac{1}{2}$	6	6	20	20
Delaware	1	3	6	20	20
District of Columbia	1	3	4 2 6 6 6 3 5	12	12
Florida	$ $ $\bar{2}$	5	5	20	20
Georgia	1	4	6	7	20
Idaho	3	2	4	5	5
Illinois	1	5	10	20	10
Indiana	2	6	20	20	20
lowa	2	5	10	20	10
Kansas	$\begin{bmatrix} \frac{1}{2} \\ 1 \\ 1 \end{bmatrix}$	3	5 5	5	15
Kentucky	1	5	5	15	15
Louisiana	1	3	5	10	20
Maine	2	6	20	20	20
Maryland	3	3	3	12	12
Massachu setts,	2	6	20	20	20
Michigan	1 2 3 2 2 2 1	$\mid 6 \mid$	6	10	10
Minnesota	2	6	6	10	20
Mississippi	1	332266335425653536366634266	6	7	7
Missouri	1	4	20	5 5	10
Montana	$\begin{bmatrix} \bar{2} \\ 2 \end{bmatrix}$	2	.4	5	4
Nebraska	2	6	20	20	10
Nevada	2,6		20	20	20
New Hampshire	1 1	-		10	10
New Jersey	2	6	6	20	20
New York	1	0 0	10 15	15	15
North Carolina	1	0	10	10	10
	i	0	15	15	15
Ontario (U. Canada)	i	5		30	30
Oregon	$\frac{1}{2}$	1	5 6	10.	26
Pennsylvania	i	6	6	20	20
Quebec (L. Canada)	1.2	5	6 5 6	30	30
Rhode Island	1,2	6	6	20	20
South Carolina		6	6	20	20
Tennessee	2	6	6	20	20
Texas	i	2	4	10 l	10
Utah	i	2	4	5	7
Vermont		6	14	8	. 8
Virginia	5	5		10	20
Washington Territory.	2	3	6	9	20
West Virginia	5	5	5 6 6	10	10
Wisconsin	2 5 2 5 2	-6363651656662265356	6	20	20
Wyoming	1	6	6 15	10	21

EXEMPTION LAWS OF UNITED STATES.

EXEMPTION LAWS OF UNITED STATES.						
	Value of	Acres	Value			
STATES.	Personal	of	of			
DIAIDS.	Property.	Land.	Homestead.			
		·				
Alabama	\$1,000	160	\$2,000			
Arizona	900		5,000			
Arkansas	500	160	2,500			
California	900		5,000			
Colorado	1.000	ş	2,000			
Connecticut	500	٥	*			
Dakota	1,500	160	*			
Delaware.	200	100	*			
District of Columbia	300		*			
Florido	1.000	160				
Florida		50	1 000			
Georgia	300	90	1,600			
Idaho	300		5,000			
Illinois	300		1,000			
Indiana	600		*			
Iowa	200	40				
Kansas	800	160	i i			
Kentucky	200		1,000			
Louisiana	Ť	160	†			
Maine	300		500			
Maryland	100		*			
Massachusetts,	450		800			
Michigan	400	40	1,500			
Minnesota	860	80	1,000			
Miggigginni	550	80	0.000			
Mississippi		160	2,000			
Missouri	300	100	1.500			
Montana	900	7.00	5,000			
Nebraska	*****	160	2,000			
Nevada	900		5,000			
New Hampshire	450		500			
New Jersey	200		1,000			
New Mexico	900		5,000			
New York	250		1.000			
North Carolina	500		1,000			
Ohio	100		1,000			
Oregon	175		*			
Pennsylvania	300		*			
Rhode Island	500		*			
South Carolina	500		1,000			
Tennessee	1.200		1,000			
Texas	1.200	200				
Utah		200	5,000			
Utah		-	1,000			
Vermont	200		500			
Virginia	<u>.</u> .					
Washington	1	‡	‡			
West Virginia	200		1.000			
Wisconsin	450	40				
Wyoming	900		5,000			
4.37 77						

<sup>\*</sup>No Homestead Law. † The homestead, land and personal property not to exceed \$2,000. ‡ Similar to California. § Any number. || No limit.

### RULES OF PARLIAMENTARY PROCEDURE.

Trace each motion to its respective references on the next page, and you master at a glance the intricacies of Parliamentary usages, comprising some three hundred points of order:

Motion to adjourn	1 a * B a J x
Motion to adjourn	
journ	2atAaJx
Motion to amend	$3a \dagger A \alpha J X$ $3a * A \alpha J X$
Motion to amend an amendment	$3a * A \alpha J x$
Motion to amend the rules	3 a † A · b J x
Motion to appeal from Speaker's decision	1 . 1
re indecorum.	la†AaJn
Motion to appeal from Speaker's decision	9 T
generally	3 a * A a J n 1 a * A a S n
Motion to close debate on question	
	$1a \dagger A b J x$ $3b \dagger A a J x$
Motion to commit	SUIAUSX
tion	lațAaJx
tionLeave to continue speaking after inde-	Idiana
corum	1 a * A a J x
Motion that do lie on the table	1a * CaJx
Motion to limit debate on question	1atAbJx
Objection to consideration of question	la*AbSn
Motion for the orders of the day	1a*AaSn
Motion to postpone to a definite time	1 a * A a S n  4 a † A a J x
Motion to postpone indefinitely	3 b * A a J x
Motion for previous question	1a*AbJx
Questions touching priority of business	1a†AaJx
Questions of privilege	3a†AaJx
Reading papers	1 a * A a J x
Motion to reconsider a debatable question.	3b*BaJz
Motion to reconsider an undebatable ques-	1 - 4 7 7
tion.	$1a * B \alpha J z$
Motion to refer a question	3b † A a J x
Question whether subject shall be discussed	1a * B a J x 1a * A b S n
Motion to make subject a special order	3atAbJx
To substitute in the nature of an amend-	Jairos
ment	3 a † A a J x
Motion to suspend the rules	1a * B b J x
Motion to take from the table	1a * CaJx
To take up question out of its proper order	1a * AbJx
Motion to withdraw a motion	la * AaJx
Questions of precedence of questions	567891012
Forms in which questions may be put131	4 15 16 17 18 19

RULES OF PARLIAMENTARY PROCEDURE-Condensed.

1. Question undebatable: sometimes remarks tacitly allowed.

2. Undebatable if another question is before the assembly.

3. Debatable question.

4. Limited debate only on propriety of postponement.

a. Does not allow reference to main question.

b. Opens the main question to debate.

\*. Cannot be amended.

t. May be amended. A. Can be reconsidered.

B. Cannot be reconsidered.

C. An affirmative vote on this question cannot be reconsidered.

b. Requires two-third vote unless special rules have been enacted.

a. Simple majority suffices to determine the question.
 J. Motion must be seconded.

S. Does not require to be seconded.

x. Not in order when another has the floor.
 n. Always in order though another may have the floor.

z. May be moved and entered on the record when another has the floor, but the business then before the assemby may not be put aside. The motion must be made by one who voted with the prevailing side, and on the same day the original vote was taken.

5. Fixing the time to which an adjournment may be

made; ranks first.

To adjourn without limitation; second.

7. Motion for the Orders of the Day; third. 8. Motion that .. do lie on the table; fourth. 9. Motion for the previous question; fifth.

10. Motion to postpone definitely; sixth. 12. Motion to commit; seventh.

13. Motion to amend; eighth.

14. Motion to postpone indefinitely; ninth.

15. On motion to strike out words, "Shall the words stand part of the motion?" unless a majority sustains

the words they are struck out.

16. On motion for previous question the form to be observed is, "Shall the main question be now put?" This, if carried, ends debate.

17. On an appeal from the Chair's decision, "Shall the decision be sustained as the ruling of the house?" The

chair is generally sustainded.

18. On motion for Orders of the Day, "Will the house now proceed to the Orders of the Day?" This, if carried,

supersedes intervening motions.

19. When an objection is raised to considering question, "Shall the question be considered?" objection may be made by any member before debate has commenced, but not subsequently.

# Law of Grace on Sight Drafts, and Damages on Protested Bills of Exchange.

Protested	Bills of Exchange.
STATES.	ON SIGHT DRAFTS.
Alabama	Grace is allowed.
Arizona	Grace allowed.
Arkansas	No statute.
California	No grace.
Colorado	No grace.
Connecticut	No grace.
Dakota	Allowed by statute of 1873.
Delaware	No grace.
District of Columbia	No grace.
Florida	No grace by custom.
Georgia	No grace. Act Feb. 8, 1850.
Idaho	No grace.
Illinois	No grace.
Indiana	Grace allowed.
Iowa	Grace allowed.
Kansas	Grace allowed.
Kentucky	Grace allowed.
Louisiana	Grace not allowed by custom.
Maine	Grace allowed. Rev. St'ts., p. 264.
Maryland	Grace not allowed.
Massachusetts,	Grace allowed.
Michigan	Grace allowed by custom.
Minnesota	Grace allowed by custom.
Mississippi	Grace allowed by custom.
Missouri	Grace not allowed by custom.
Montana	Grace allowed by custom,
Nebraska	Grace allowed by statute.
Nevada	Grace not allowed.
New_Hampshire	Grace allowed by Rev. St'ts p 389.
New Jersey	Grace allowed by statute.
New Mexico	Grace allowed.
New York	Grace not allowed. Act Ap'l, 1857.
North Carolina	Grace allowed. Act Jan'y, 1849.
Ohio	Grace not allowed. Act Feb. 1861.
Oregon	Grace allowed by statute.
Pennsylvania Rhode Island	Grace not allowed. Act May 1857.
South Carolina	Grace not allowed. Act May 1857. Grace allowed. Act 1848.
	Grace not allowed by statute.
Tennessee	Grace not allowed by usage.
Utah	Grace allowed by custom.
Vermont	Grace not all'ed. St'te Jan. 1873.
Virginia	Grace not allowed by statute 1873.
Washington	No Grace.
West Virginia	No grace by custom.
Wisconsin	Grace all'ed. Rev. statutes, 1849.
Wyoming	Grace allowed by custom.
Canada	Grace allowed by custom.

The damages on a domestic Bill of Exchange or note, consist of Notaries' fees, postage, &c., and range from \$1.25 to \$2.50, according to the Statute of the State where it goes to protest. Foreign Bills, that is, drafts drawn by a person out of the United States upon another within the same, or the reverse, and protested for non-paymeut. are subject to a total expense for protest, &c., of from \$1.50 upwards.

### WEIGHTS AND MEASURES.

### AVOIRDUPOIS WEIGHT.

16 drachms	equal	1 ounce.
16 ounces	-66	1 pound.
25 pounds	+6	1 quarter.
4 quarters		1 hundred.
20 hundred	64	1 ton

The English quarter is 28 fbs. Hundred weight 112 fbs. Ton 2240 pounds.

### TROY WEIGHT.

	grains	equal	1 pennyweight.
20	pennyweight	**	1 ounce.
10	Omnood	6.6	1 nound

Weighing Diamonds 31/3 grains equal one carat.

The standard unit of weight (the Troy fb.) is equal to 22.794422 inches of distilled water, at the temperature of 39.88°, the barometer being at 30 inches. This is the unit measure of weight, (in the U. S. Mint).

7000	Troy	grains	equal	1 fb.	avoirdupois
175	66	pounds	-6.6	144 lb.	46
175	66	ounces	66	192 oz.	66
4371	/2 "	grains	66	1 oz.	44

### APOTHECARIES WEIGHT.

20 grains (gr)	equal	1 scruple, or 3
3 scruples	7.6	1 dram, or 3
8 drams	4.6	1 ounce, or 3
12 ounces	6.6	1 pound, lb or Ib.

### APOTHECARIES FLUID MEASURE. \*

60 minims (or drops) 8 fluid drams	equal	1 fluid dram fl 3. 1 " ounce fl 3.
16 " ounces	66	1 pint.
8 pints	44	1 gallon.

45 drops, or a common teaspoonful, make about 1 fluid dram; 2 teaspoonfuls about 1 fluid-ounce; a wineglassful about  $1\frac{1}{2}$  fluid-ounces; and a teacupful about 4 fluid-ounces.

### LIQUID OF WINE MEASURE.

2276022		MANUAL MANUAL
4 gills	equal	1 pint.
2 pints	• •	1 quart.
4 quarts	6.6	1 gallon.
311/2 gallons	6.6	1 barrel.
42 gallons	66	1 tierce.
63 gallons	66	1 hogshead.
2 tierces	66	1 puncheon.
2 hogsheads	66	1 pipe or butt.
2 pines	66	1 fun

The following cylinders contain some of these measures very closely.

Gill		meter.		ight ns.		Gallon		meter.		ght.
1/2 Pint	214	6.	35/	8 "	2	••	7	44	12	66
Pint	31/2	66	3	""	8	66	14	4.6	12	6+
Quart	31/2	66	6	4.6	10	4.6	14	6.6	15	66

The Standard Unit of Liquid Measure adopted by the U.S. Government is the Winchester Wine Gallon, which contains 231 cubic inches, and holds 8.339 fbs. Avoirdupois of distilled water, at its maximum density weighed in air, the barometer being at 30 inches.

The *Imperial Gallon* adopted by Great Britain contains 277.274 cubic inches, containing 10 lbs. Avoirdupois of distilled water, weighed in air, at a temperature of 62°, the barometer at 30 inches and equals 1.20032 U. S. gallons.

To convert Imperial gallons to U. S. gallons multiply by 1.20032. And to convert U. S. gallons to Imperial gallons multiply by .83311.

### UNITED STATES AND BRITISH LINEAL MEASURE.

The Standard Unit of the U. S. and British linear measure is the yard. It was intended to be exactly the same for both countries, but in reality the U. S. yard exceeds the British Standard by .00087 inch. The actual Standard of length of the U. S. is a brass scale 82 inches long prepared for the Coast Survey and deposited in the office of Weights and Measures at the U. S. Treasury Department Washington. The yard is between the 27th and 63rd inches of this scale. The temperature at which this scale is designed to be standard and at which it is used in the U. S. Coast Survey, is 62° Fahrenheit.

The Imperial (British) standard yard is referred to a natural standard, which is the length of a pendulum vibrating seconds in vacuo in London, at the level of the sea; measured on a brass rod, at a temperature of 62°.

### LONG MEASURE.

12 inches	equal	1 foot.
3 feet	-6.	1 yard.
51/2 y'ds or 161/	9 ft. "	1 rod.
40 rods	4	1 furlong.
8 furlongs	66	1 mile.

One yard is .000568 of a mile. One inch is .0000158 of a mile.

### SQUARE MEASURE.

144 square inches	equal	1 sq. foot.
9 '" feet	-66	1 sq. yard.
3014 " yards	66	1 sq. rod.
40 " rods	66	1 rood.
4 roods	66	1 acre.
640 acres	66	1 sq. mile.

An acre is 63.5701 yards square; or 208.710321 feet square; 220 feet by 198 feet square equal 1 acre.

### SURVEYOR'S MEASURE.

7.92 inches	equal	1 link.
25 links	**	1 rod.
4 rods	66	1 chain (66 ft).
80 chains	66	1 mile.

A Nautical mile contains 6080 feet. A Statute mile 5280 feet. Three Nautical miles 1 league; 20 leagues 1 degree; 6 feet 1 fathom. One knot or geographical mile is 1-60 of a degree; 3 knots make 1 marine league; 60 knots or 69.19 statute miles equal 1 degree. A hair's breadth is 1-48 part of an inch. A ship's cable is a chain usually about 120 (720 ft.) fathoms long.

### DRY MEASURE.

2 pints	equal	1 quart.
4 quarts	***	1 gallon.
2 gallons	66	1 peck.
4 pecks	66	1 bushel.

The standard bushel is the Winchester, containing 2150.42 cubic inches, or 77.627 avoirdupois pounds of distilled water at its maximum density. Its diameter (cylinder) inside is 181/2 inches, outside 191/2 inches, its depth is 8 inches.

The Imperial (English) bushel equals 2218.192 cubic inches, equals 1.03152 U. S. bushels.

 $36~\mathrm{U.~S.}$  bushels equals 1 chaldron equals 58.658 cubic feet and weighs  $3.136~\mathrm{pounds.}$ 

Heaped bushel, 191/2 inches in diameter, cone 6 inches equals 2815, 4872 cubic inches.

32 British or Imperial bushels are equal to 38 U.S. bushels. The English quarter equals 814 (nearly) U.S. bushels and contains 10.2694 cubic feet. Four quarts or 1/2 peck equals 282 cubic inches.

### SOLID OR CURIC MEASURE.

	cubic	inches	equal	1 cubic foot.
27	6.6	feet	66	1 " yard.
128	66	feet	+6	1 cord.

8 feet long, 4 feet wide, 4 feet high, equal 128 cubic feet or 1 cord of wood. 2434 cubic feet equal 1 perch of stone, or masonry. One cubic foot of water weighs 62½ pounds. A cubic foot contains 2200 cylindrical inches, 3300 spherical inches, or 6600 conical inches.

### CLOTH MEASURE.

21/4 in	ches	equal	1 nail.
. 4 🗀 na	ils	746	1 quarter.
4 qu	arters	66	1 yard.
3	66	66	1 ell Flemish.
5	4.6	4.6	1 ell English.
6	66	66	1 ell French.
4 2-15	"	. "	1 ell Scotch.

### METRIC, OR FRENCH LIQUID AND DRY MEASURE.

Litres.						
Millilitre equal .001	equal	.061	={	Liquid Dry	.00845 $.0018$	gill. pint.
Centilitre equal .01	equal	.61	= {	Liquid Dry	.0845	gill. pint.
Decilitre equal .1	equal	6.1	= {	Liquid Dry	.845 .18	gill. pint.
Litre equal 1. eq						pints.
Decalitre equal 10.						galls.
	<i>U. S.</i>		,			
			(	Liquid	26,414	galls.

Hectolitre equal 100. equal  $3.531 = \begin{cases} \text{Liquid } 26.414 \text{ galls.} \\ \text{Dry} & 2.837 \text{ bush.} \end{cases}$ Kilolitre equal 1000. equal  $35.31 = \begin{cases} \text{Liquid } 264.141 \text{ gals.} \\ \text{Dry} & 28.374 \text{ bush.} \end{cases}$ Myrialitre equal 10000. equal  $353.1 = \begin{cases} \text{Liquid } 2641.42 \text{ gals.} \\ \text{Dry} & 283.74 \text{ bush.} \end{cases}$ 

### METRIC, OR FRENCH LINEAL MEASURE.

		Metres.		U. S. Me	easure.
Mynametre	equal	10,000.	equal	6.2137	miles.
Kilometre	- 44	1,600.	66	.62137	6.6
Hectometre	+6	100.	4.6	328.1	feet.
Decametre	+6	10.	66	393 7	inches.
Metre	6.6	1.	6.6	39.37	66
Decimetre	66	.1	6+	3.937	6.6
Centimetre	44	.01	4.6	.3937	6.6
Millimetre	6.	.001	66	.03937	66

### METRIC, OR FRENCH SQUARE MEASURE.

	S	q. Met	res.	U. S.	Sq. Measure.
Sq. Centimetre	equal	.01	equal	.155	sq. inches.
Sq. Decimetre	7.0	.1	7.6	1.55	sq. "
Centiare	66	1.	**	10.763	sq. feet.
Are	6.6	10.	64	119.6	sq. yards.
Hectare	6.6	100.	6.6	2.47	Acres.
Sq. Kilometre		.38607		s equa	al 247 acres.

Sq. Mynametre equal 38.607 sq. miles equal 247 acres.

### METRIC, OR FRENCH CUBIC OR SOLID MEASURE.

	Cu	. Metres		U. S. (	Cu. Measure	
<b>Cubic Centimetre</b>	equal	.0001	equal	6.10165	cu. inches.	
" Decimetre	-66	.001	-66	61.0165	cu. "	
Centistere	66	.01	6.6	.353105	cu. feet.	
Decistere	6.6	.1	6.6	3.53105	cu. "	
Stere	6.6	1.	66	1.3078	cu. yards.	
Decastere	6.6	10.	6.0	13.078	cu. "	
Hectostere	6.6	100.	66.1	30.78	cn. "	

### METRIC, OR FRENCH WEIGHTS.

		Grammes.		Avoir	
Millegramme	=	.001	=	.00003528	ounce.
Centigramme	==	.01	=	.0003528	**
Decigramme	=	.1	=	.003528	44
Gramme	= "	2.	=	.03528	64
Decagramme	==	10.	=	.3528	• 6
Hectogramme	=	100.	=	3.52758	4.6
Kilogramme	=	1,000.	=	35.2758	66
Myriogramme	=	10,000.	=	22.04737	pounds.
Quintal	=	100,000.	=	220.4737	- **
Tonneau	=1	,000,000.	=	2204.737	4.6

### THE FRENCH METRE.

The French metre is intended to be the one ten-millionth part of the distance from either pole of the earth to the equator; but after it had been introduced into use, errors were discovered in the calculations employed for ascertaining that distance; so that the French metre, like the British standard yard, is not what it was intended to be. By the British standard, the length of the metre is, approximately, 1.093633 yard; or 3.280899 feet; or 39.37079 inches. By the U. S. standard it is, very approximately, 1.0935697 yard; or 3.280709 feet; or 39.368505 inches. The unit of Length is the *Metre*. The unit of Weight is the *Gram*. The unit of Capacity is the *Liter*. The unit of

Area is the Are. A Cubic Metre is called Stere.

The higher denominations are expressed by prefixing to the unit, the Greek words: Deca (10), Hecto (100), and Kilo (1000). Thus, a decametre = 10 Metres; a hectoliter = 100 Liters; a kilogram = 1000 Grammes.

The lower denominations are expressed by prefixing the Latin words: Deci (10), Centi (100), Milli (1000). Thus, a decigram is the 10th part of a Gram; a centimetre is the

100th part of a Metre, etc.

# COMMON MEASURES AND WEIGHTS, WITH THEIR METRIC

EQUIVA	LENTS.	
Common Measure.	$Eq^{\cdot}$	uivalents.
An inch	2.54	Centimetres.
A foot		Metres.
A yard	.9144	+4
A rod	5.029	
A mile	1.6093	Kilometres.
A square inch	6.452	
A square foot	.0929	
A square yard	.8361	Sq. "
A square rod	25.29	Sq. "
An acre	.4047	
A Square mile	259.008	Hectares.
A cubic inch	16.39	Cu. Centimetres.
A cubic foot	.02832	Cu. Metre.
A cubic yard	.7646	
A cord	3.624	Steres.
A liquid quart	.9465	Liter.
A gallon	3.786	Liters.
A dry quart	1.101	66
A peck	8.811	66
A bushel	35.24	44
An ounce Avoir.	28.35	Grams.
A pound "	.4536	Kilogram.
A ton _ "		Tonneau.
A grain Troy	.0648	
An oz; "		Grams.
A 1b., "	.3732	Kilogram.

WAGES TABLE-YEARLY, MONTHLY, WEEKLY AND DAILY-TEN HOURS TO THE DAY.

					_		
WAGES	WAGES	WAGES	WAGES	WAGES	WAGES	WAGES	WAGES
PER	PER	PER	PER	PER	PER	PER	PER
YEAR.	MONTH.	WEEK.	DAY.	YEAR.	MONTH.	WREE.	DAY.
\$1000 is	\$83.33	\$19.23	\$2.74	\$295 is	\$24 58	\$5.67	81c.
975	81 25	18.75	2 67	290	24.17	5.58	79
950	79.17	18.27	2.60	285	23 75	5.48	78
925	77.08	17.79	2.53	280	23.33	5.38	77
000	75 00	17.31	2.47	275	22 92	5.29	75
875	72.93	16.83	2.40	270	22.50	5.19	74
650	70.83	16 35	2.33	260	21.67	5 00	71
825	68.75	15.87	2.26	250	20.80	4.81	69
500	66.67	15.39	2.19	240	20.00	4.62	66
775	64.58	14.90	2.19	235	19 58	4 52	64
750	62.50	14.42	2.05	230	19.17	4.42	63
725	60.42	13.94	1 99	225	18.75	4 33	62
700	58.33	13.46	1.92	220	18.33	4 23	60
675	56.25	12.99	1.85	215	17.92	4 13	59:
650	54 17	12.50	1.78	210	17.50	4 04	58
625	52.08	12.02	1.71	205	17.08	3.94	56
600	50.00	11.54	1.64	200	16.67	3 85	55
675	47.92	11.06	1.58	195	16.25	3.75	53
550	45.83	10 58	1.54	190	15.83	3.64	52
525	43.75	10.10	1.44	185	15.42	3.56	51
500	41.67	9.62	1.37	180	15.00	3 46	49
475	39.58	9.13	1.30	175	14.58	3.37	48
450	37.50	8.66	1.23	170	14.17	3.27	47
425	35.42	8.17	1.16	165	13.75	3 17	45
400	33.33	7.69	1.10	160	13.33	3.08	44
390	32.50	7.50	1.07	155	12.92	2.98	42
330	31.67	7.31	1.04	150	12.50	2.88	41
375	31.25	7.21	1.03	145	12.08	2.79	404
370	30.83	7.12	1.01	140	11.67	2 69	38
360	30.00	6.92	.99	135	11.25	2.60	37
350	29.17	6.73	.96	130	10.83	2 50	30
31)	28.33	6.54	,93	125	10 42	2.40	3₽
330	27.50	6.35	.90	120	10.00	2 31	33
325	27 08	6.25	.89	115	9.58	2,21	31
320	26 67	6.15	.88	110	9.17	2.11	30
310	25.83	5.96	.85	105	8.75	2 02	20
300	25.00	5.77	82	100	8.33	1.92	27
		5.96	.82		8.33		

TABLE OF BOARD OR RENT, BY THE WEEK, SHOW-ING IT FOR DAYS.

. 25	.50	.75	SI	\$2	\$3	\$4	\$5	Days.	86	\$8	\$9	\$10	\$11	\$12	\$15
.02	.07	.05	.07	.29	.21	.57	.71	ĩ	.43	1.14	264 1∴29	1.43	1.57	1.71	2.14
.07	.21	.32	.29	.86	1 29	1.14 1.71	2.14	3	2.57	3.43	3.86	4.29	3.14 4.71	5.14	6.43
,18	.36	.43 .54 .64	.71	1.43	2.14	2.29 2.86 3.43	3.57	5	4.29	5.71	6.43	7.14	6.29 7.86 9.43	8.57	10.74
21ء 25ء	.50	. 75	1 00	2.00	3.00	4.00	5 00	7	6.00	8.00	9.00	10.00	11 00	12.00	15.00

TABLE OF WAGES

For One Week, Two Weeks, Three Weeks, or Four Weeks.

	-								_			
EE.	DAYS.	\$1 00	\$1 50	\$2 00	\$2 50	\$3.00	\$3.50	\$4.00	\$4.50	\$5.00	\$5.50	\$6.00
FIRST WEEE.	1 2 3 4 5 6	.16% .33½ .50 .66% .83½ 1 00	.25 .50 .75 1.00 A.25 1.50	.331/3 .662/8 1.00 1.331/3 1.662/9 2.00	.41% .831% 1.25 1.66% 2.081% 2.50	1.00 1.50 2.00 2.50 3.00	.55½ 1.16⅔ 1.75 2.33⅓ 2.91⅙ 3.50	12 00	.75 1.50 2.25 3.00 3.75 4.50	.831/8 1.66*/3 2.50 3.331/4 4.16*/8 5.00	.91% 1.831% 2.75 3.66% 4.581% 5.50	1.00 2.00 3.00 4.00 5.00 6.00
2ND WEEK.	7 8 9 10 11 12	1.16% 1.33% 1.50 1.66% 1.83% 2.90	1.75 2.00 2.25 2.50 2.75 3.00	2.331/3 2 667/8 3.00 3 331/6 3 667/3 4.00	2.91% 3.331% 3.75 4.16% 4.58% 5.00	3.50 4.00 4.50 5.00 5.50 6.00	4.08½ 4.66⅔ 5.25 5.83⅓ 6.41⅔ 7.00	4.66% 5.33% 6.00 6.66% 7.33% 8.00	5,25 6,00 6 75 7,50 8,25 9,00	5.83½ 6.66% 7.50 8.33⅓ 9.16% 10.00	6.41% 7.331% 8.25 9.16% 10.081% 11.00	7.00 8.00 9.00 10.00 11.00 12.00
SRD WEIR.	13 14 15 16 17 18	2.16% 2.33% 2.50 2.66% 2.83% 3.00	3.25 3.50 3.75 4.00 4.25 4.50	4.331/s 4.66% 5.00 5.331/s 5.66% 6.00	5.41% 5.831% 6.25 6.66% 7.081% 7.50		10.50	12.00	10.50 11.25 12.00 12.75 13.50	12.50 13.33½ 14.16⅔ 15.00	12.83\/3 13.75 14.66\/3 15.58\/3 16.50	13.00 14 00 15.00 16 00 17.00 18.00
drn Weer,   3mb	19 20 21 22 23 24	3.16% 3.331/4 3.50 3.66% 3.831/5 4.00	4.75 5.00 5.25 5.50 5.75 6.00	6.331/4 6.662/3 7.00 7.331/3 7.662/9 8.00	7.91% 8.33% 8.75 9.16% 9.58% 10.00					15.831/s 16.662/s 17.50 18.331/s 19.163/s 20.00	17.41% 18.331% 19.25 20.16% 21.031% 22.00	19.00 20 00 21.00 22 00 23.00 24.00
EK.	DAYS.	\$6.50	\$7.00	\$7.50	\$8.00	\$9.00	\$10	\$11	\$12	\$13	\$14	\$15
FIRST WEEK.	GUNGUNE DAYS.	1.081/6 2.162/3 3.25 4.331/4 5.412/3 6.50	\$7.00 1.16% 2.331% 3.50 4.66% 5.831% 7.00	\$7.50 1.25 2.50 3.75 5.00 6.25 7.50	1.33\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	1.50 3.00 4.50 6.00 7.50	\$10 1.66% 3.33% 5.00 6.66% 8.33% 10.00	1.831/3 3.66% 5.50	2.00 4.00 6.00 8.00 10.00	2 16% 4.331% 6.50 8.66%	2.33½ 4.66¾ 7.00	2.50 5.00 7.50 10.00
WEEK.	123456 789011	1.081/4 2.162/3 3.35 4.331/4 5.412/3 6.50 7.581/6 8.662/3 9.75	1.16% 2.331/3 3.50 4.66% 5.831/3	1.25 2.50 3.75 5.00 6.25 7.50 8.75 10.00	1.33½ 2.66⅔ 4.00 5.33⅓ 6.66⅔ 8.00 9.33⅓ 10.66⅔	1.50 3.00 4.50 6.00 7.50 9.00 10.50 12.00	1.66% 3.33% 5.00 6.66% 8.33% 10.00 11.66% 13.33%	1.83½ 3.66% 5.50 7.33½ 9.16% 11.00 12.83¼ 14.66%	2.00 4.00 6.00 8.00 10.00 12,00 14.00 16.00	2 162/3 4 .331/3 6 .50 8 .662/3 10 .831/3 13 .00 15 .162/3 17 .331/3 19 .50	2.33½ 4.66¾ 7.00 9.33⅓ 11.66¾ 14.00	2.50; 5.00; 7.50; 10.00; 12.50; 15.00; 17.50; 20.00; 22.50;
_	7,7890112 13415617	1.09¼ 2.16% 3.35 4.33¼ 5.41% 6.50 7.58¼ 8.66% 9.75 10.63¼ 11.91% 13.00	1.16°24 2.331/3 3.50 4.66°23 5.831/3 7.00 8.16°24 9.331/3 10.50 11.66°24 12.831/3 14.00 15.16°23 16.331/3 17.50	1.25 2.50 3.75 5.00 6.25 7.50 8.75 10.00 11.25 12.50 13.75 15.00	1.33\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	1.50 3.00 4.50 6.00 7.50 9.00 10.50 12.00 13.50 16.50 18.00 21.00 22.50 24.00 25.50	1.66% 5.00 6.65% 8.331/3 10.00 11.66% 13.331/3 15.00 16.66% 20.00 21.66% 23.331/3	1.83\/, 3.665\/, 5.50 7.33\/, 9.16\/, 11.00 12.83\/, 14.66\/, 16.50 18.33\/, 20.16\/, 22.00 23.83\/, 25.66\/, 27.50	2.00 4.00 6.00 8.00 10.00 12,00 14.00 18.00 22.00 22.00 24.00 28.00 28.00 30.00 32.00 31.00	2 16% 4.331/4 6.50 8.66% 10.831/3 13.00 15.16% 17.331/3 19.50 23.831/4 26.00 28.16% 30.331/4 30.331/4	2.331/3 4.662/3 7.00 9.331/3 11.662/3 14.00 16.331/3 18.662/3	2.50 5.00 7.50 10.00 12.50 15.00 17.50 20.00 22.50 25.00 27.50 30.00 32.50 35.00 35.00 35.00

### TABLE OF WAGES BY THE WEEK, FROM \$2 TO \$20.

\$2	\$21/2	\$3	\$31/6	\$4	\$41/6	\$5	Days	\$7	88	\$9	\$10	\$12	\$15	\$20
.29		.43		.57		.71			1.14					
.08		~13						. 29	.33	.38	.42			.83
.17	.21	.25					26	,58	.67					1.67 2.50
.23	.31				.56 .75			1 12	1.00	1.10	1.67			
.50					1/13				2.00					
.67	.83		1.17	1.33	1,50	1.67	2	2.33	2.67	3.00	3.33		5.00	
					1.88				3,33				6.25	
					2.25								7.50	
					2.63 3.00				$\frac{4.67}{5.33}$				8.75 10.00	
					3.38				6.00				11.25	
					3.75				6.67				12,50	
1 83	2.29	2.75	3.21	3.67	4.13	4.58	516	6.42	7.33	8.25	9.17	11.00	13.75	18.33
2.00	2.50	3,00	[3.50]	4.00	4.50	5.00	6	7.00	8.00	9.00	10.00	12.00	15.00	20.00

EXPLANATIONS.—The rate per week will be found in the top lines, and the time, in the middle columns. For example, at \$7 per week, the wages for four-and-a-half days will amount to \$5.5.

### TABLE OF WAGES BY THE DAY .- The 10 Hour System.

\$1	\$11/4	\$13%	\$134	\$2	\$21/4	\$21/2	Hours.	\$23/4	\$3	\$31/4	\$31/2	\$1	\$11/2	\$5(
.10		.15	.18	.20	.23		1	.28	.30	.33		.40	.45	.50
.20							2	.55	.eo					1.00
.30	.38	.45					3	.83	.90				1.35	
.40						1.00 1.25	- 2						$\frac{1.80}{2.25}$	
.60						1.50							2.70	
.70						1.75							3.15	
						2.00							3.60	
.90			1.58										4.05	
1.00	1.25	11.50	1.75	2 00	2.25	2.501	10	12.75	13.00	13.25	3.50	14.00	4.50	5.00

### TABLE OF WAGES BY THE DAY .- The 8 Hour System.

\$1	\$11/4	\$11/2	\$134	\$2	\$21/4	\$23%	Ecurs.	\$23/4	\$3	\$31/4	\$31/2	\$1	\$13/2	\$3
.13	.16	.19	.22					.34	.38				.56	
.25								.69		.81	.88	i.00	1.13	1.25
.38					.84								1.69	
.50			.88											2.50
.63	.78		1.09											3.13.
.75			1.31											3 75
			1.53					2.41	2.63	2.84	3.06	[3.50]	3.94	4.38
1.00	11.25	11.50	1.75	2 00	12.25	13 20	_ ŏ	2.75	3 00	3 25	3 50	14.00	14.50	5 00

# TABLE OF WAGES BY THE WEEK. \*Ten Hours Rev Day.

							1 2	
Per	5	4	3	2	r <sub>1</sub>	14	Day.	∠1
Week.	Days.	Days.	Days.	Days.	Day.	Day.	Day.	Hour.
2.00	1.66%	1.331/6	1.00	.662/3	.331/3	.16,66	. 8 33	3.56
2.50	2.0813	1.652%	1.25	.801/3	212/3	.20 08		4 1
3.50	2.91%	2.3314	1.75	1.16%	.581/3	.29 }	.10 1/2	5.08
4.00	3.331%	2.66%	2.00	1.331/3	.66%	.33 33	16.06	
4.50	3.75	3.00	2.25	1.50	.75	.37 1/2	.18 34	6 06
i.00	4.16%	3,3316	2.50	1.66%	.831/9	.41.66	.20 08	8 33
5.50	4.162/3	3.66%	2.75	1.831/3	.91%	.45.08	.22.23	9 1
6.00	5.41%	4.3313	3.25	2.16%	1.081/3	.54 분	.27.12	9 1
7.00	5,831/6	4.66%	3.50	2.3613	1.16%	.58.33	.29 1	11.66
7.50	6.25	5.00	3.75	2.50	1.25	. 62 1/2	.31 1/4	12 1/2
8.00	6.66%	5,331/3	4.00	2 66%	1.331/3	. 66.66	.33.33	13.33
9.00	7.50	6.00	4.50	3.00	1.50	.75	.37 1/2	15 '.
10.00	8.331/6	6.66%	5.00	3.331/3	1.66%	.83.33	.41.66	16.66
11.00	9.16%	7.331/3	5.50	3.66%	1.831/3	.91.66	.45.08	18.33
13.00	10.831/6	8.66%	6.50	4.331/3	2.16%	1.08.33	.54 4	21.66
14.00	11.66%	9.331/8	7.00	4.66%	2.331/6	1.10.66	.58.66	,23_33
16.00	13.331/3	10.66%	8.00	5.361/3	2.66%	1.33.33	.66.66	26 66
	14 16%	11.331/3	8.58	5.66%	2.831/3	1.41.66	.70.08	28.33
19 00	15.831/8	12.66%	9.50	6.331/3	3 16%	1,58.33	.70 ह	31,68
20.00	16 66%	13 331/3	10.00	6 66%	3 331/3	1.66.66	.83.33	33 33
21.00	17.50	14.00	10.50	7.00	3 50	1.75	.87 1/9	35
22.00	18.331/6	14.66%	11.00	7.331/1	3 66%	1.83.33	.91.65	36.AG
23.00	19.16%	15.331/3	11.50	7.66%	3 H31/4	1.91.66	.95.08	38.33
25.00	120.83	116,66%	12.50	8.331/3	4 16%	12.08.33	1.01 6	41.00

## INDEX.

								70	37.
								Pag	ge No,
Acre, hills and plants on			_	_					189
			_	_					. 190
hills in an - planted in rows or	A.s.i	11	•	•					187
planted in rows or	arı	118		•	-	•	-		190
measure of seeds, bulbs, etc., r	-	: .	-	•	-	•	-	•	188-189
seeds, bulbs, etc., r	equ	ired	for		•	-	-		
seeds to an -		•	-	-	-	-	-	- •	- 188
square feet and fee	et sq	uare	Э	-	-	•	- (		190
to estimate grain of	crops	s for	•	-	-	-	-		- 190
Air, in motion -	. 1	-	-	-	-	-	-		172
	ortic	n o	f	_	-	_	-		- 216
Alloys and composition fusible points of	01 010	-					_		25-26
fusible points of				_	_	_			- 26
Alphabets of different la			ī			-			219
				-	-	•			143
American and German	rybe		-	•	-	-	-		
Amount of earnings of 1	ran	IS 01	1	-		-		·	220
Amount of earnings of I	cen	it to	200	per	day,	Ior	nve :	rears	201
					-	-	-	- '	
Appleby's table single-ac	ctin	g pu	mps	3	-	•	-	-	- 169
Area of a circle, rule for	r	-	•		-	-	-		- 210
Areas, circum ferences, e			-	-	-	-	-		- 69-77
of cylinders				_		-	_		- 167
Belting, horse-power of		_	_	_					- 32-34
planing machi	nov	_							- 37
	nes				1				- 35
remarks on	•	•	•	~	•	•			- 36
velocity of		٠,	-	-	-	-	-		194-195
Bins and graneries, con	tent	sor		-	- 1	-	•	•	228
Birds and Animals, grou	apın	g of		•	-	-	-	-	- 204
Birds ages attained by			-	-	-	-	-	-	
Black wash	-	-	•		-	-	-	•	- 182
Blackening for moulds		-		-	-	-	-	-	- 182
Blasting	-	-		-		-	-	-	211
Blue print solution	_	-	-	_	-	-	-	-	- 185
Board measure -				_		_	_	-	155-156
contents of 1 line	al fo	not c	f ti	mhe	7"		-		- 150
Boiler makers, facts for		000		-					- 23
		-	_	-				_	. 173
tubes, surface of		à	•	·	·		•	•	- 23
pressure allowed		Gov	ern	men	t ru	ie	-	•	. 24
decrease of stren	gtn			٠.		•	•	•	
Fairbairn's dime		ons	of ri	vets	sfor			1	. 23
horse-power of							,		. 24
thickness of				1					. 22
Bolts and nuts, dimens:	ions	of							. 52
diamete	ers a	nd l	rea	kin	g str	ain			. 214
Boots, to render water-p							- 1		184
Boring and turning						Ĭ.			6-7
Boxes, capacity of	•	•	•	•	•	-	•	•	195-196
		•	•	•	•	•	•	•	183
Driels wouls	•		•	•	•	•		•	88-89
Brick work			•	•	•	•	•	•	90
Directo, number require	(I								。 90 89
red wash for									
Bronzing	c		,						181-182
Castings, shrinkage of					-				. 208
Cattle, age of . ,									. 198
Cements									176-178
Chemical kingdom									. 5-6
substances, co	amn	ion	nam	es f	or				216-21 <b>7</b>
zuostances, c	J.1111	MOIL.							

Cisterns, capacity of									170-171
Consumption of coal in		nes	•						. 167
of hay for	food								. 200
Copyright, regulations (			•.	,					175
Cores and core prints, re			for		•			•	215
Corn, to protect newly pl	lante	ed.	•				•		189
Corn stalks, to protect fr	om i	nice	•	•	•	•	•		190
Cost of articles by piece	or ac	ozen	L	•	•	•	•	•	223 16
Couplings, flang and hal Cubic feet, weight of in	1 lap	mond	anh			•	•		199
Cutter, speed of .	шпе	геп	sub	stan	ices			•	20
Days from 1 month to gi	van	day	in a	noth	or	•	•	•	233
Decimal approximation	for	calc	ulati	ons	101	•			144-145
equivalents for					ch			•	147
fractional equiv									148
parts of a carat							,		148
foot									146-147
pound									148
Difference between perce	enta	ge o	n an	d di	scou	ınt			221
Distance in feet gone by Domestic animals, value	y in a	sec	ond						207
Domestic animals, value	e of t	food	for						199-200
Draining, laying pipe fo	r			•					191
Drawing, colors for	•	•			•	•			212
Dyeing	a	•			•	·_		•	95-98
Electricity, conductors	ina i	ion-	cond	ucu	ors (	) [		٠.	80 179
Enamels Engines, horse-power of	•	•	•	•	•	•	•		210
Etching, solution for ire	an or	id of	Loo	•	• "	9	•	•	183
Everlasting naste	JII 41	III SI	cer			•	•	•	183
Everlasting paste Exemption laws of the U	Inite	a S	tates	•	•	•	•	•	237
Farmers, facts for .			-		:				185
Fields and lots, contents	sof	•	1						. 191
Files, recutting .									181
remarks on the u	se of								208
Flour paste								-	182
Fly-wheels	,			,					212
Fodder, nutritive qualit			٠.						200
Food in stock raising, re	elativ	ve v	alue	of	-	-	-	-	201
Foods, nutrition in	5		-	-	-	-	-	-	203
Foot soldier, speed of in	1 m	mui	e	-	-	-	-	-	213
Force requisite to move	a bo	ay	-	-	-	-	-	-	207 196
Freight car, capacity of	nant	-	-	-	-	-	-	-	204
Fresh water, component Gas, delivery of coal	par	US.	-		-	-	-		54-55
Gas metro state of -	-	-			-		1	-	56
Gas nine diameter and	lengi	h o	f		-		-		55-56
Gas pipe, diameter and Gearing, horse-power of		-	-		-	-	-	-	13
pitches for	_	_	-	-	-	-		-	- 8
scales for -	_	-				_	-	-	9-12
simple rules for	r	-	-	-	-	-	-	-	13
Glues	-	-	-	-	-	-	-	~	180
Goods, how to mark	-	-	-	-	-	-	-	-	224
Grains, legal weights of		:	-, ,		-	-	-	-	199
and fruits, comp	arat	ive	yield	ot		-	-	-	191
Grindstones, weight of			·	-	-	-	-	-	208
Gross price known, to fi	na si	ngl	e bri	сө	-	-	-		$\frac{221}{182}$
Hands, to clean from dy	0	•	•	-	-	-	•		$\frac{182}{211}$
Heat, effects of Herschel's table for for	atall	ina	wond	ban					218-211
Hogs, corn for food for	00011	11134	W Cott	rier					202
Holes in castings, cemer	nt fo	r		_			-		181
Hoops, angle iron -	-	-		-	-	-		-	17
Horn, to soften -	-1	-		-	-	-	-	-	182
Horse power of		-			_	_			206

			_						
Household weights and	me	asur	es						204-205
How to bend brass rule			0.5					-	105
Tee atropath of		•	•	•			•		212
Ice, strength of			•	•			•		232
Interest, calculating			٠.	٠.					252
compound, tir		none	ey de	oub	les				232
handy rules of	n								232
\$1 compounde	d								230
rates of .									234-235
on \$1 .	•	•	•	•	•	•	•	•	229
Iron, to prevent rusting		•	•	•	•	•	•	•	183
fron, to prevent rusting	В	•		•					181
value of per ton									
Knots, to kill Law, facts in									181
Law, facts in .									219
List price by which to f	ind	per o	cent	. ar	ıd n	et co	st		222
to find cost d	isco	nnte	d fr	rom	1				222
Loam	1000								182
Loggand planks to pre		t anl	:++:-		•	•	•	•	184
Logs and planks, to pre			16611	ıg	•	•	•		
Machinery, depreciation	n oi								174
Man, power of .									206
Masonry									213
Measurement, cisterns	and	casl	(S						197
corn in	oh	CLEIDA							196
corn in c	rib								196
	110				,			:	
grain in	oin	S		-					196
. of hay									197
Mensuration of solidity of solids	v of	tim	ber						151
of solids									214
of surface	20								214
of timber	. Ala	+' am	han	'n.			•	•	150
or crimber	, па	ror	ooa.	ra .	шеа	sure			
Metals, average lineal	expa	nsio	n or		•	•	-		209
relative hardne									209
to convert weig	ht o	f							145
Metric equivalents									246
Metre French									246
Notes relating to	•	•	•	,	•	•	•	•	219-220
Notes, relating to Number rivets in 100 po	٠,	•		•				-	
Number rivets in 100 po	una	S	-	-	-	-		-	44-45
Painting, glazier's putt	у	-	-	-	-	-	-	-	94
rules for	-	-	-	-	-	-	-	-	94
to soften put	tv		-	-	-	-	-		94
washes	-	_	_	_				_	95
Paints or inks, how to r	niv								109
			-	•	-	-	-	-	
Parliamentary proceed	ıngs		-	-	-	-	-	-	238-239
Parting sand	•	•	-	-	-	-	-	-	182
Patent fees, schedule o	f (U.	.S.)		-	-	-	-	-	176
Patterns, shrinkage of	cast	ings	in	-	-	-	-	-	215
weights of cas	tine	re fo	r	_	_		_	_	215
Petroleum, cutting me	e le	rith	-						184
Piling	ner I M	TUIL							
			-					-	213
Pipes, gallons and cubi	c Te	et of	wat	er	ın	-	-		172
Piston speeds, length o units of	fstr	oke		•	-	-	-	-	168
units of	$\mathbf{H}.\mathbf{P}$	. for		-	-	-	-	-	168
Pitch, diametral and c	ircu	lar	-	-		-	-	_	12
Plants, hills or trees in	acre	A				-		-	186-187
Plactoring motorials for	acr.	•		-	-	_	-	_	
Plastering, materials for	31	-			-	-		-	90-91
Plating metals	-	-	-	-	-	-	-	-	81-84
cleansi	ngo	I	-	-	-	-	-	-	85-87
Plummer-blocks, propo	rtio	ns o	f	-	-	-	-	-	18
Poisons, antidote for	-	-	-	-	-	-	-	-	224-225
Polishing compounds	-	-	-				-		180-181
Polygons									174
Population content									
Population, center of		•	-					-	206
Poultry, food for -	-		-	-	•	-		-	201
Printing, a corrected p	roof	she	et	-	-	-	-	-	115
amount of pa	per	rean	ired		-	-	-	- 1	107-108
casting of cor	v	-	-	-			-	-	104
colored on pa	ner							_	112
combination	loo d								103
combination	read	3	-	-	-	-	-	•	103

Printing, complete table of	sign	atui	ces					117-119
composition roller	rs							109
corrections of the first proof from th	pres	ss						113
first proof from th	e ty	pe						114
folding paper								106-107
how to estimate qu	aant	ity o	of ty	pe				105
imposition of for				•		1.		120-143
ink, how to mix								109
leads and slugs								109 111
leads for newspape	ers							111
marks or punctual	tion				-			113
newspaper measur	eme	nt						110
proof sheet correc	ted							116
Riley's indispensa	ble							105
roman numerals								105-106
standard newspap	er m	easi	are					111
weight of matter Proportion of the circle and								112 213
Proportion of the circle and	lits	equ	al					213
Pulleys, keys for								19
metal, round eye o:	£							19
speed of								35-36
Rail fences								198
Railway signal code ,			,		9			207
Ready reckoning and accou	nts							220
Rock and earth, measure of								207
Rooting, corrogated iron					-			98
Round timber, cubic conter	ats o	f						158
when square	ed. c	ubic	cor	tent	tś c	of		159
Saw logs, reduced to board :								149
Saws, speed of								208
Scantling measure .								152-154
Screws, cutting by lathe						•		14
gearing up lathes fo	r cu	ttin	g					18
threads for English threads for U.S.	star	dar	ď				-	16
threads for U.S.								15
Seeds, amount of oil in								204
number in pound					-			187
quantity to plant a g	iven	spa	ce					185-186
vitality of								188
Shafting, distances between	ı bea	arin	gs	-	-	-	-	19
horse-power of	-	-	-	-	-	-	-	27-31
Sheep and goats, ages of	-	-		-	-			198
food for	-	-	-	-	-	-		202
Ship building, Lloyd's rule	for		-	-	-	-	-	28
Shipping admeasurement	-	-	-	-		-	-	218
Shingles, facts about -	-	-	-	-	-	-	•	9]
Skates, sizes compared with	sho	es	-	-	-	-	2	212
Slating, facts about -	-	-	-	-	-		-	92
Slates, sizes of		-	-	-	-	2	-	98
Soldering or welding, fluxes	s for		-	-	-		•	210
Solders		-	-	-	-	-	-	210
Sound, speed of	-	-	-	-	-		-	207
Sight drafts and protested b	oills		-	-	-	-	-	240
Staining for wood -	-	-	-	-	-			183-184
Staining for wood Standard contents of logs			-	-	-	-	-	160
Statutes of limitations	-		-		-	-	•	236
Steam boilers, covering for cylinders, thickness			-	-	-	-	-	162
cylinders, thickness:	for		-	-		-	-	18
lap required for slide	e val	ves			-	-	-	166
pressure of -		-	-		-	-	-	162-164
remarks on		-	-	-	-	-	-	164
temperature of -		-	-		-	-	-	161
to ascertain average	pres	sure	of	-	-	-	-	. 166
to find lap and lead	-	-	-	-		-	•	165
vacuum to temperate	re,	ratio	)	-		-	-	165
velocity of	- A		-	-		-	-	167
Steel, preservation of -	-		-	-		-	-	183

Steel, to ascertain heat of	. 209
Stone work	. 88
Strength of cast iron square beams	. 57
cast iron columns	. 63-65 . 67-68
flat and round ropes hollow cast iron pillars	. 64
manilla cordage	. 66
materials to resist transverse strain	. 65
metals, relative power to resist torison	59
metals, tensile , .	. 59
rolled iron beams	. 65
ropes, chain cables and anchors .	. 67
short linked crane chains or ropes	. 66
white pine struts or pillars	. 60-62
wrought iron drawn tubes	. 173
Square frames, number of feet in	157
Table for marking articles @ given per cent. advance	
Tempering recipes	21-22
steel	20-21
Tile, capacity of gallons	. 192
draining of by different sizes of	. 192
Tin roofing, cost of	. 92
To compute weight of cattle	. 198
Township plat	. 205
Tracing paper	. 184
Trees, growth of	. 203
United States and foreign money	. 226-228
Varnishes	. 178-179
Wages, tables, monthly, weekly, daily, etc	- 248-250 181
Watch maker's oil	: 183
at different temperatures	: 217
flows of, at fall of 10 feet	209
power to raise	170
pressure lbs per square inch	209
Weight of materials	- 38
cast iron pipes, etc	43-44
English tin plates	- 52-53
flat rolled iron	- 50
galvanized sheet iron	- 38
iron, brass, copper, lead	- 42
iron, steel, copper and brass wire	- 46 - 39-40
lead pipe leaden balls	- 39-40
number nails in 1 pound	- 45
tacks in 1 pound	- 46
tacks in 1 pound parallel angle and T iron	- 44
round bolt copper	- 41
sheet and bar brass	. 41
shot	- 41
square and round malleable bar iron	- 47-48
taper, angle and T iron	· 45
water at different temperature	51
" in pipes of various diameters	- 51
window glass	- 40
Weights and measures	- 47
miscellaneous	- 241-245 - 203
Welding steel, mixture for	- 183
Wheat, English weight of	- 204
Wines and liquors	- 215
Wire guages, American and English	- 33
rope, horse-power of	37
Wood-working machinery, velocity of	- 7
Woods for fuel, value of	- 212
wrought from welded tubes, dimensions of	- 53-54

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